



UC San Diego

2025 PEER Annual Meeting



Friction-based Force-limiting Connections

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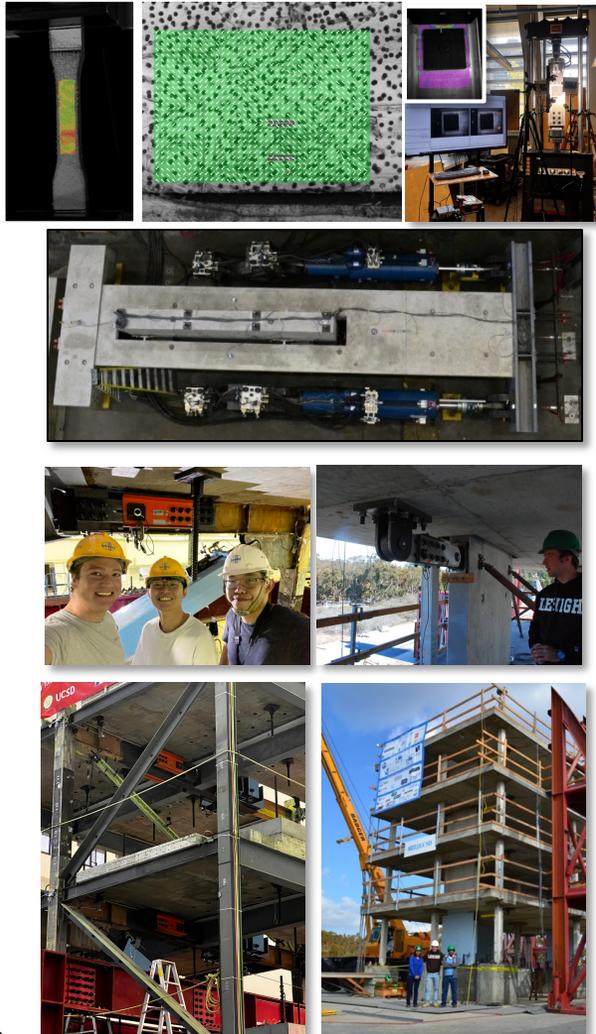
March 26, 2025
UC Berkeley, CA



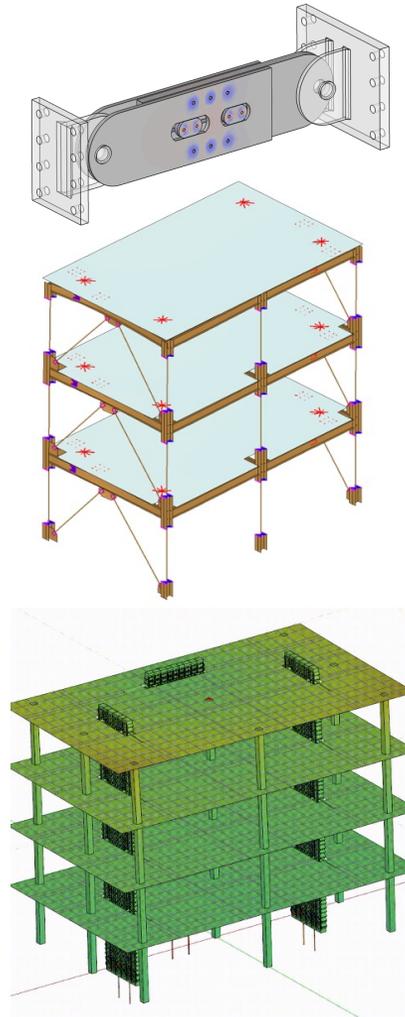
<http://tsampras.ucsd.edu>

Overall, our research group at UC San Diego aims to contribute to the improvement of safety and resilience of our built environment and education of structural engineering students

Experimental



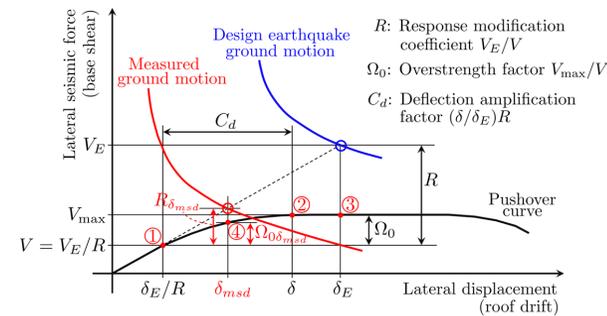
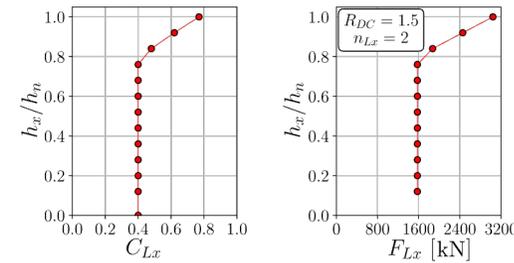
Computational



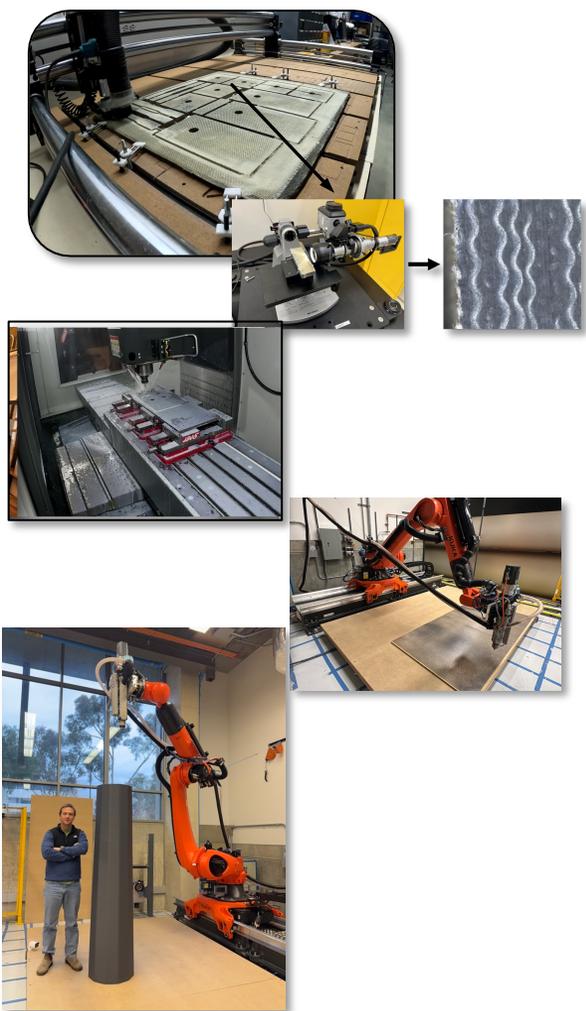
Design

$$F_{Lx} = \frac{C_{Lx}}{R_{DC}} \frac{w_{px}}{n_{Lx}}$$

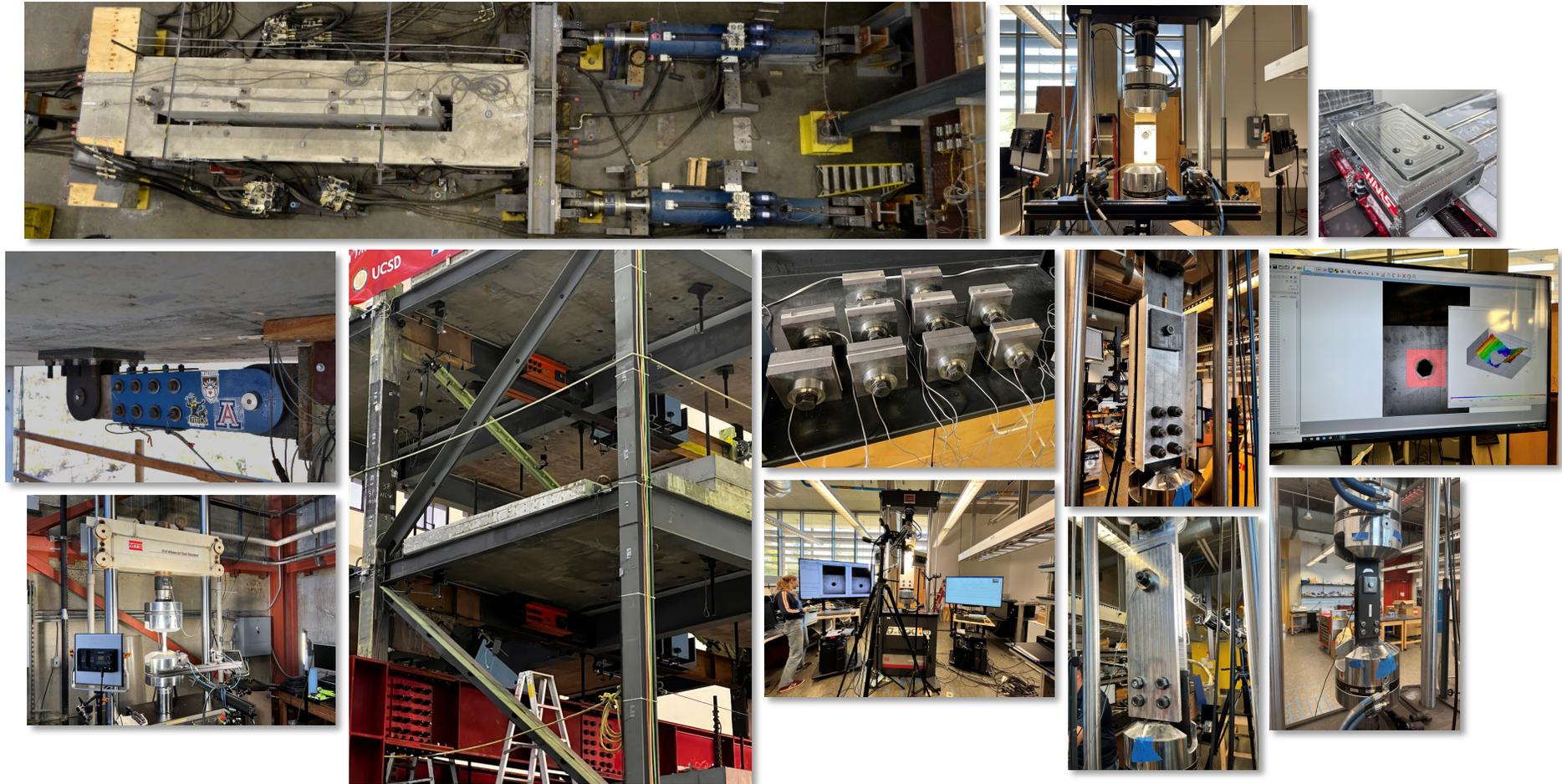
Connection force vs Connection deformation graph showing a bilinear relationship with parameters $\alpha K_e L_x$ and $K_e L_x$.



Hybrid Manufacturing



My **Goal** is to share findings from friction related experimental research at the material-, component-, and system-level that we conducted since 2011.



<http://tsampras.ucsd.edu>

Scope

- Benefits of friction-based structural components
- Experimentally observed challenges
- Research to address the challenges

ACKNOWLEDGMENTS – WORK RELATED TO FRICTION

Inertial Force-limiting Floor Anchorage Systems For Seismic Resistant Building Structures (2011-2016): Robert Fleischman, Jose Restrepo, Richard Sause, Joe Maffei, David Mar, Dichuan Zhang, Zhi Zhang, Ulina Shakya, Arpit Nema, Gabriele Guerrini

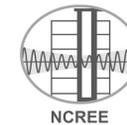


Alternative designs of friction-based connections (2020-Present):

Kaixin Chen, Franco Mayorga, Yeon Li, Dominic Tran, Anne-Sophie Roobol, Anthony Li



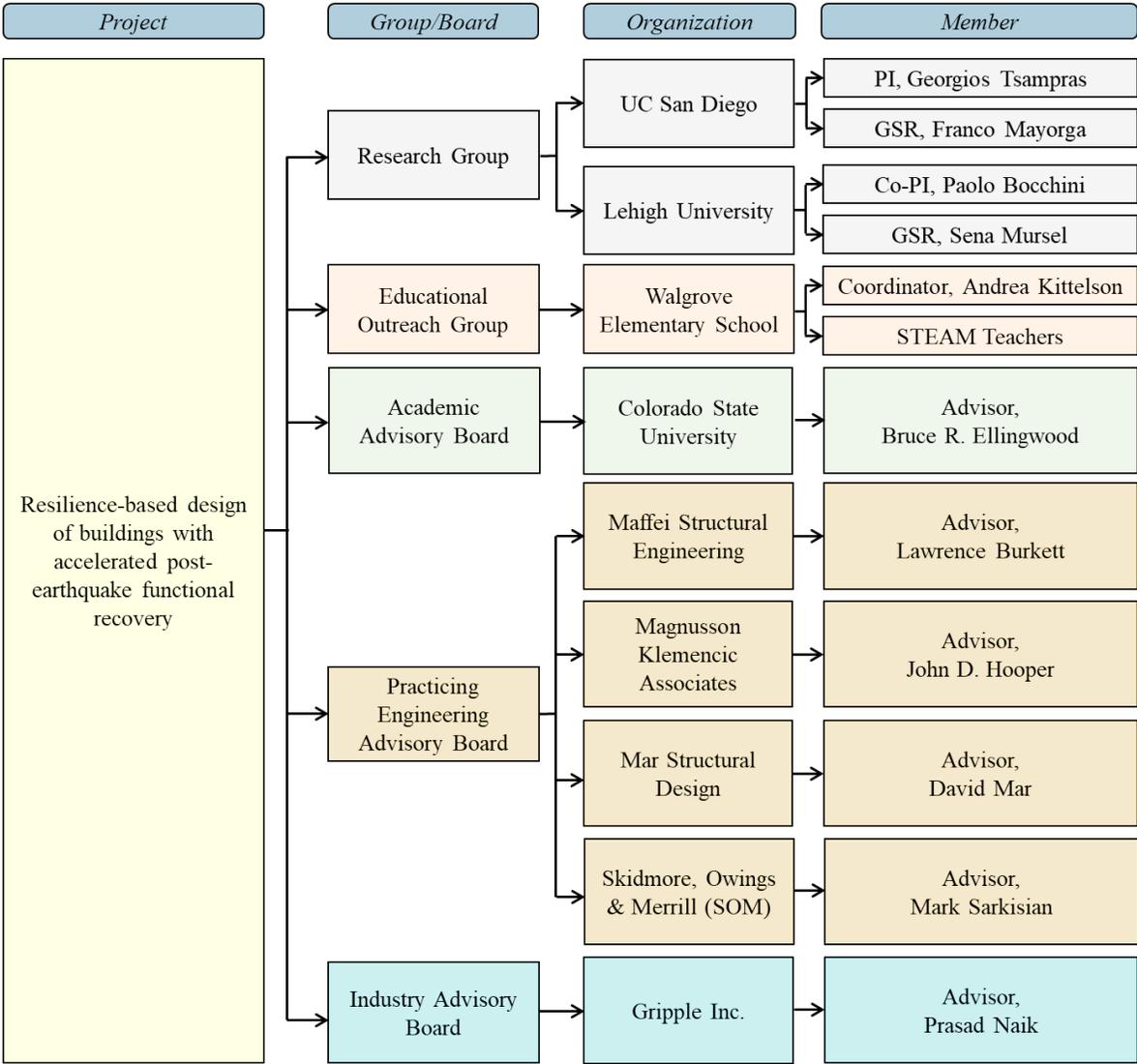
Steel buildings with sliding floors and elastic frames (2022-2025): Chung-Che Chou, Shih-Ho Chao, Chia-Ming Uang, Li-Yu Huang, Chi-Jeng Wu, Alvaro Cordova, Huang-Zuo Lin, Shu-Hsien Chao, Nicholas Tedjasukmana, Ming-Yen Xie, Wei-Xuan Chen, Hao Wei Jian



