New Near-Fault Adjustment Factors for Caltrans Seismic Design Criteria Considering Elastic and Inelastic Response Spectra

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Project Scope & Presentation Outline



0. Current Caltrans Near-Fault Factor -- 2019



Sites located near a rupturing fault may experience elevated levels of shaking at periods longer than 0.5 second due to phenomena such as constructive wave interference, radiation pattern effects, and static fault offset (fling). As a practical matter, these phenomena are commonly combined into a single "near-fault" adjustment factor. This adjustment factor, shown in Figure B.1, is fully applied at locations with a site to rupture plane distance (R_{olgo}) of 15 km (9.4 miles) or less and linearly tapered to zero adjustment at 25 km (15.6 miles). The adjustment consists of a 20% increase in spectral values with corresponding period longer than one second. This increase is linearly tapered to zero at a period of 0.5 second.



Figure B.1 Near-Fault adjustment factor as a function of distance and spectral period. The distance measure is based on the closest distance to any poir t on the fault plane

1. Maximum Distance

- 2. Maximum Amplification Factor
 - 3. Minimum Elastic Period-



PAST RESEARCH PROJECTS



1. NHR3 PSHA with Directivity Project & Products: 2023

www.risksciences.ucla.edu/nhr3/california-directivity



Map Data PSA With&No Directivity (Vs30 ratio) PSA No Directivity PSA With Directivity (Vs760 ratio) PSA With Directivity (Vs30 ratio) PSA With&No Directivity (Vs760 ratio PSA With&No Directivity (Vs30 ratio) Recommended Dir Amp Ratio Dir Amp Ratio Weighted Models Dir Amp Ratio BS13 Dir Amp Ratio BSS20 Dir Amp Ratio CS13 Dir Amp Ratio BS13_FaultNormal Dir Amp Ratio BS13_FaultParallel Site-Specific Vs30 Site-Specific Z1.0 Site-Specific Z2.5 **UCERF-3** Faults Oscillator Period T=3 sec (Directivity) T=0.04 sec (No Directivity) **Return Period** T=0.05 sec (No Directivity) T=0.075 sec (No Directivity) RP=2474.911 vr T=0.1 sec (No Directivity)

P=2474.911 vi T=0.15 sec (No Directivity) RP=50.862 yr T=0.2 sec (No Directivity) RP=99.499 vr T=0.25 sec (No Directivity) T=0.3 sec (No Directivity) RP=474.561 vr T=0.4 sec (No Directivity) RP=949.118 yr T=0.5 sec (Directivity) RP=999.500 vr T=0.75 sec (Directivity) RP=5000.000 yr T=1 sec (Directivity) T=1.5 sec (Directivity) RP=10000.000 vr T=2 sec (Directivity) T=3 sec (Directivity) Site Class Vs30 T=4 sec (Directivity) Vs760 T=5 sec (Directivity) T=75 pac (Diractivity Vs180 T=-1.0 (PGV) sec (No Di Vs500 Ve1100 VsSS (PSHA @ Site-Specific Vs30)

/sSS_ZSS (PSHA @ Site-Specific Vs30,Z1.0,Z2.5)

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Goal: merge three pieces together and take it to PHSA for the State of CA:

- Directivity models
- NGA models
- UCERF3

→ First to develop directivity-based PSHA results and maps for the State of CA

ightarrow PSHA was carried out at over 19,000 sites in the State

- 1. PSA without directivity
- 2. PSA with Directivity
- 3. Directivity Amplification Factor

CS13: Chiou and Spudich (2013) (2022) BS13: Bayless and Somerville (2013) BSS20: Bayless et al. (2020)

2. NHR3 Inelastic-Response Spectra Project: Silvia Mazz Bahrampo

 Compute Inelastic Response Spectra for NGA-West2 database (Bozorgnia, et al, 2014) for strength reduction factors R_mu= 1, 1.5, 2, 2.5, 3, 3.5, 4.
Silvia Mazzoni

1,225,230,300 OpenSees 2D-Model Analyses

2. Develop a **ground motion models** for median and uncertainty for **inelastic spectra**:

Mahdi Bahrampouri

- Displacement ratio (max inelastic displ / Sd_elastic)
- Constant-Ductility Inelastic Response Spectrum
- Adjustment of NGA-West2 elastic PSA model to get inelastic response model

Silvia Mazzoni, Mahdi Bahrampouri, Yousef Bozorgnia

Idealized BILINEAR Model:



Lateral Deformation





Effect of directivity pulses on inelastic and elastic spectra



The average effect of inelasticity on predicted and observed inelastic C_y for those 137 ground motions identified as pulse-like: (a) the ratios of observed over median predicted C_y and (b) the average of the total residual of inelastic C_y minus the total residual of elastic C_y (i.e., PSA)





Directivity-Amplification Factor (Weighted-Avg Model)







Directivity-Amplification Factor (Weighted Model)



Modal Distance ightarrow



DATA MODELING



Objectives



- 1. Determine **Threshold Distance** for Directivity (Modal or Mean)
- 2. Directivity Amplification Factor vs Distance (& Magnitude?) (& Period)





1. Determine Threshold Distance for Directivity



1. Median Value of Directivity-Threshold Distance



2. Directivity Amplification vs Distance – Hinged Fit



Modal Distance (log) ightarrow

2. Directivity Amplification vs Distance – Hinged Fit



Mean Distance (log) →



ALT DIRECTIVITY-AMP MODELS

Quadratic fits for different directivity models



Distance at Directivity Amplification=1.05 vs. Period Mode Data



Mean Data





Maximum Amplification vs. Period



Mean Data





Summary

- Project started April 2024
- Statewide PSHA directivity results have been reduced and simplified
- Distance and directivity amplification ranges for *elastic* response spectra have been quantified via different models
- Next: Work with Caltrans to develop the recommendations on model and metrics
 - Disaggregation Magnitude & Distance
 - Modal
 - Mean

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- o Threshold Distance
 - Median
 - 84%ile

- Directivity Amplification Model
 - Hinged
 - Quadratic
- Directivity-Model Combination
 - Weighted average
 - Envelope the 3 directivity models

Next Steps

Inelastic-Response Spectra

- Modification of directivity amplification and oscillator period range for ductility > 1
- Ground-Motion Selection
 - Use the modified near-fault factors, select and scale input motions at various sites in CA for two return periods (e.g., 975 years and 5000 years).
- Numerical Simulation of Bridge
 - Simulate the responses of bridges (e.g., ductility demand) and compare them using the current Caltrans near-fault factors