Design related ongoing research



Disaster Resilience Research Grant



Video Presentation



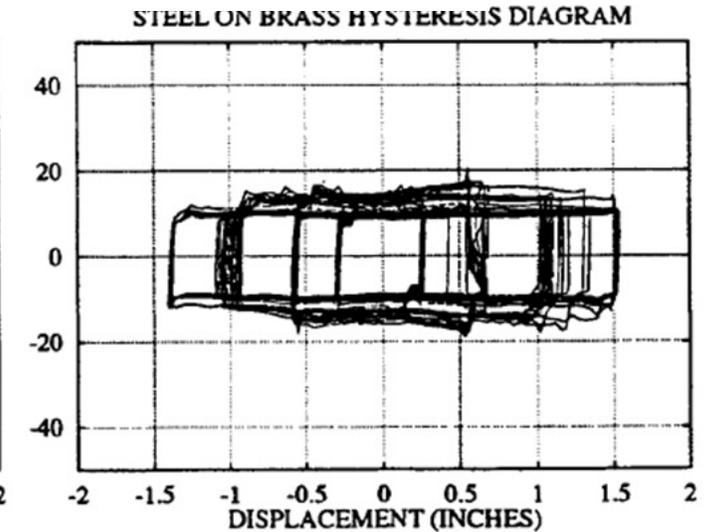
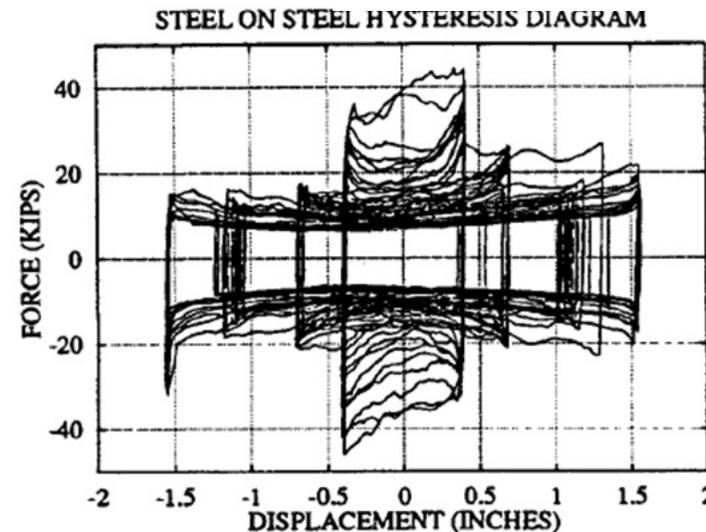
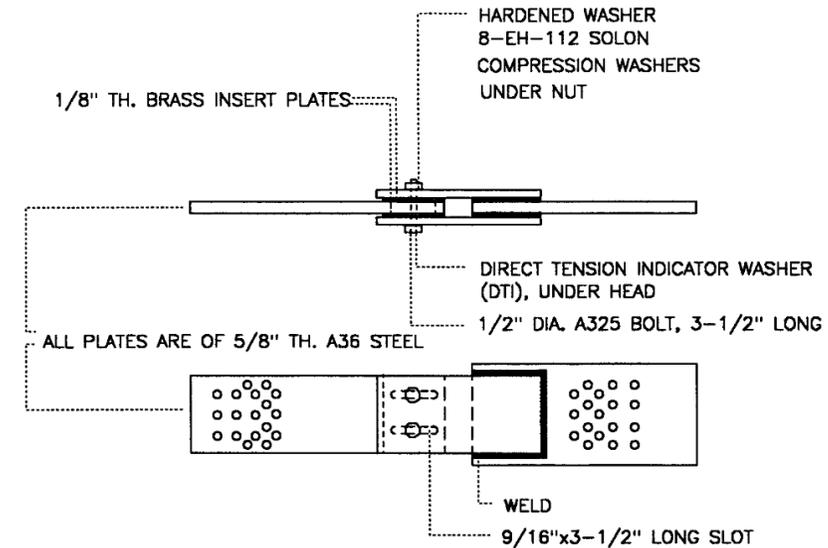
Friction-based components in structural engineering

Early work by

- Clark et al. 1973 – Limit forces in foundations
- Pall 1979, Pall and Mash 1982
- Filiatrault and Cherry 1987
- Aiken, Kelly, Pall 1988
- Anagnostides 1988
- Giacchetti, Whittaker, Bertero, Aktan 1989
- FitzGerald, Anagnos, Goodson, and Zsutty 1989
- Tremblay 1993
- Grigorian, Yang and Popov 1993

Example applications

- Bridge structures
- Precast concrete structures
- Steel braced frames
- Moment resisting frames
- Self-Centering Moment Resisting Frames
- Rocking Walls (Reinforced concrete and timber)
- Friction dampers
- Self-centering friction-based braces

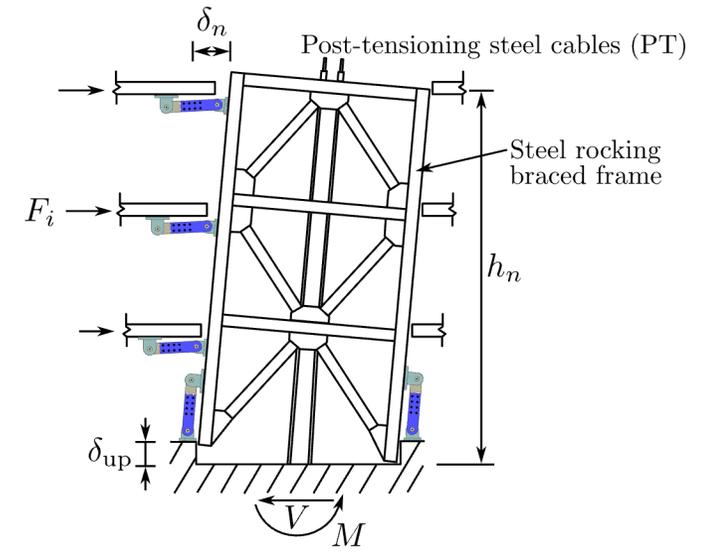
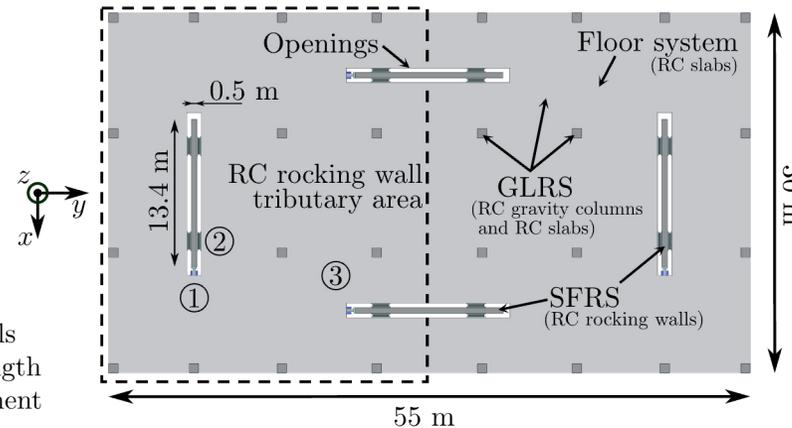
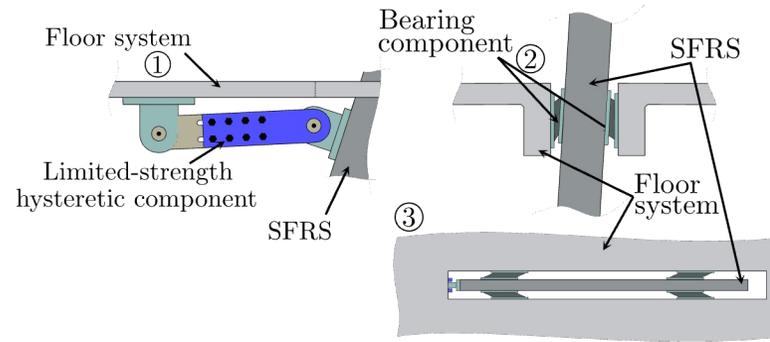
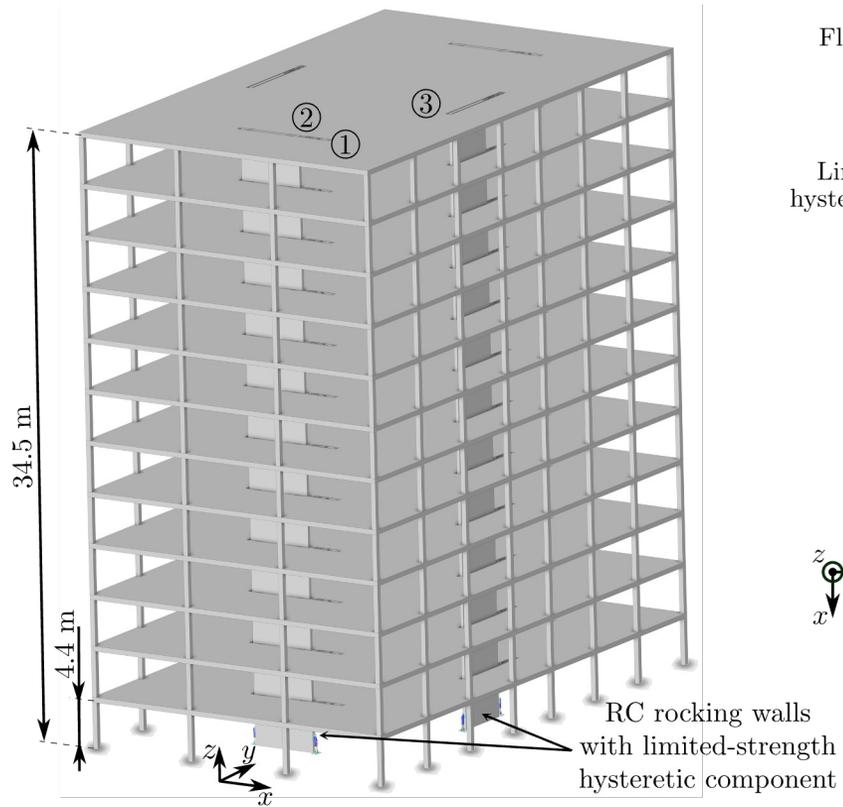


Grigorian, Yang and Popov 1993

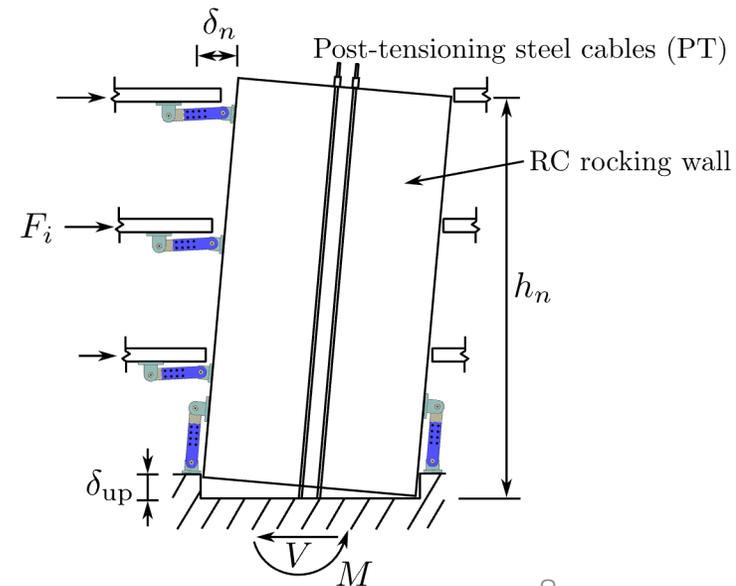
Literature review available in:
Tsampras et al. (2018), Chen et al. (2023)



Example use of friction-based force-limiting connections

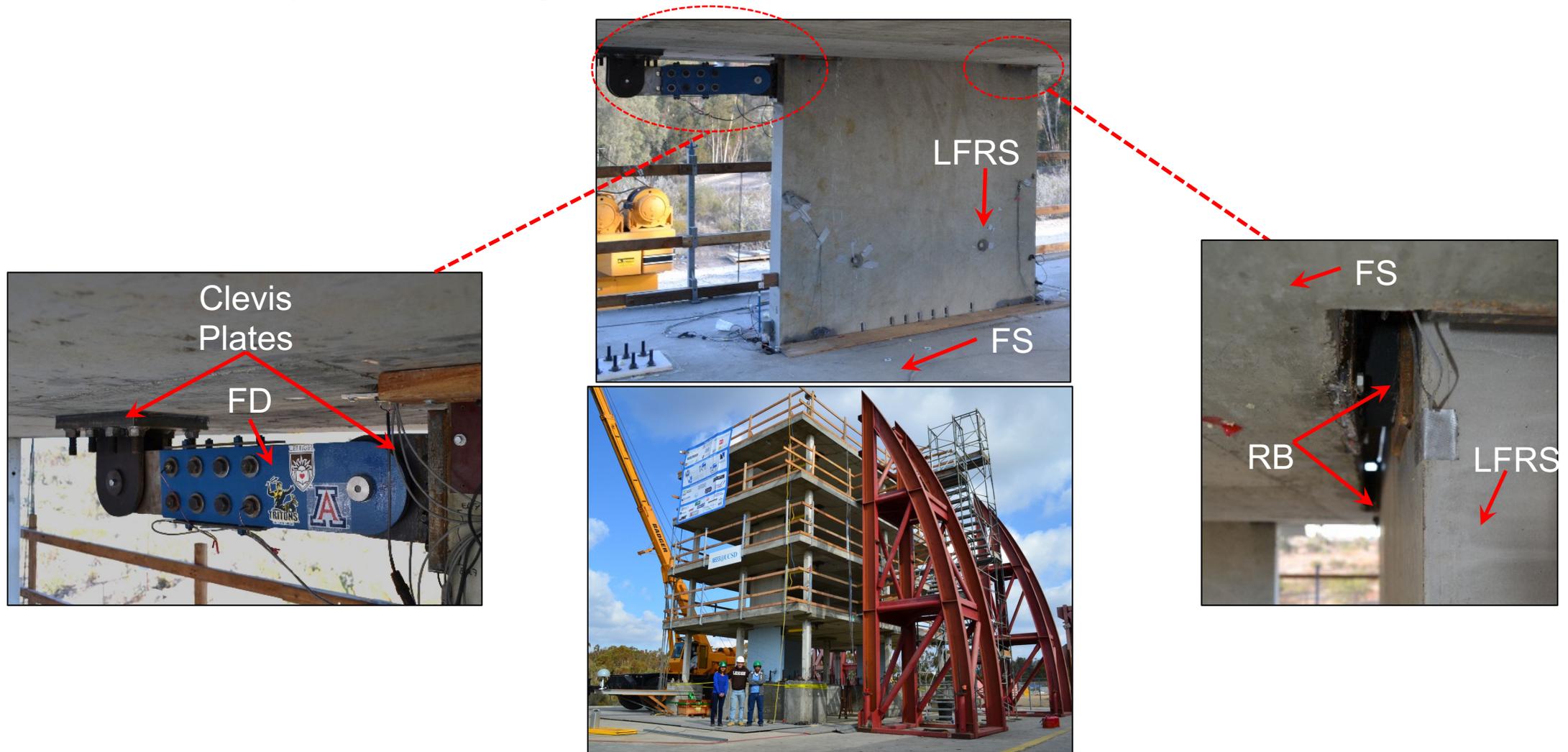


or



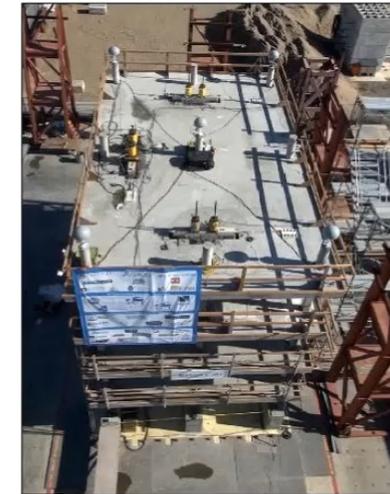
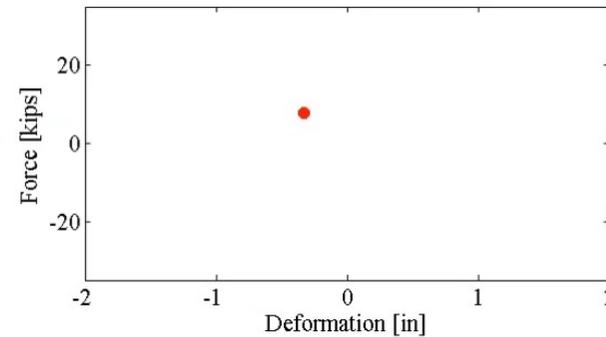
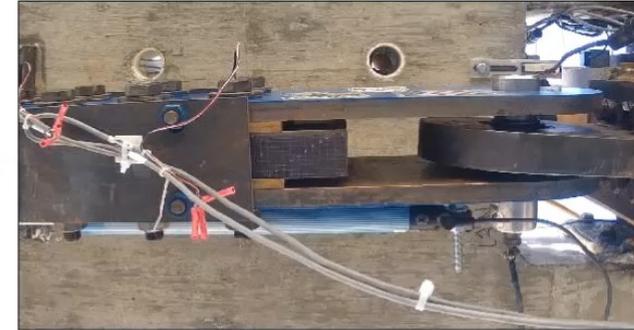
Example Installation of Force-Limiting Connection

Half-Scale 4-story Precast Rocking Shear Wall Structure at NEES @ UCSD



Example Installation at NEES @ UCSD

EQ 14: Berkeley MCE - Floor 4

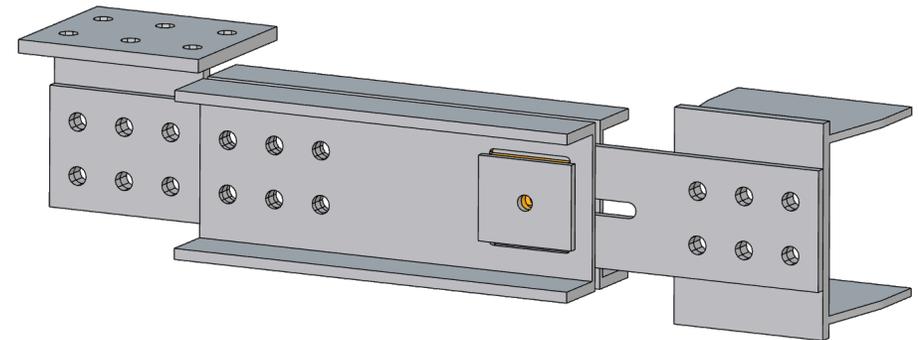
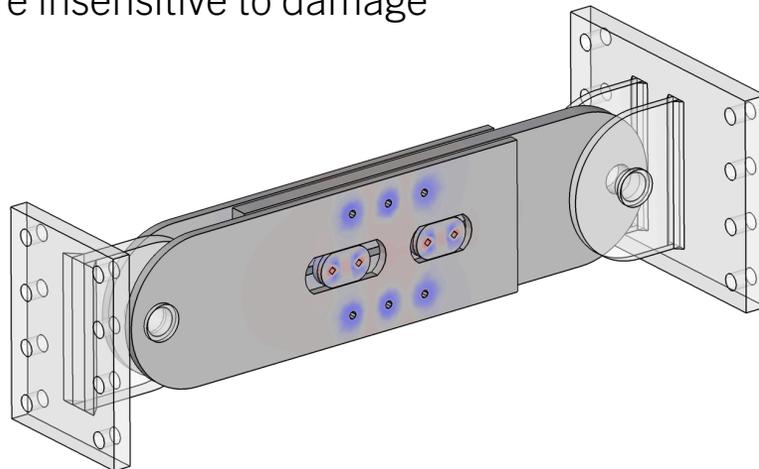
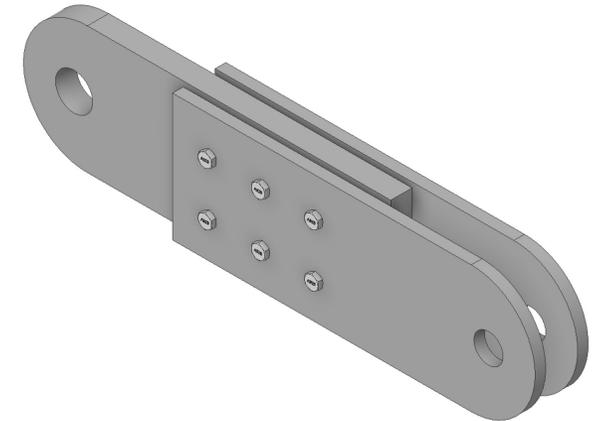
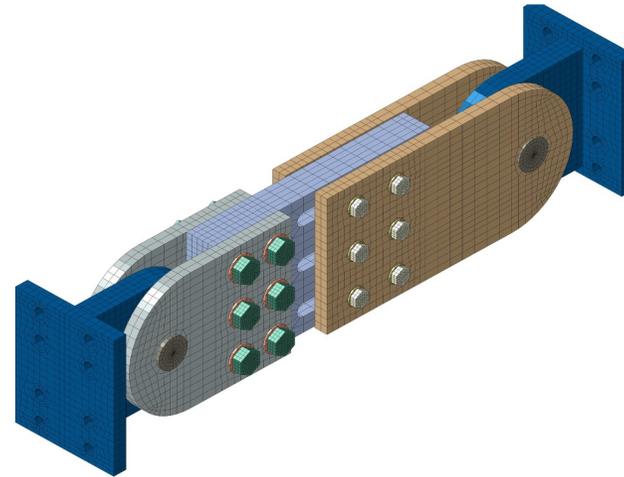


Zhi Zhang, Robert B. Fleischman, José I. Restrepo, Gabrielle Guerrini, Arpit Nema, Dichuan Zhang, Ulina Shakya, Georgios Tsampras, Richard Sause (2018), Shake table test performance of an inertial force-limiting floor anchorage system, *Earthquake Engineering & Structural Dynamics*, 47 (10), 1987-2011, doi: [10.1002/eqe.3047](https://doi.org/10.1002/eqe.3047)

Georgios Tsampras, Richard Sause, Robert B. Fleischman, José I. Restrepo (2017) Experimental study of deformable connection consisting of friction device and rubber bearings to connect floor system to lateral force resisting system, *Earthquake Engineering & Structural Dynamics*, 47 (4), 1032-1053, doi: [10.1002/eqe.3004](https://doi.org/10.1002/eqe.3004)

Why friction-based force-limiting connections?

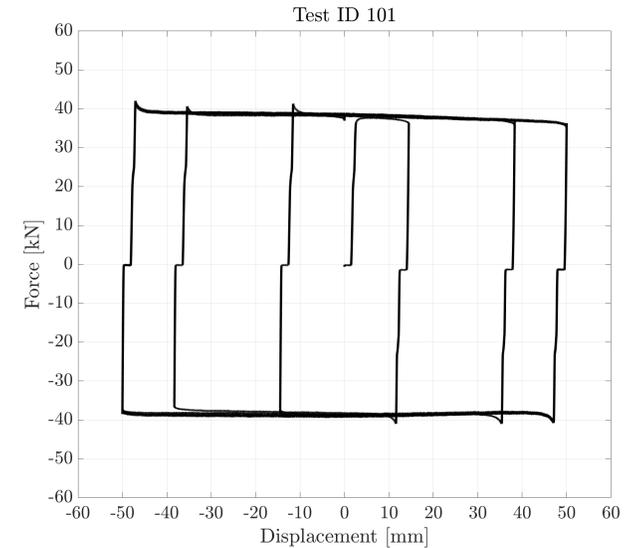
- **Structural engineers have freedom in detailing**
- Easy adjustments to achieve target force levels
- Decoupled stiffness and sliding friction force
- Possible designs with easy manufacturing and assembly
- Increase of displacement capacity by including longer slots in the design – no strain limitations
- Designs that allow low-damage and easy reparability
- Some designs are insensitive to damage



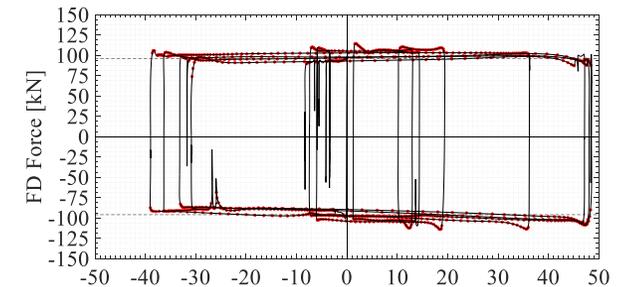
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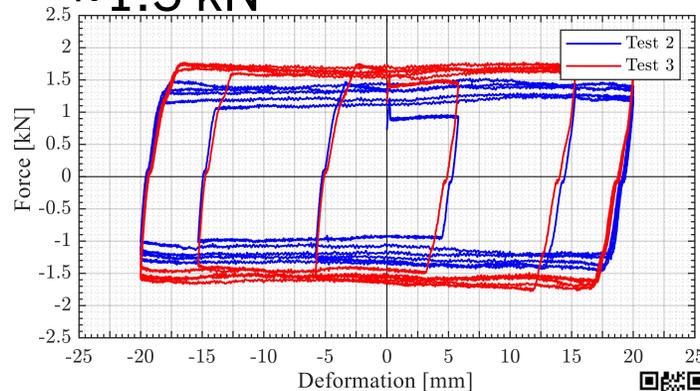
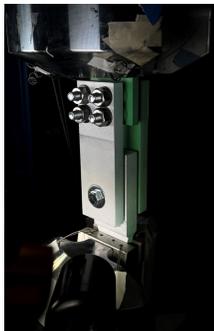
~40 kN



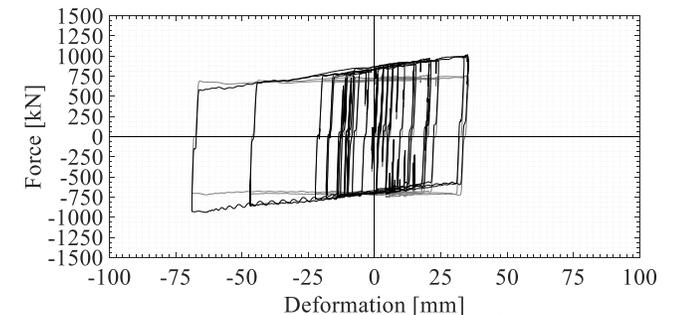
~100 kN



~1.5 kN

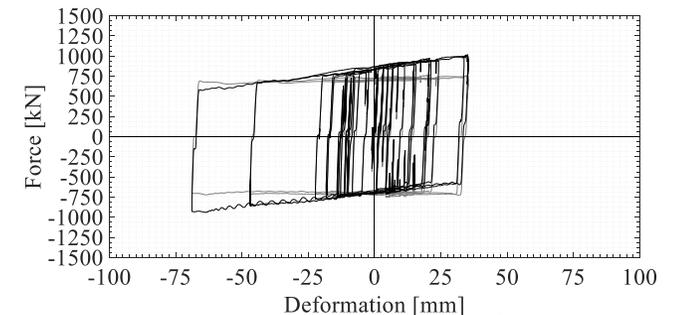
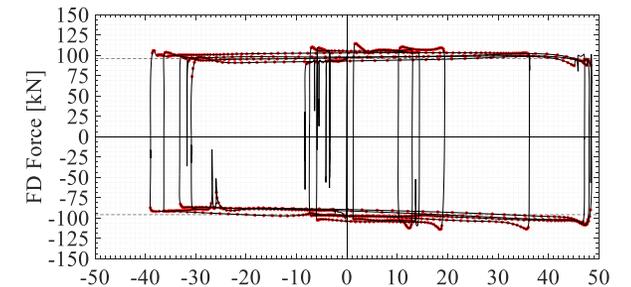
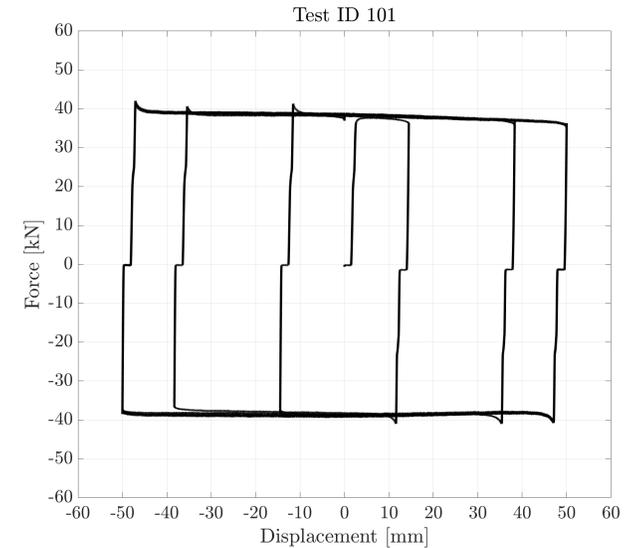


~750 kN



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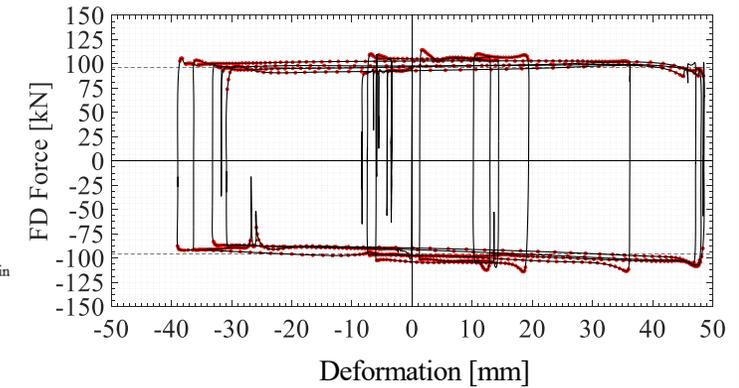
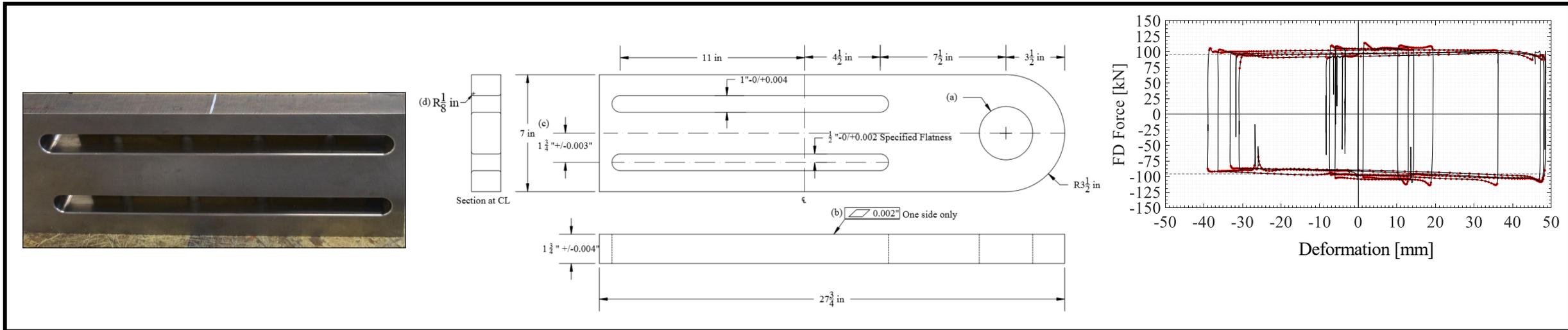
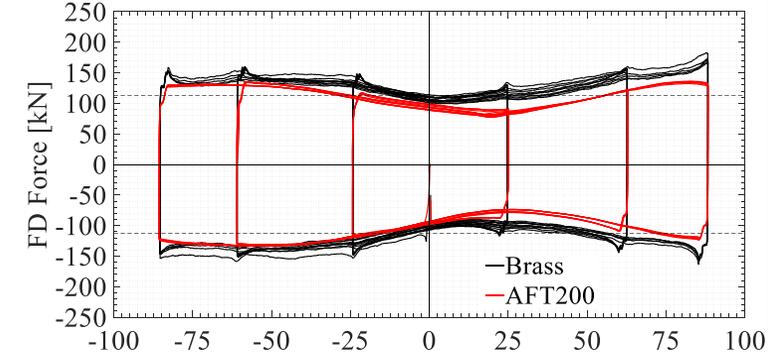
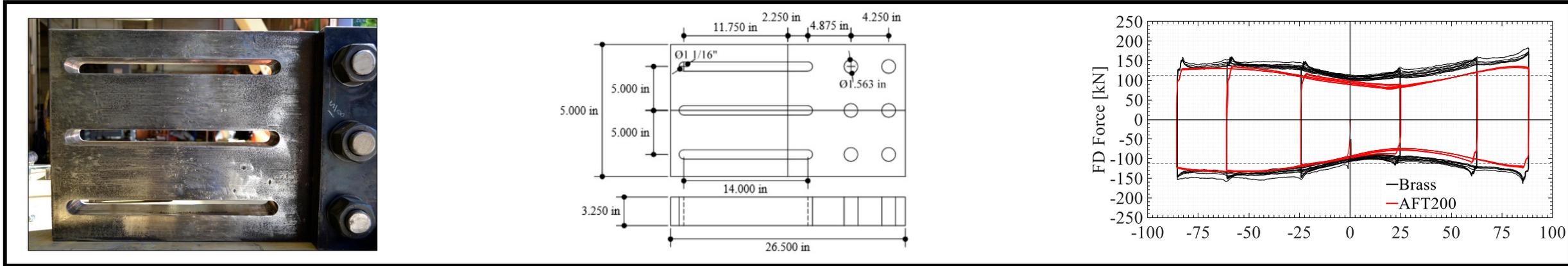


Why friction-based force-limiting connections?

- Structural engineers have freedom in detailing
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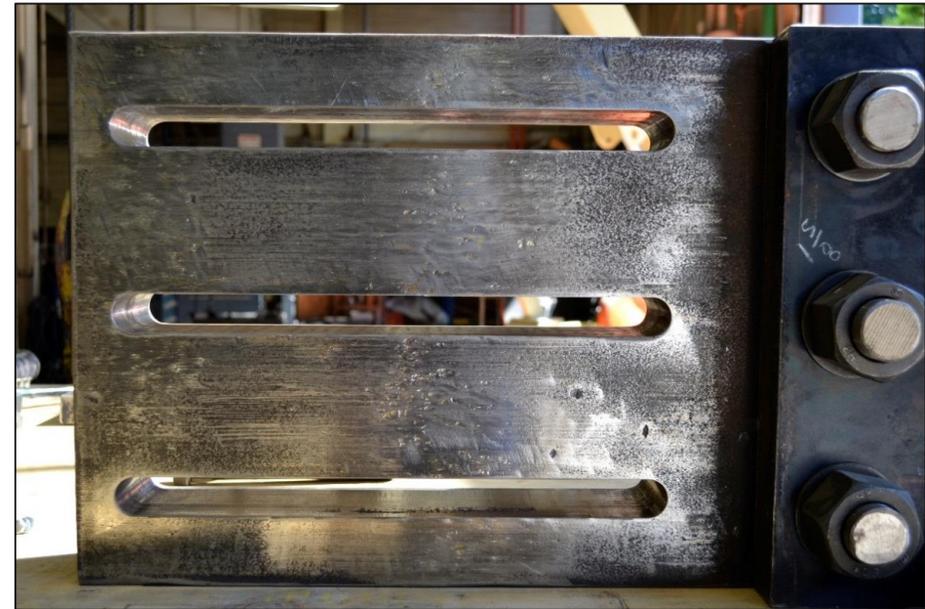


*Manufacturing requirements depend on the design



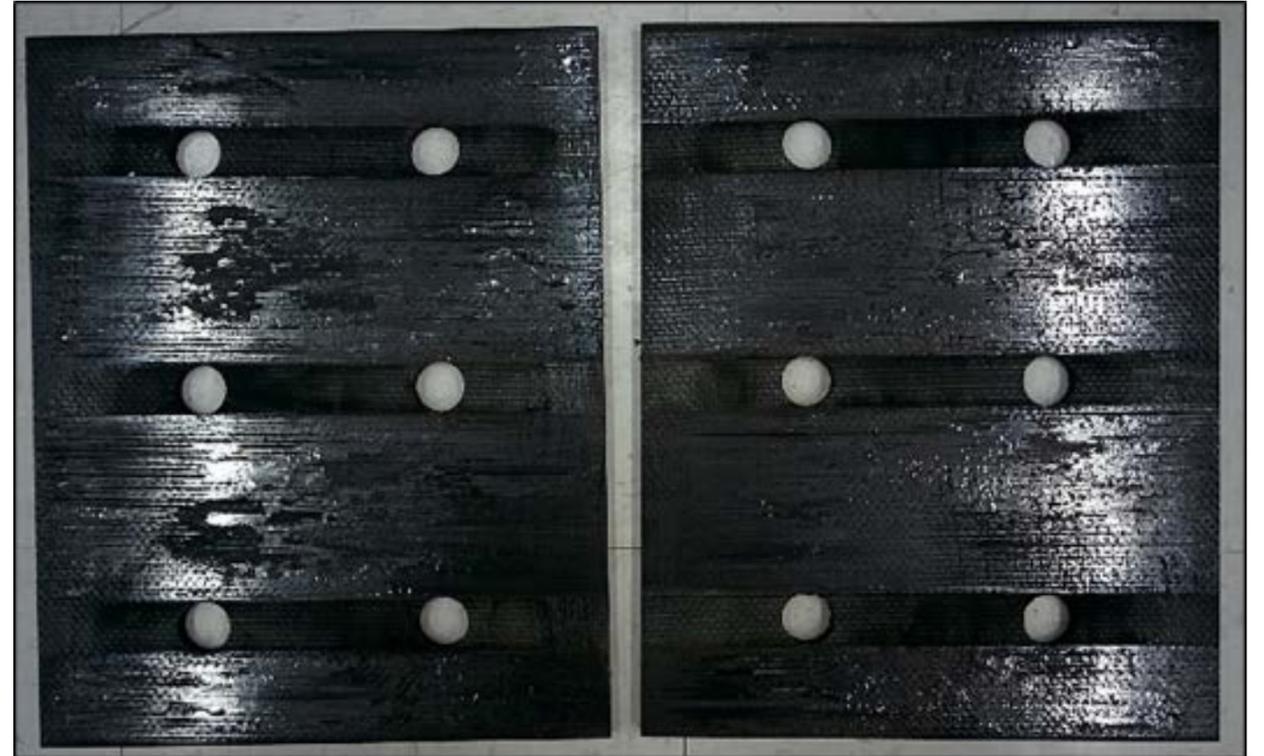
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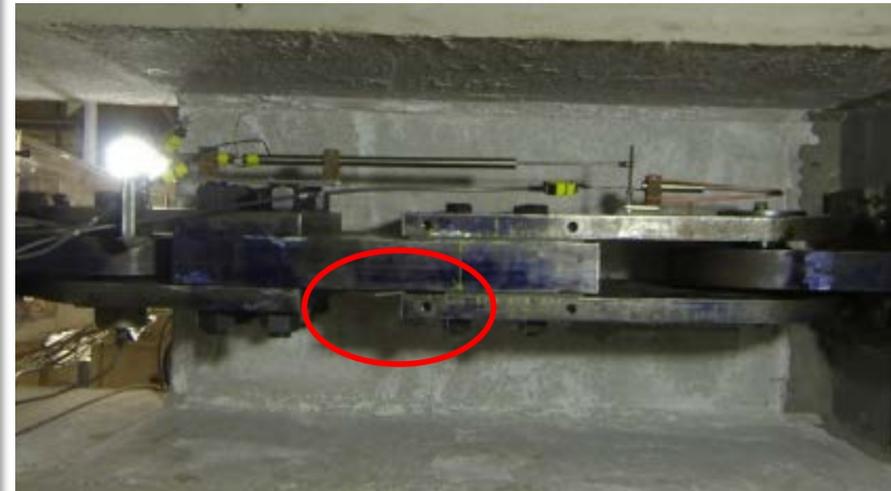


*Depends on design



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- **Some designs are damage tolerant**



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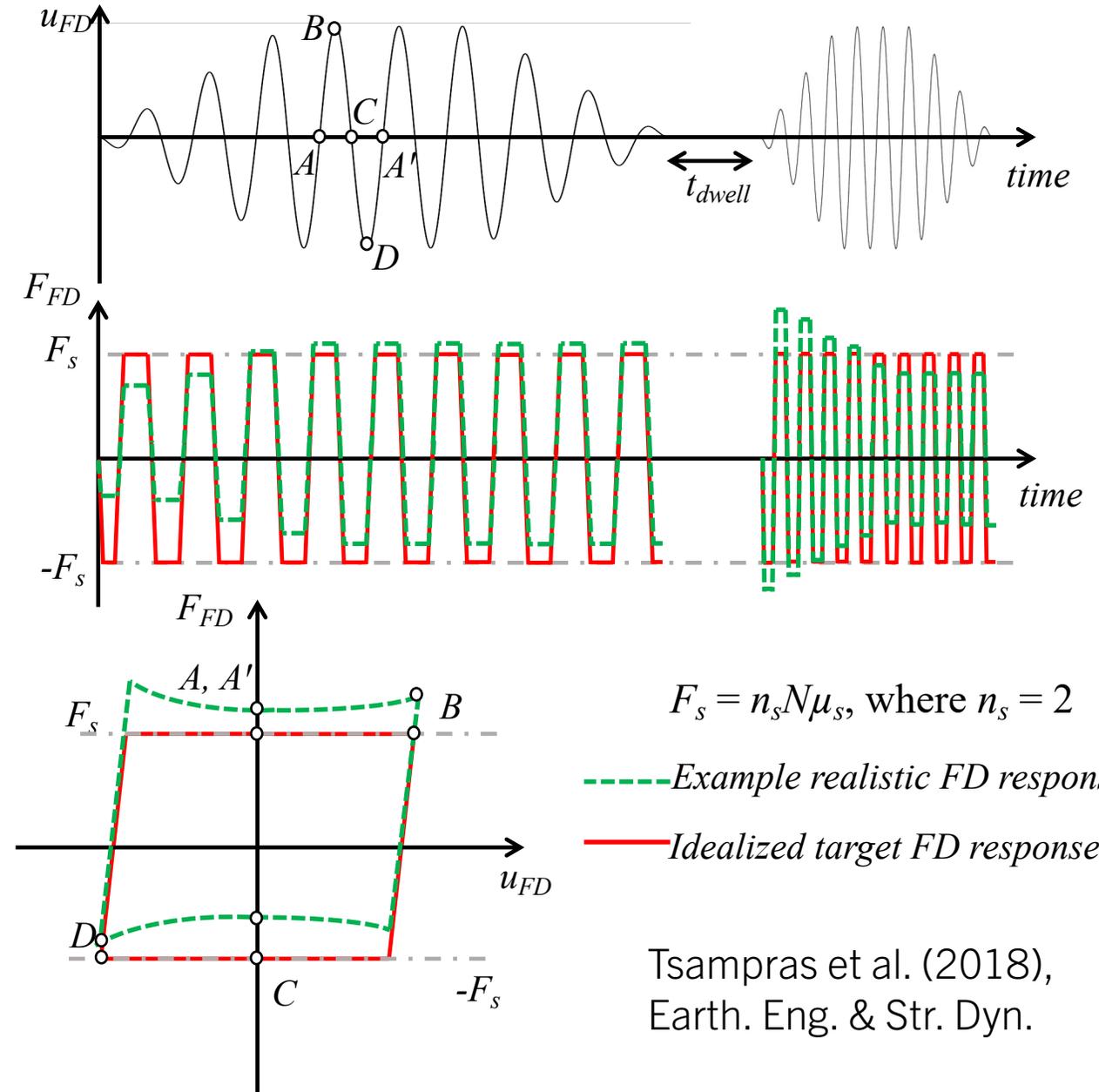
Challenges



Challenges with friction-based structural connections

Friction-sliding behavior is affected by:

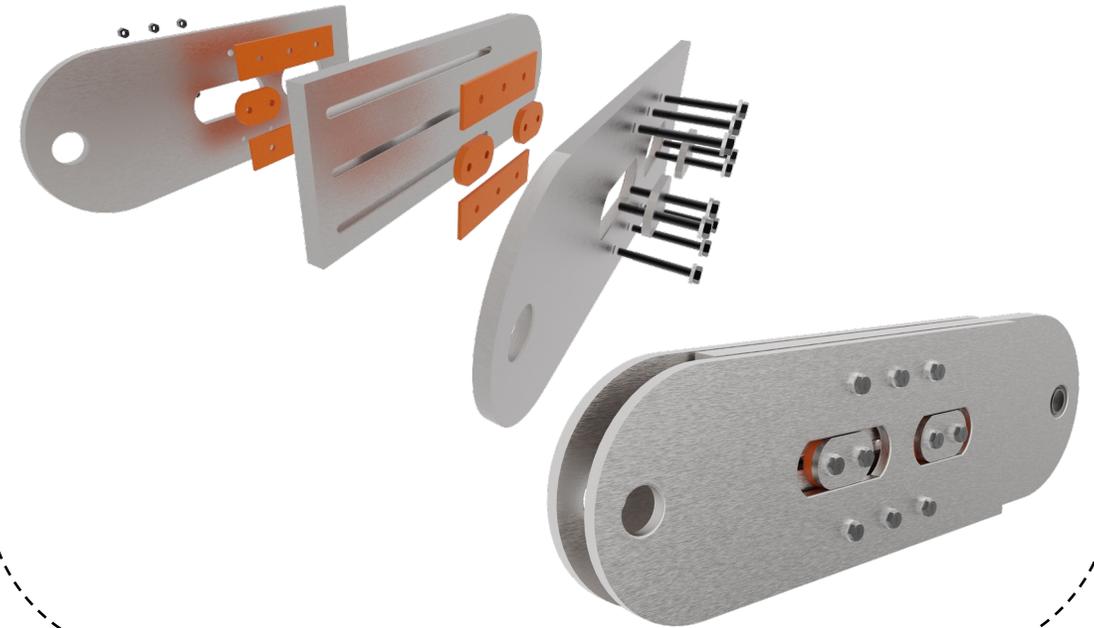
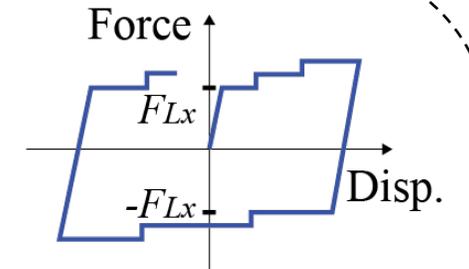
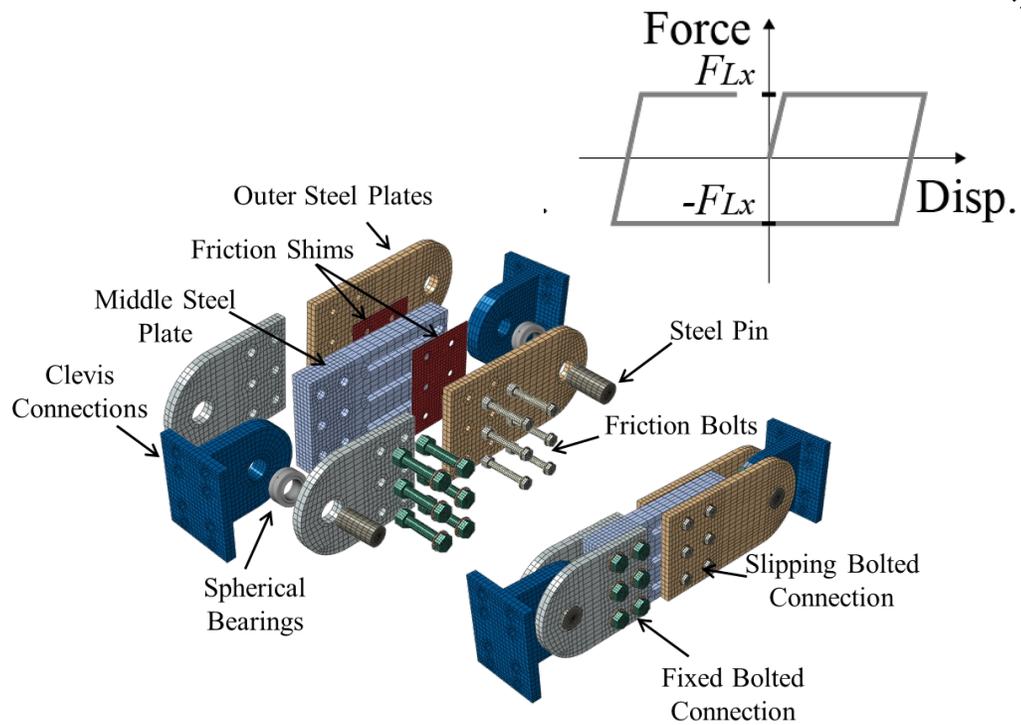
- Sliding velocity
- Dwell time
- Galvanic corrosion in bimetallic friction interface
- Creep of composite materials
- Break-in and cumulative sliding effects
- Effect of machining and geometric tolerances
- The effectively zero post-elastic stiffness can be both an advantage and disadvantage



MODIFIED FRICTION DEVICE

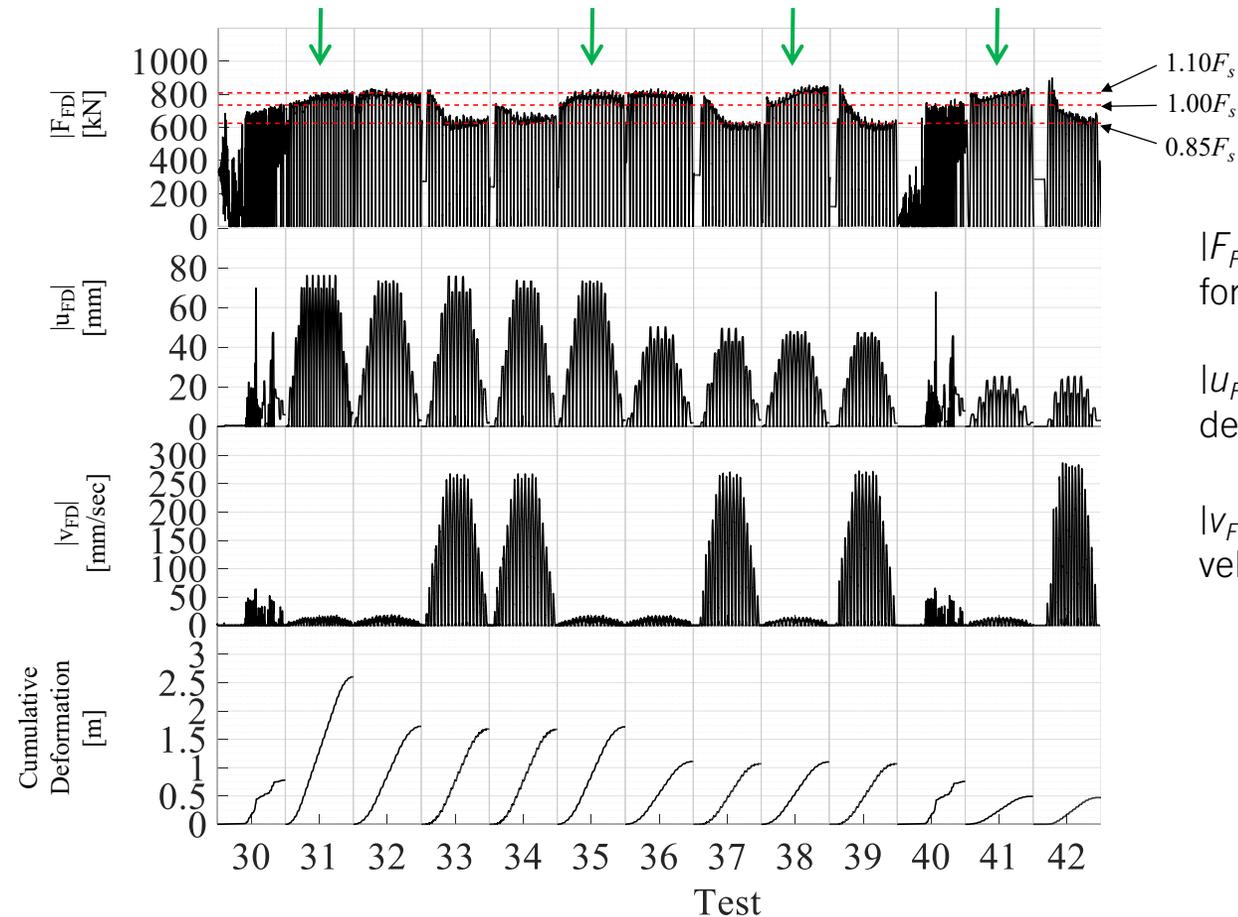
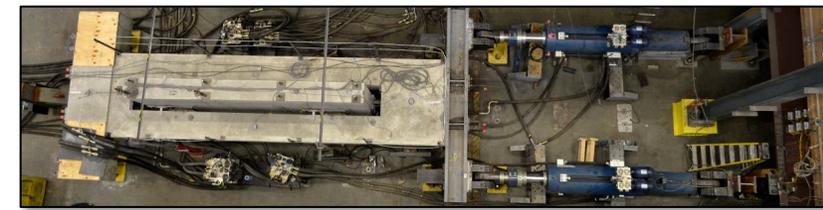
Tsampras et al. 2014, 2018

Modified friction device



Sliding History: Low velocity effect

$|F_{FDs}|$ in quasi-static tests that follow dynamic tests or earthquake tests increases to approximately $1.10F_s$



$|F_{FD}|$ is the absolute FD force

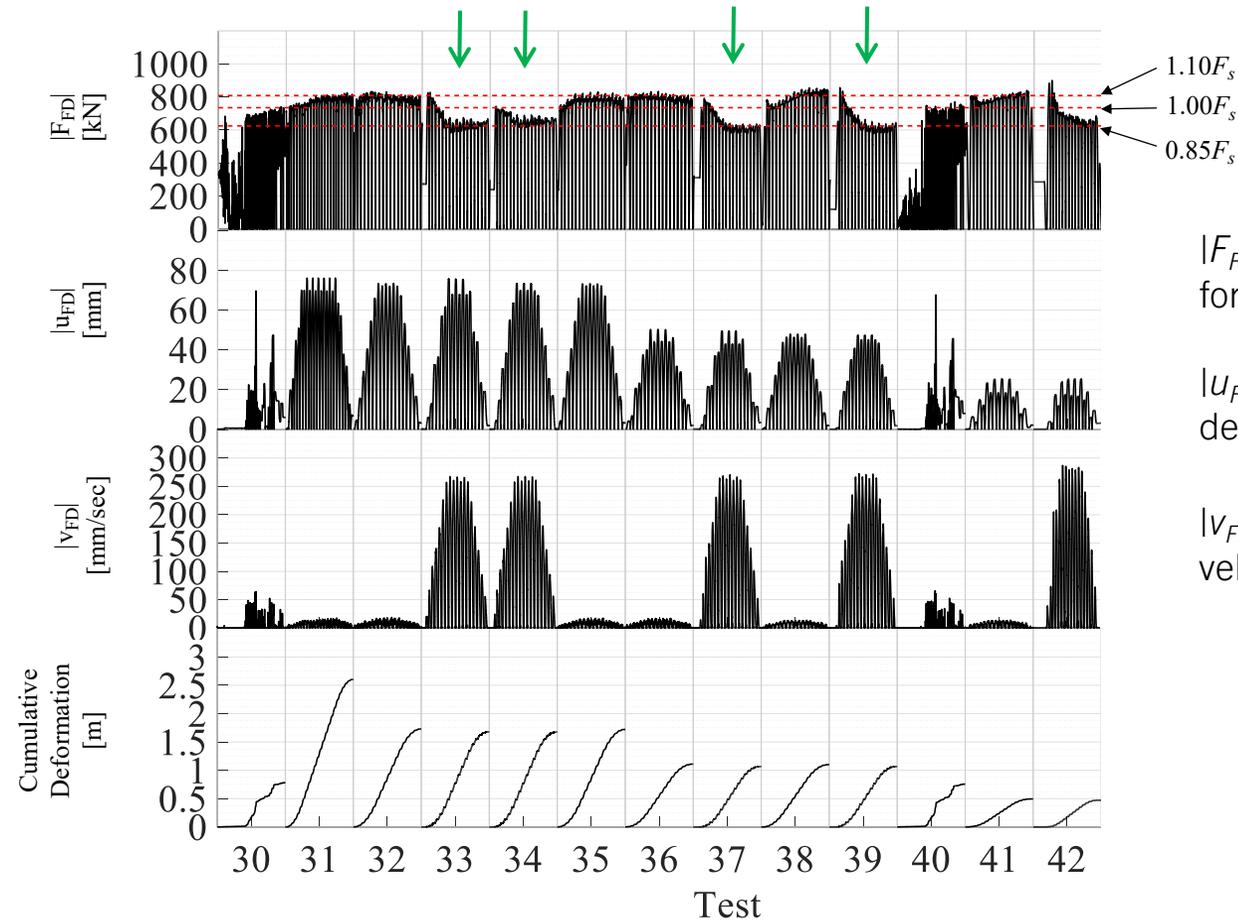
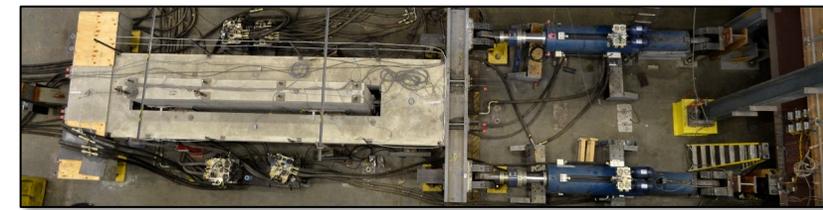
$|u_{FD}|$ is the absolute FD deformation

$|v_{FD}|$ is the absolute FD velocity



Sliding History: High velocity effect

$|F_{FDs}|$ in dynamic tests decreases to approximately $0.85F_s$



$|F_{FD}|$ is the absolute FD force

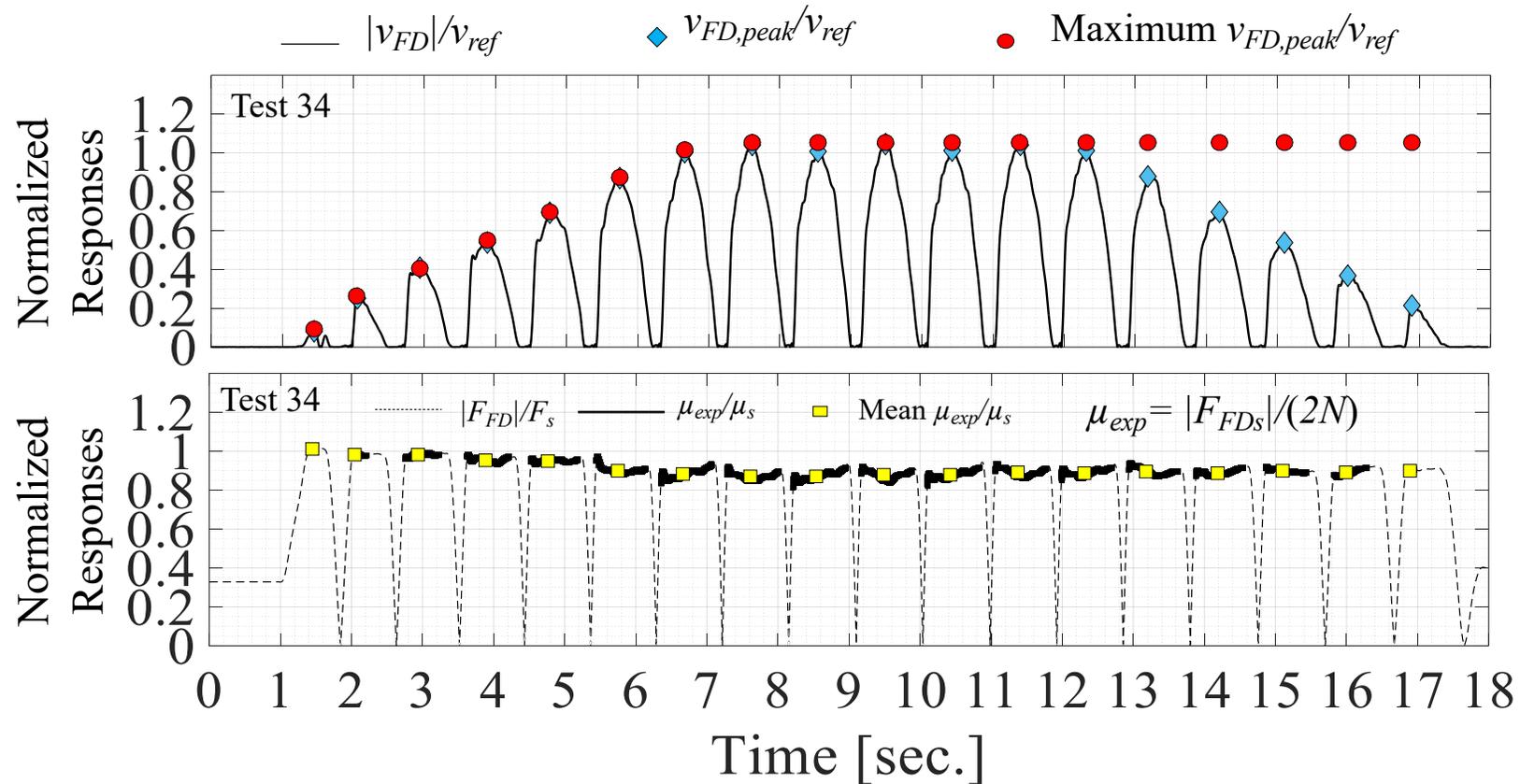
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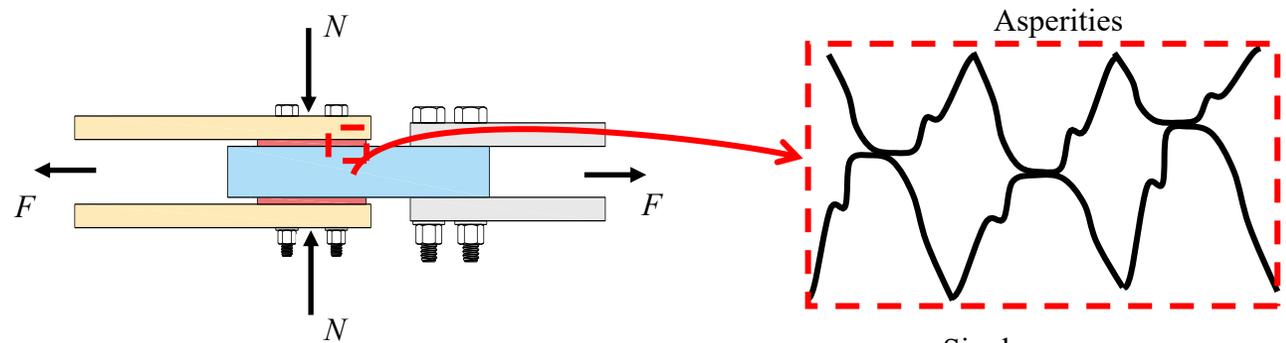


Sliding History: High velocity effect (Cont'd)

- (1) μ_{exp} does not depend on the instantaneous v_{FD}
- (2) μ_{exp} decreases as the maximum $v_{FD,peak}$ increases



Evolution of friction interface with respect to sliding velocity

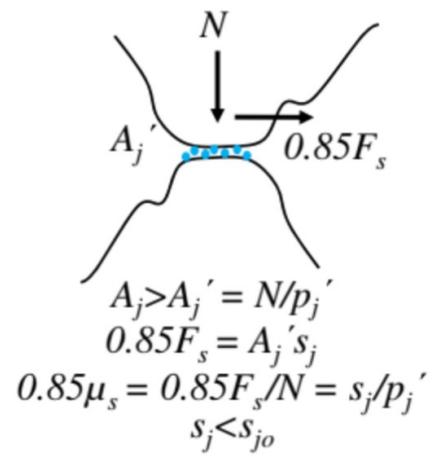
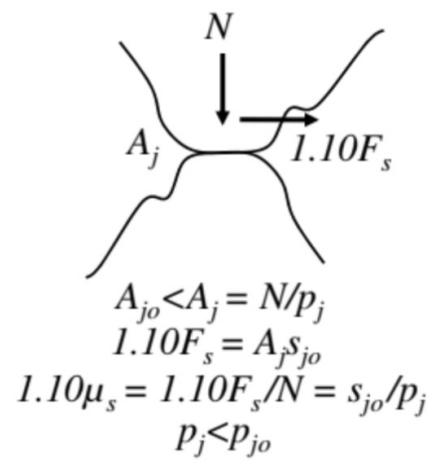
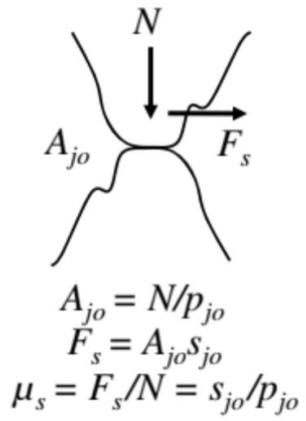


Single Junction

Single Junction
Small Sliding Velocity

Single Junction
Large Sliding Velocity

A_j : true contact area
 N : total normal force at friction interface
 p_j : normal pressure
 s_j : interface shear stress (strength)
 μ_s : friction coefficient



- D. Tabor, "Friction - The present state of our understanding," Journal of Lubrication Technology, vol. 103, pp. 169-179, 1981
 - Tsampras G., Sause R., Fleischman R. B., Restrepo J. I., Experimental study of deformable connection consisting of friction device and rubber bearings to connect floor system to lateral force resisting system. Earthquake Engng Struct Dyn. 2018;47:1032-1053.
<https://doi.org/10.1002/eqe.3004>

Research to address material-level challenges

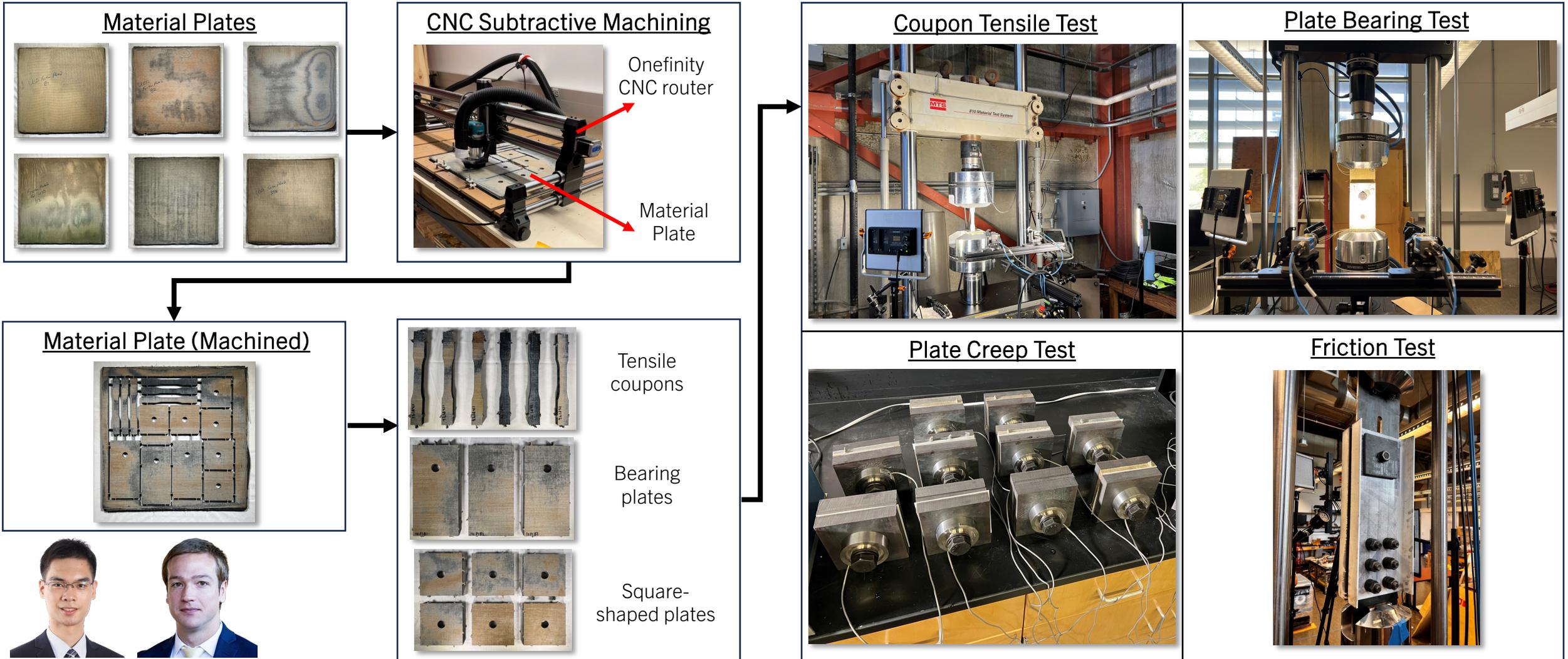
Challenges with friction-based structural connections

Friction-sliding behavior is affected by:

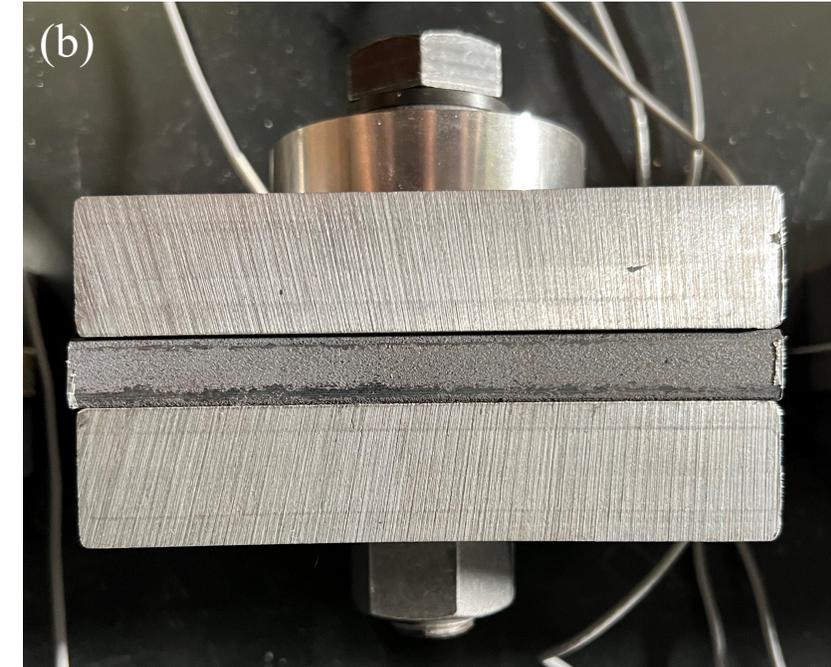
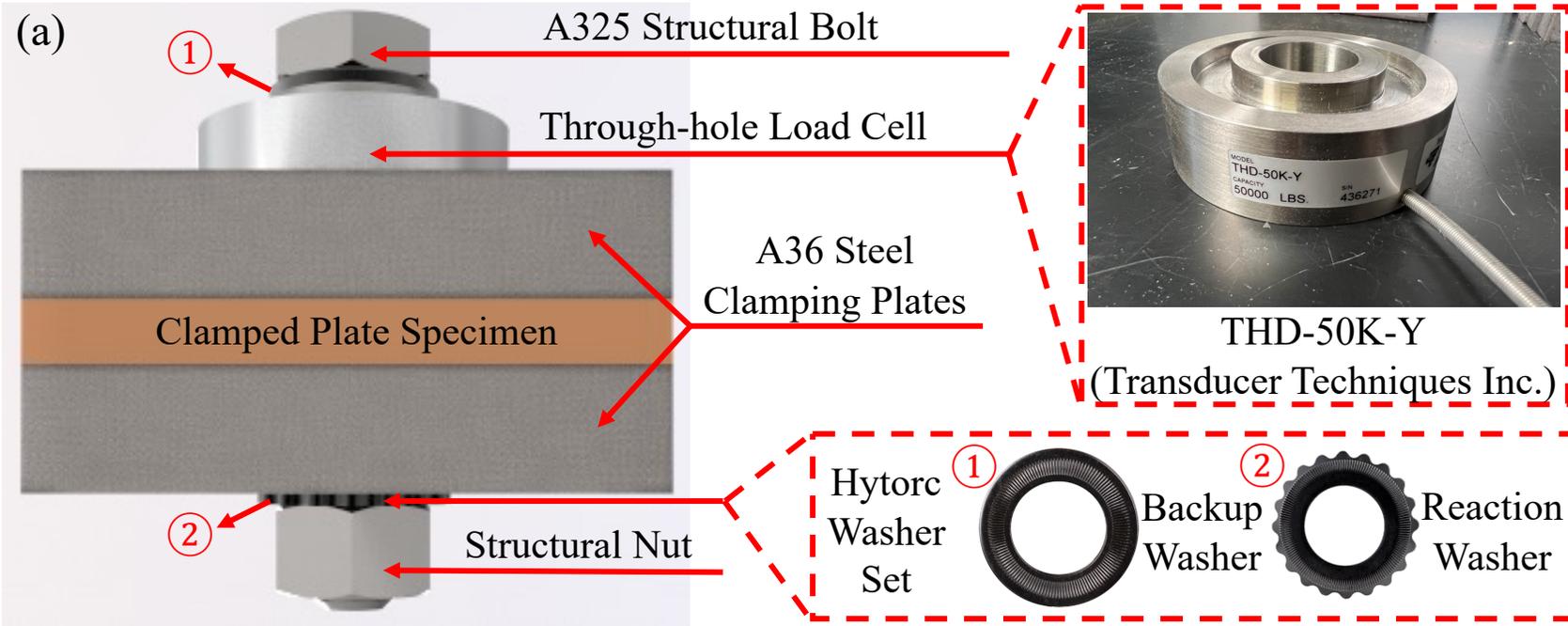
- Sliding velocity
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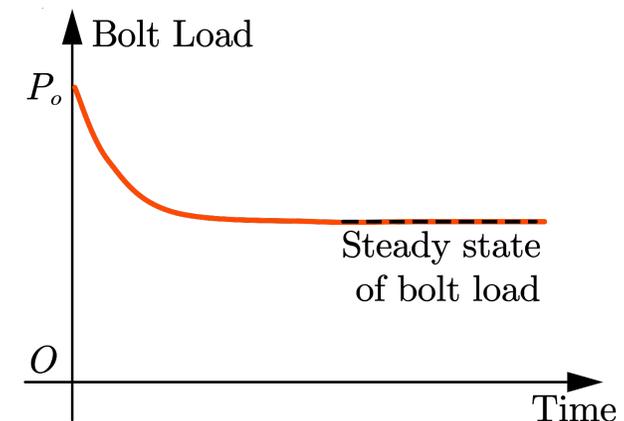
Experimental characterization of composite materials in friction interfaces for structural applications



Material-level Study: Bolt Relaxation Test

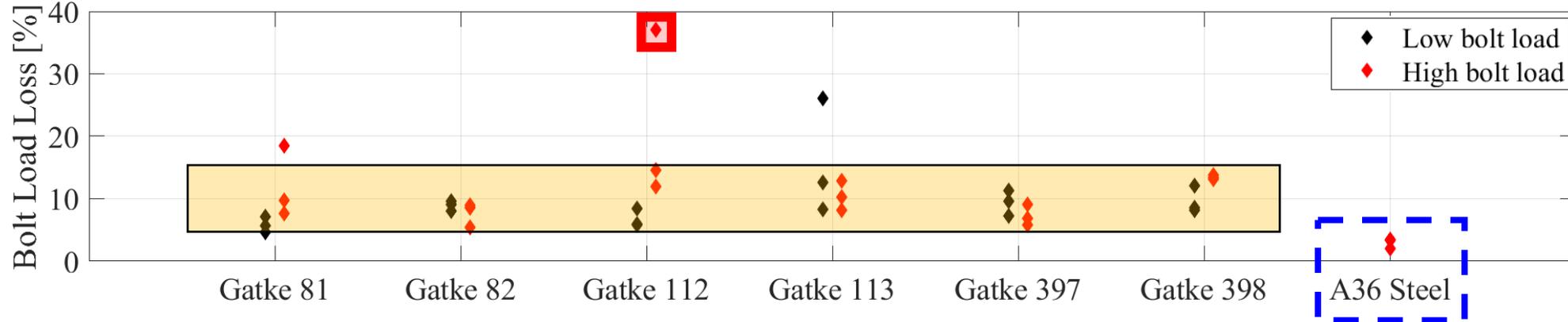
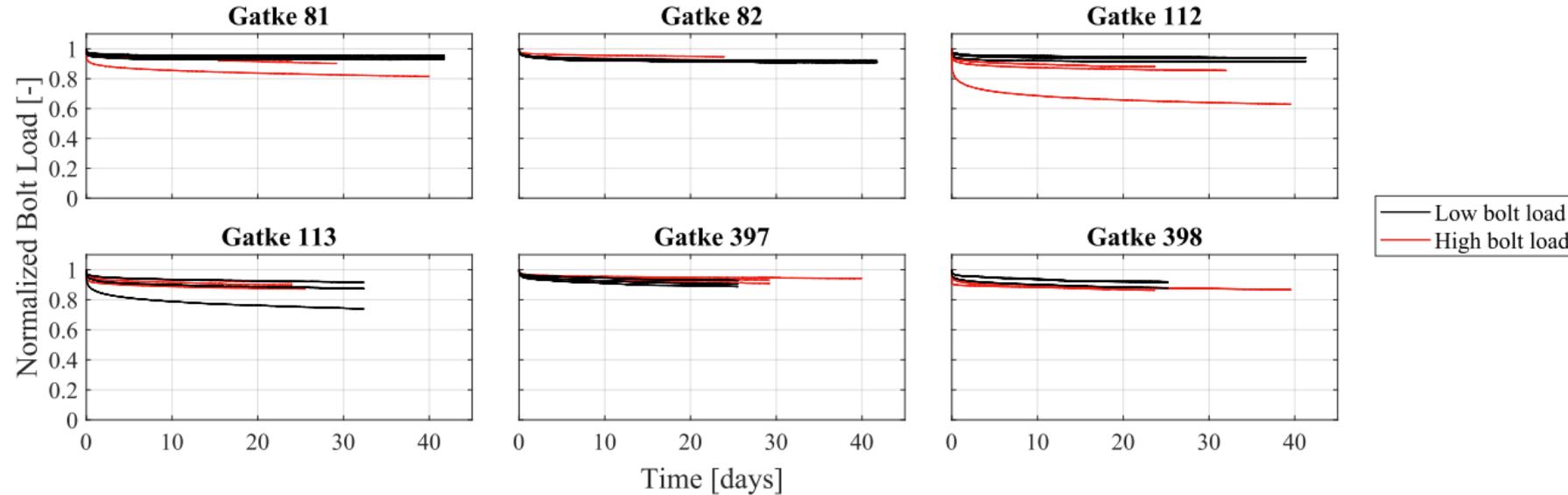


- **Two target bolt load levels** were considered
 - High bolt load (173.5 kN = 39 kips): minimum pretension of 7/8" ASTM A325 structural bolt
 - Nominal normal pressure = 11 MPa
 - Low bolt load (57.8 kN = 13 kips): 1/3 of high bolt load
 - Nominal normal pressure = 3.7 Mpa
- For each material under each load level, **three specimens** were tested
- Three specimens of **A36 steel plates** were tested, as a **baseline test case**
- Bolt load was recorded until a **steady state** of bolt load was observed
 - In this test, defined as when the bolt load loss rate was lower than or equal to -5×10^{-6} kN/sec



Schematic representation of the bolt load time history

Material-level Study: Bolt Relaxation Test Results

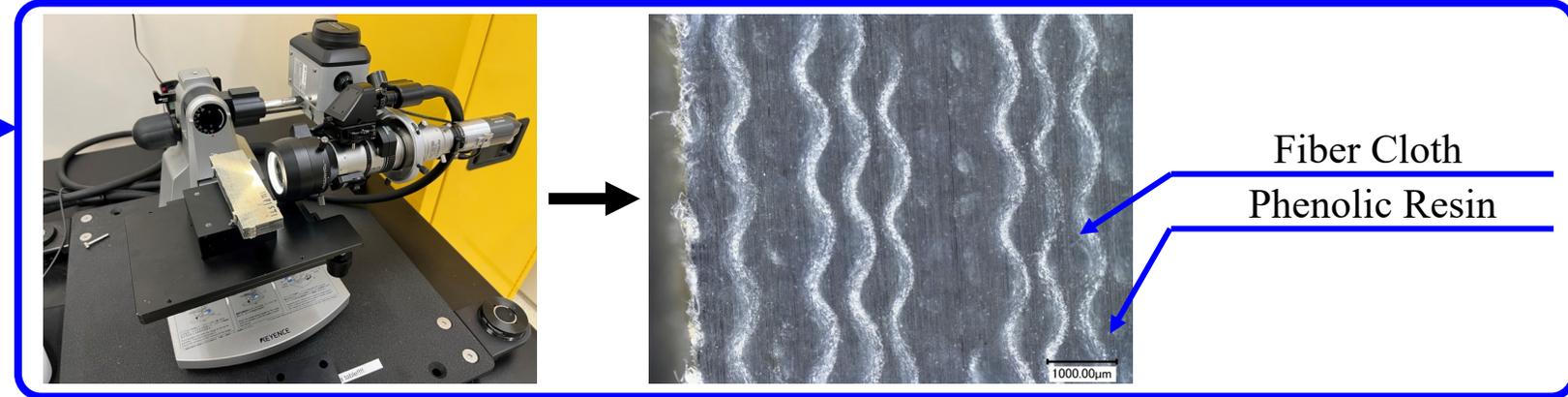
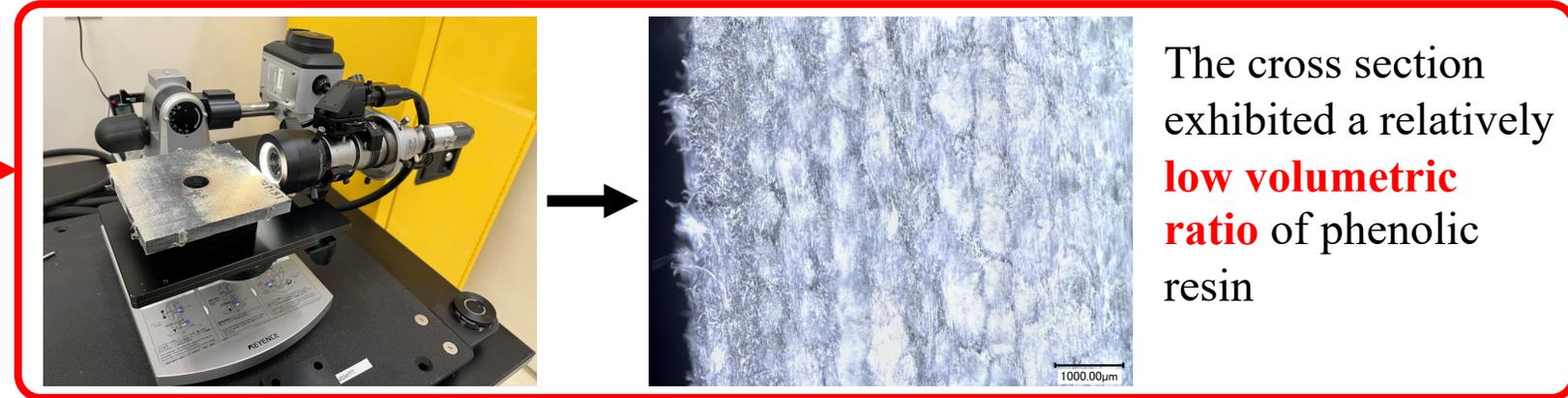
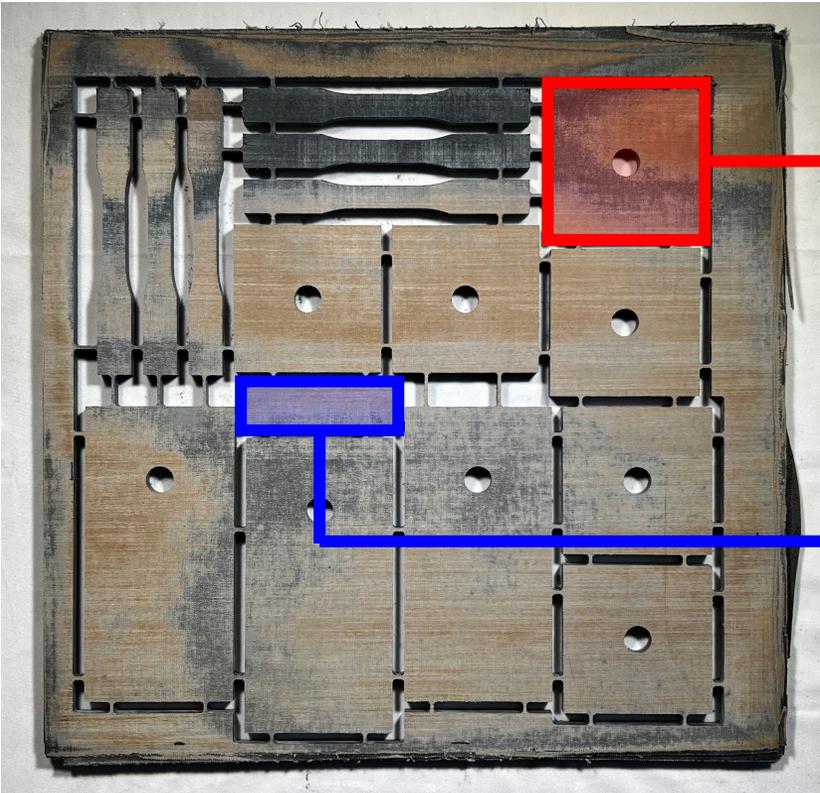


- Observation 1: As expected, the reference test group with **A36 steel** exhibited **least percentage of bolt load loss**
- Observation 2: For all the composite materials, the percentage of bolt load loss ranged **approximately from 5 to 15%**
- Observation 3: The correlation between material constituents and the percentage of bolt load loss was **insignificant**
- Observation 4: One specimen of Gatke 112 exhibited a **37.12%** bolt load loss
 - Deemed to be **excessive** and required **further investigation**

Material-level Study: Bolt Relaxation Test Results



- **Microscopy** study of the Gatke 112 specimen with a 37.12% bolt load loss

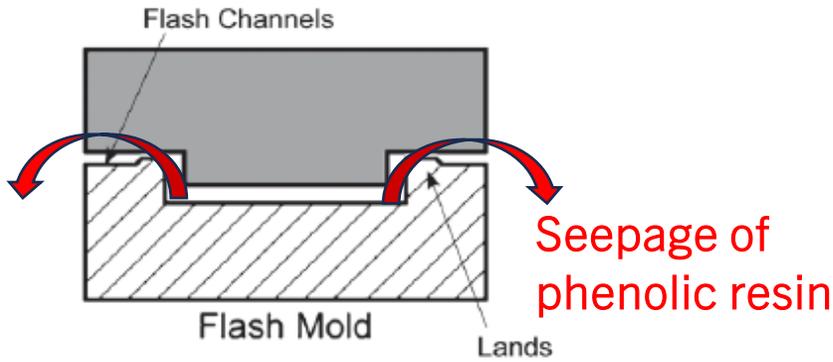


- Gatke 112 plate inducing a 37.12% bolt load loss exhibited **a relatively low volumetric ratio of phenolic resin**

Material-level Study: Bolt Relaxation Test Results

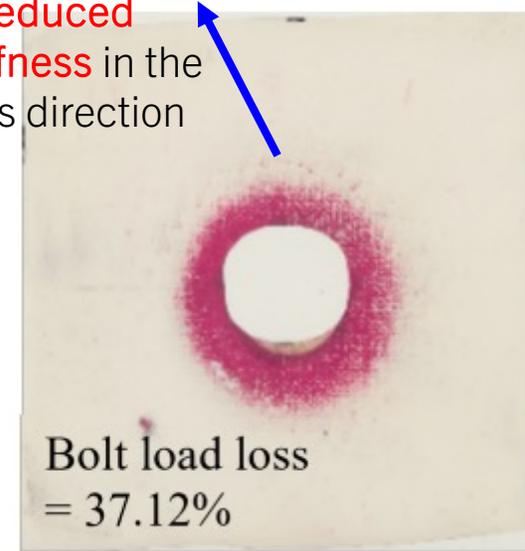


- The relatively low volumetric ratio of phenolic resin was attributed to the **flash compression molding manufacturing process**

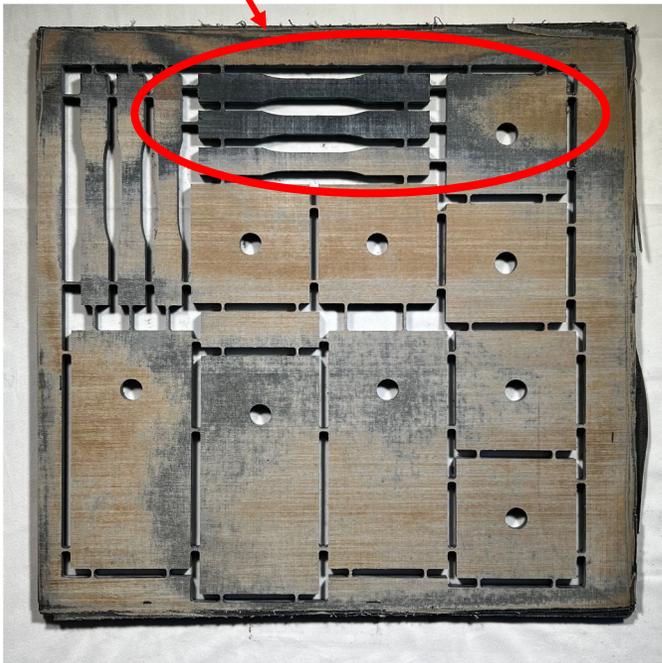


Resin-poor region

Concentrated normal pressure due to **reduced compressive stiffness** in the through-thickness direction

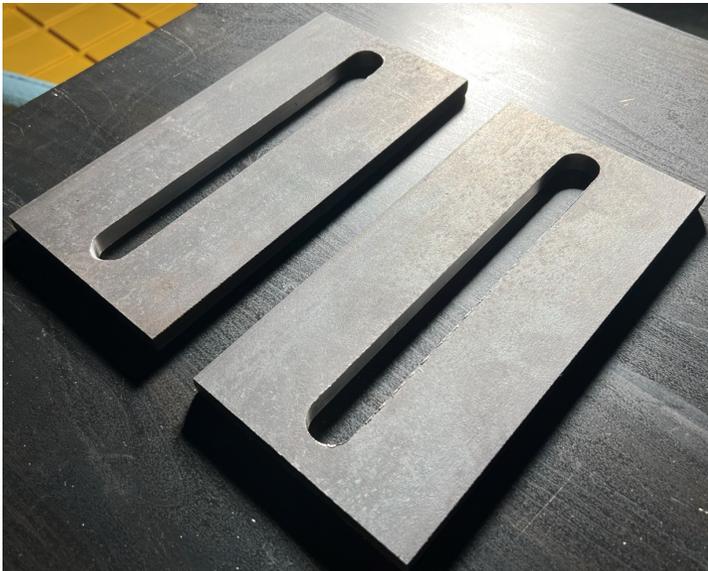
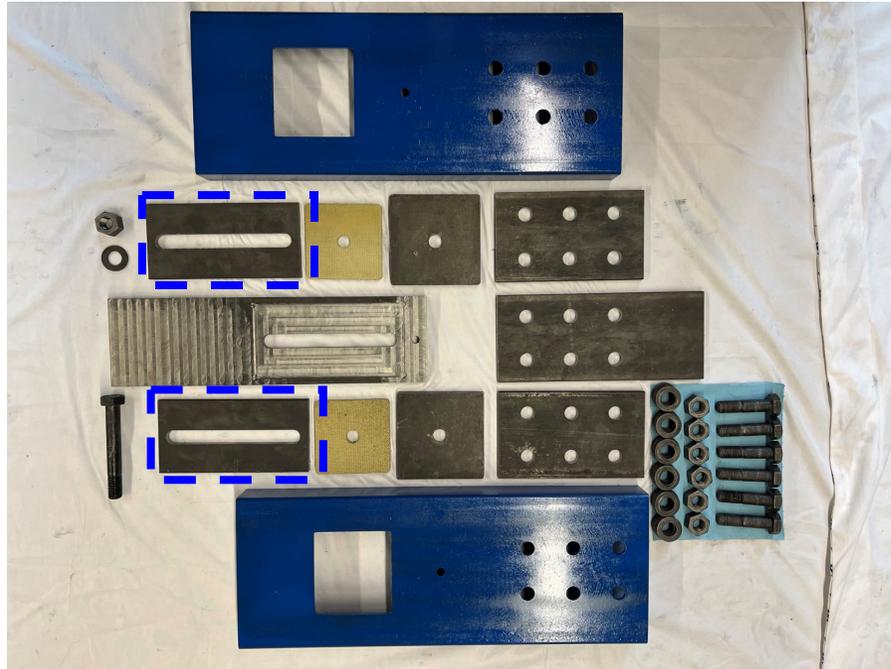


Selected pressure recording film results of Gatke 112 specimens



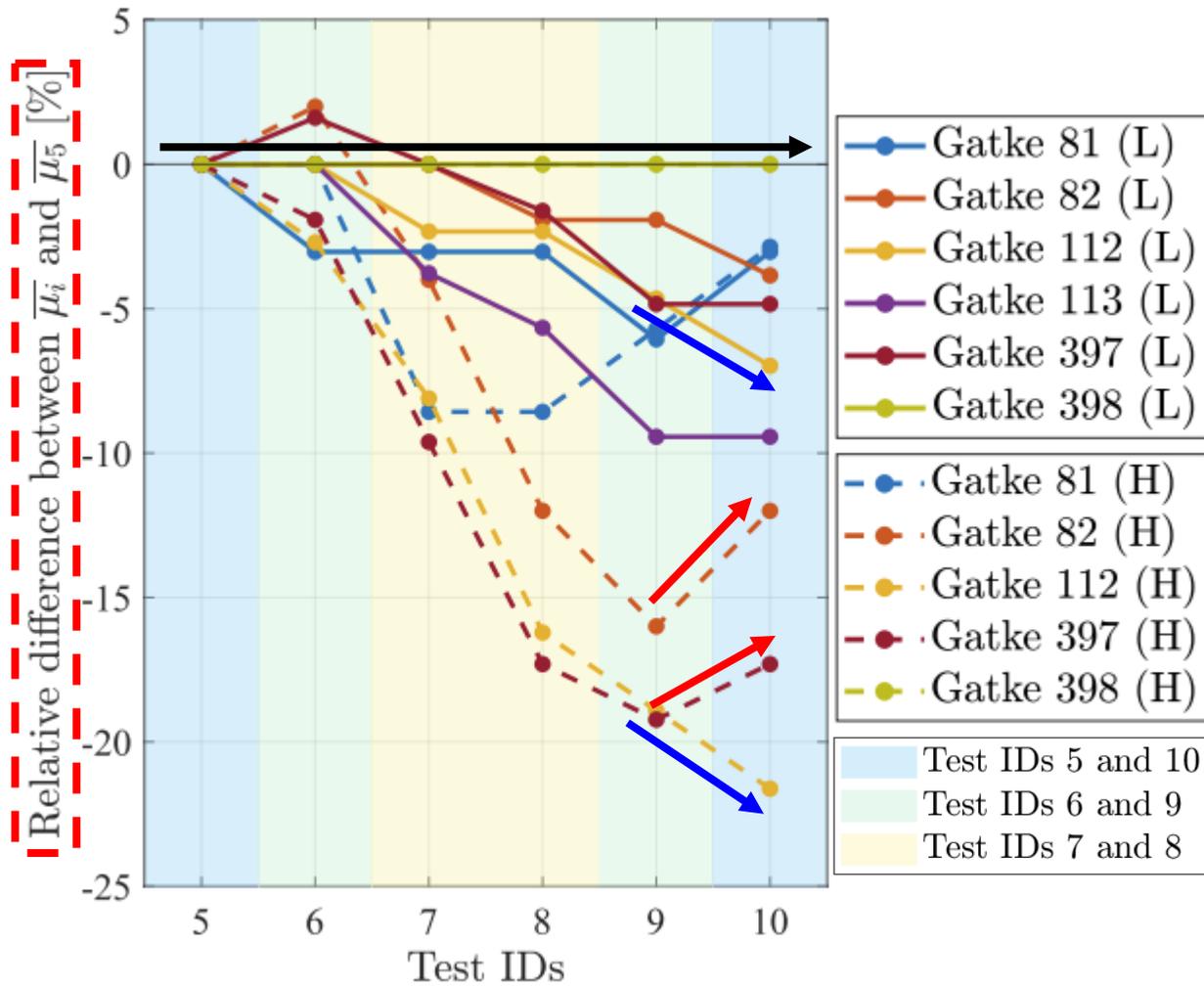
The results of the bolt relaxation test highlighted the **importance of quality control in the manufacturing process** of composite friction materials for friction-based structural components.

Material-level Study: Friction Test



- A **slotted-bolted** friction-based component was designed for the friction test
- The friction interface was established between **composite friction materials** and **A36 steel (low-carbon structural steel)**
 - The surface of the A36 steel sliding plates was **not** specially treated
- **Two normal load levels** were considered, i.e., 39 kips and 13 kips
 - Exception for Gatke 397 under higher normal load case: a reduced normal load of 31 kips was applied (to prevent the friction force from exceeding the testing machine's capacity)
- Data collection
 - Connection force
 - Connection displacement
 - Bolt load

Test IDs 5~10
Velocity effect
assessment



- Composite materials that consist of phenolic resin, glass fibers, graphite, Teflon and molybdenum disulfide MoS_2 are among the most suitable materials for use in friction-based structural components for earthquake structural engineering applications.

Challenges with friction-based structural connections

Friction-sliding behavior is affected by:

- Sliding velocity
- Dwell time
- Galvanic corrosion in bimetallic friction interface
- Creep of composite materials
- Break-in and cumulative sliding effects
- Effect of machining and geometric tolerances
- The effectively zero post-elastic stiffness can be both an advantage and disadvantage



NOTES:

(1) Draft drawings for the 40 kN friction connections used in the NCREE Shake Table test, December 2023

(2) Concept of "loose plates" was implemented to limit the effect of the bolted end connections shared with the buckling-restrained braces.

(3) Load cells allow for control of normal force. Composite friction pads allow for reduced axial compressive stiffness. Assume no use of Spring Washers.

$$F_{slip} = \mu \times N \times n_b \times n_s = 0.4 \times 50 \text{ kN} \times 1 \times 2 = 40 \text{ kN}$$

where

- μ is the friction coefficient in the interface between structural steel clean of mill scale (no special surface finish) and the composite friction pad
- N is the normal force due to the bolt preload
- n_b is the number of bolts in the friction interface
- n_s is the number of friction interfaces

For past research on the composite friction pads see:

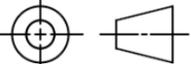
- Georgios Tsampras, Richard Sause, Robert B. Fleischman, José I. Restrepo (2017) Experimental study of deformable connection consisting of friction device and rubber bearings to connect floor system to lateral force resisting system, Earthquake Engineering & Structural Dynamics, 47 (4), 1032-1053, doi: 10.1002/eqe.3004

- Georgios Tsampras, Richard Sause (2014), Full-scale, components test of Inertial Force-Limiting Floor Anchorage Systems for Seismic Resistant Building Structures using a Buckling Restrained Brace and Steel Reinforced Low Damping Rubber Bearings, DesignSafe-CI, 10.4231/D3N87311M <https://www.designsafe-ci.org/data/browser/public/nees.public/NEES-2011-1083.0ups/Experiment-2>

Approximate mass = 85 kg
Including bolts and load cell, excluding end connections and steel beam

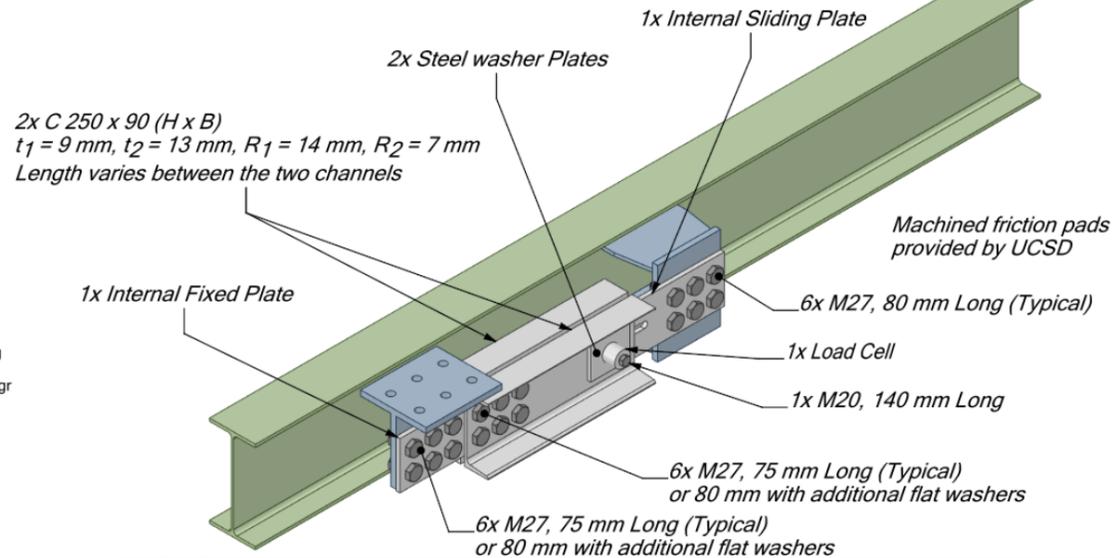
Approximate eccentricity = 17.5 mm

Units: mm

THIRD ANGLE PROJECTION	CONTRACT NO.		MATERIAL
			FINISH
	NEXT ASSY		TREATMENT
	USED ON	SIMILAR TO	
APPLICATION			

REVISION HISTORY

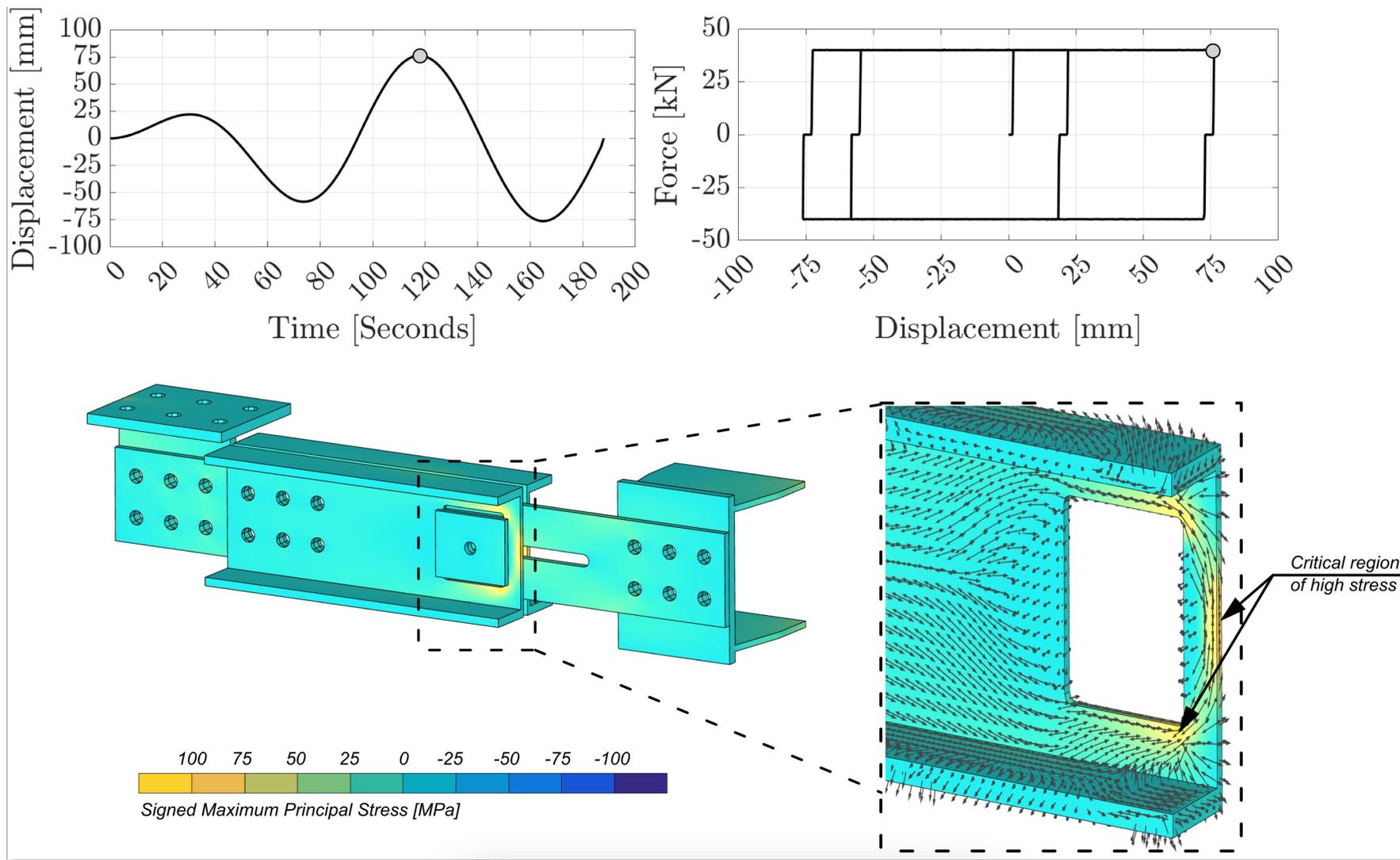
REV	DESCRIPTION	INCORP BY	DATE	CHECKED
A	Initial drawing		28 Aug. 2023	NCREE, UTA, UCSD
B	Single bolt in friction interface		06 Sept. 2023	N/A
C	Eccentric, one-sided end connection, similar to HBRB Used channel steel section common in Taiwan Added parts for end connections and framing beam Added simple safety mechanism to prevent out of plane spread of channels (unlikely to happen due to small load & large channel section)		07 Sept. 2023	N/A
D	Modified the design to reduce the total weight by approx. 10kg		08 Sept. 2023	



QTY REQD		ITEM NO.	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	
-2	-1				
PARTS LIST					
INIT	APPROVALS	DATE	INIT	APPROVALS	DATE
					9/8/2023 10:26:23 AM
Georgios Tsampras					
TITLE					
Friction Device 40 kN					
SIZE	CAGE CODE	DWG NO.		UCSD001	REV
B					D
SCALE 1:12				SHEET 1 of 7	

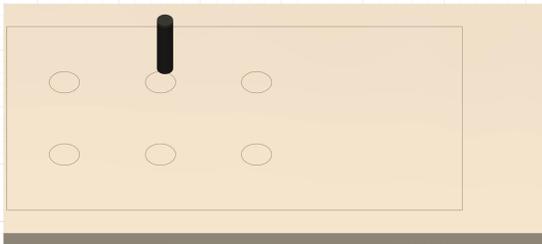


SIMULATIONS

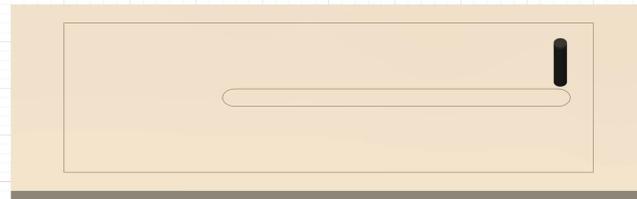


MANUFACTURING - PROGRAMMING

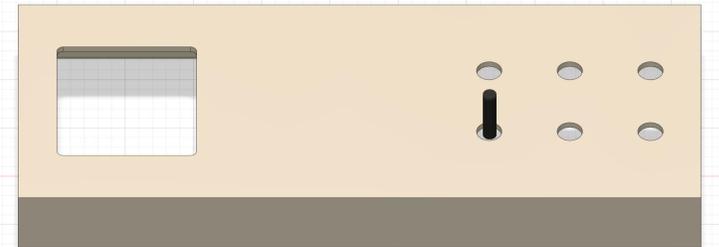
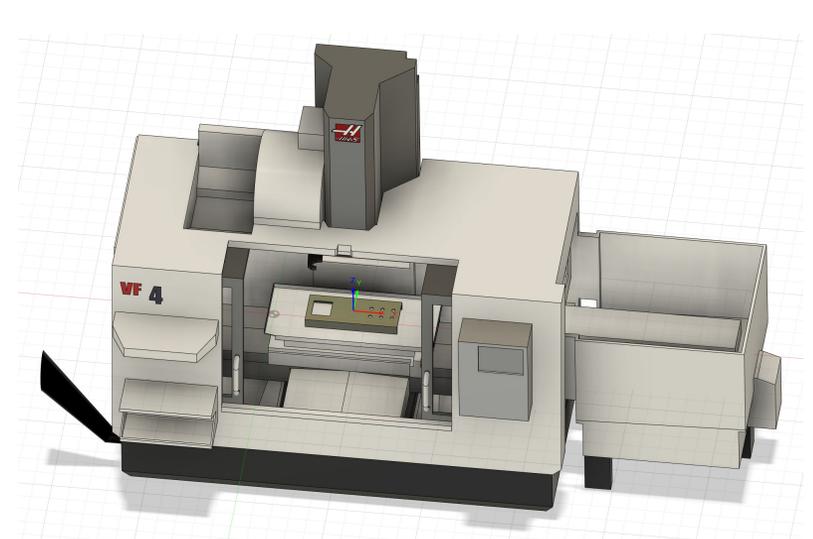
Internal fixed plate



Internal sliding plate



Channels



AUTOMATED MANUFACTURING



Automated Tooling Offsets



Workholding Setup



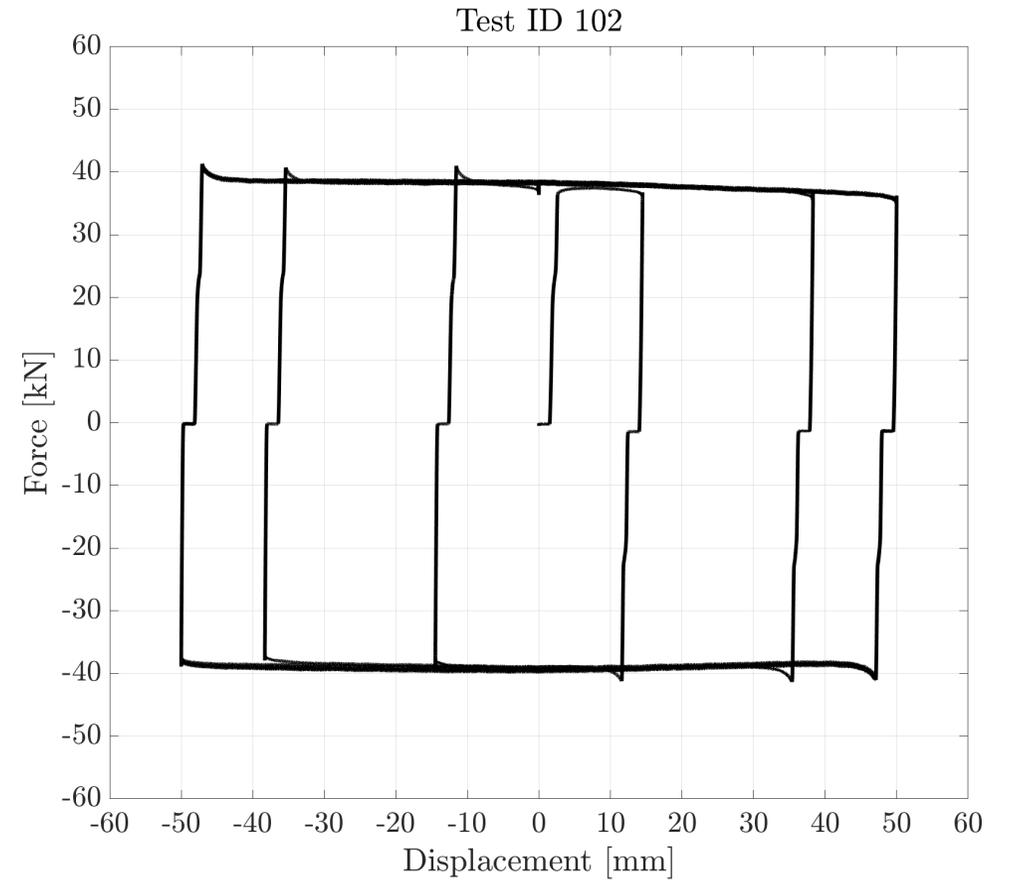
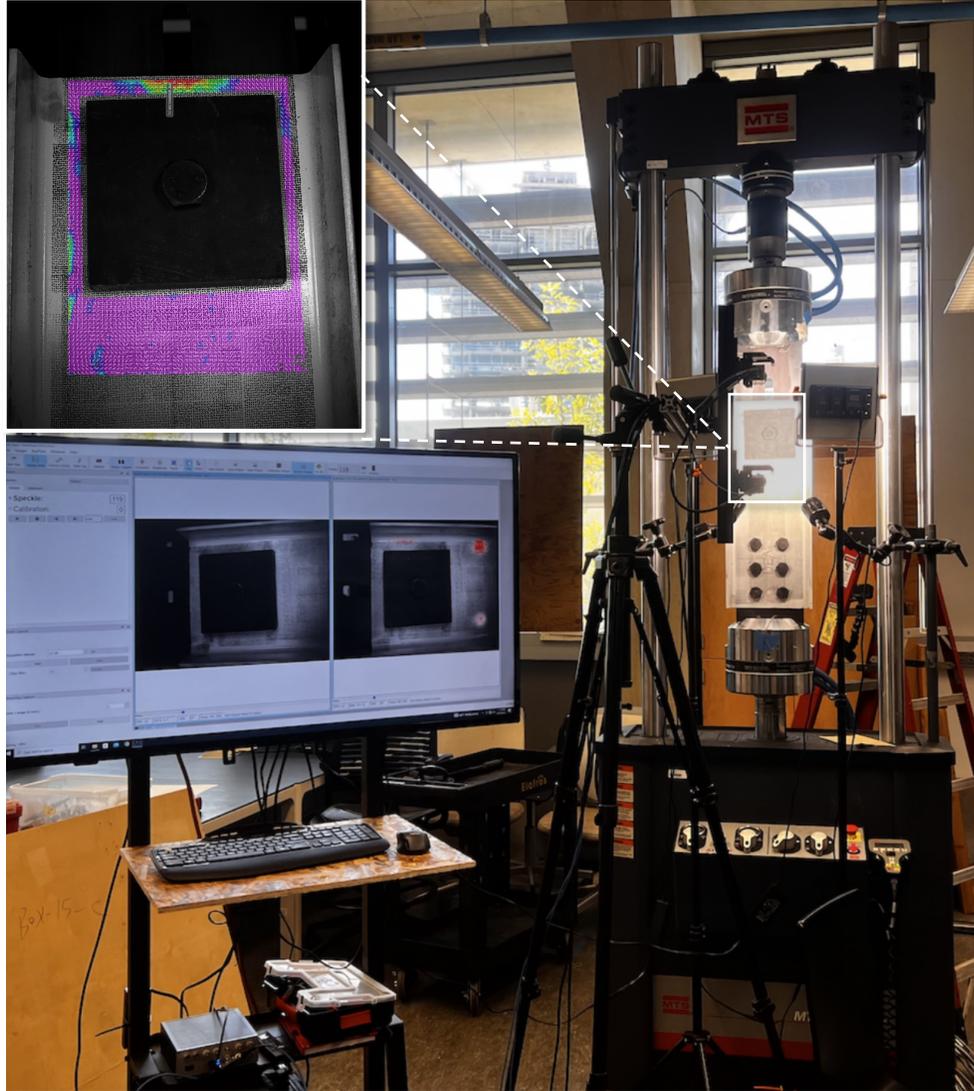
Wireless Probing



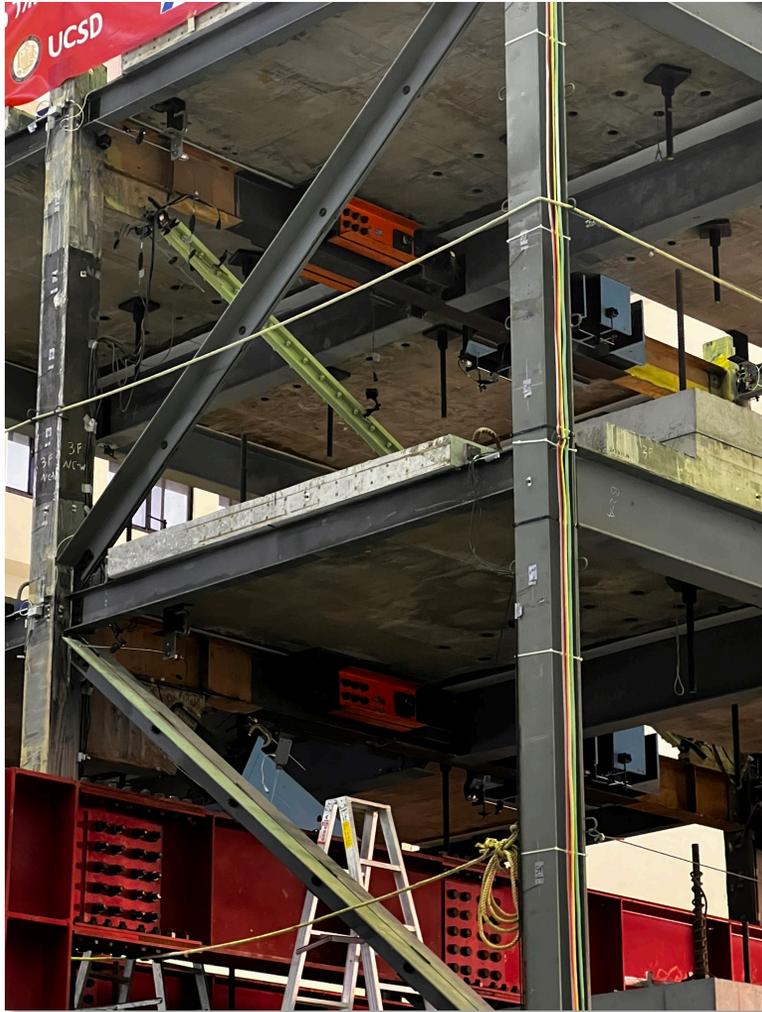
Computer Numerical Controlled Subtractive Manufacturing



COMPONENT LEVEL TESTING



2023 NCREE SHAKE TABLE TESTING



Demonstration of repairability – If needed



Relevant Publications, Open Data, and Patent

- Tsampras, Georgios; Sause, Richard, (2014), "Full-scale, components test of Inertial Force-Limiting Floor Anchorage Systems for Seismic Resistant Building Structures using a Friction Device and Carbon Fiber Reinforced Low Damping Rubber Bearings", DesignSafe-CI [publisher], doi: 10.4231/D3HH6C68B <https://www.designsafe-ci.org/data/browser/public/nees.public/NEES-2011-1083.groups/Experiment-3>
- Georgios Tsampras, Richard Sause, Dichuan Zhang, Robert B. Fleischman, José I. Restrepo, David Mar, Joseph Maffei (2016), Development of deformable connection for earthquake-resistant buildings to reduce floor accelerations and force responses, *Earthquake Engineering & Structural Dynamics*, 45 (9), 1473–1494, doi:10.1002/eqe.2718
- Georgios Tsampras, Richard Sause, Robert B. Fleischman, José I. Restrepo (2017) Experimental study of deformable connection consisting of friction device and rubber bearings to connect floor system to lateral force resisting system, *Earthquake Engineering & Structural Dynamics*, 47 (4), 1032-1053, doi: 10.1002/eqe.3004
- Zhi Zhang, Robert B. Fleischman, José I. Restrepo, Gabrielle Guerrini, Arpit Nema, Dichuan Zhang, Ulina Shakya, Georgios Tsampras, Richard Sause (2018), Shake table test performance of an inertial force-limiting floor anchorage system, *Earthquake Engineering & Structural Dynamics*, 47 (10), 1987-2011, doi: 10.1002/eqe.3047
- Chen, K., G. Tsampras, and K. Lee. 2023. "Structural connection with predetermined discrete variable friction forces." *Resilient Cities and Structures, Resilience of Structures to Earthquakes*, 2 (1): 1–17. <https://doi.org/10.1016/j.rcns.2023.02.006>.
- Kyoungyeon Lee; Georgios Tsampras; C. Franco Mayorga (Forthcoming), "Reinforced Concrete Core Wall Buildings with Modified Friction-Based Force-Limiting Connections: Connection Design Considerations and Three-Dimensional Response to Bidirectional Ground Motions " *Journal of Structural Engineering*, DOI: 10.1061/JSENDH/STENG-13609
- Chung-Che Chou, Huang-Zuo Lin, Alvaro Córdova, Jian-Ming Chen, Daniel Yen-Hsun Chou, Shu-Hsien Chao, Shih-Ho Chao, Georgios Tsampras, Chia-Ming Uang, Hsin-Yang Chung, Chin-Hsiung Loh, Hsuan-Teh Hu, "[Earthquake simulator testing of a three-story steel building for evaluating built-up box column performance and effect of sliding slab](https://doi.org/10.1002/eqe.4130)". *Earthquake Engng Struct Dyn.* 2024; 1-19. <https://doi.org/10.1002/eqe.4130>
- Georgios Tsampras, Kaixin Chen, Dominic Tran, Anne-Sophie Roobol (2024) Friction-based connections: materials, designs, manufacturing, simulations, and experiments, 18th World Conference on Earthquake Engineering, Milan, Italy
- Alvaro Córdova, Chung-Che Chou, Chi-Jeng Wu, Georgios Tsampras, Chia-Ming Uang, Shih-Ho Chao (2025), Modeling and Response of a Three-Story Steel Building with Sliding Slabs in Earthquake Motions, *Earthquake Engng Struct Dyn.*, <https://doi.org/10.1002/eqe.4300>
- Chen, K., Tsampras, G., Cheruvalath, S., & Thundathil, M., Experimental Characterization of Mechanical and Tribological Properties of Composite Materials for Friction-based Force-limiting Structural Components. *Composites Part B*, Accepted.
- Tsampras, G., Chen, K., Chou, C., Lin, H., Wu, C., Córdova, A., Uang, C., & Chao, S., Development, design considerations, and experimental characterization of a low-cost friction-based force-limiting structural connection with reduced sensitivity to machining tolerances and accelerated repairability. In Preparation
- Tsampras, Georgios, and Chen Kaixin. "Friction devices for energy dissipation." U.S. Patent Application No. 18/508,087.

