

# PEER International Pacific Rim Forum

## June 16-17, 2021

### A 4-Step Methodology for the Validation of Not-Historical Large-Event Ground-Motion Simulations: the San Francisco Bay Area Case Study

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June 17, 2021



# Agenda

- Introduction
  - Relevance of simulated GMs to engineering domains
  - Historical vs not-historical events
- Proposed 4-step validation methodology and *acceptance criteria*
  - Rock-basin canonical domain
  - The San Francisco Bay Area region
    - Simulation-based site-specific analysis vs ASCE/SEI 7-16
- Concluding remarks

## Inform and support PBEE

Understand what features relevant to the evaluation of the structural risk characterize near-field ground motions

Map the complex variability of structural risk in areas of high seismicity

Enable true site-specific evaluations of earthquake structural risk

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Evaluate seismic hazard based on a (very) large number of simulations from a range of seismic sources

Perform Nonlinear TH analyses

Predict ground-motion amplitudes

# Validation methodologies

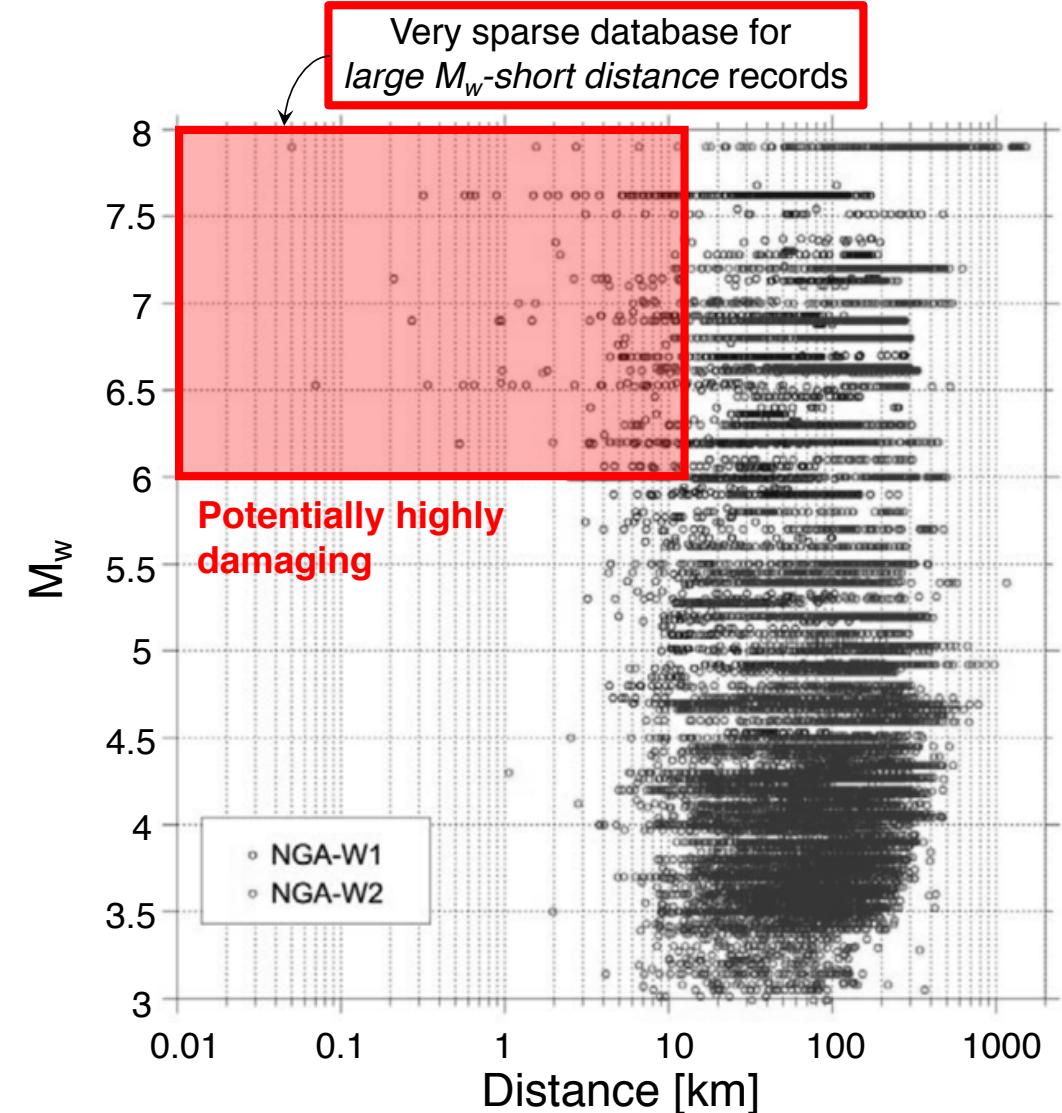
## Historical events

- Station-by-station inspection
- Seismogram waveforms comparison
- Use of well-constrained GMMs

vs

## Not-historical Events

- Records from consistent events are scarce/not available
- GMMs are not well constrained
- the expected GMs characteristics need to be inferred from the knowledge of geology/rupture



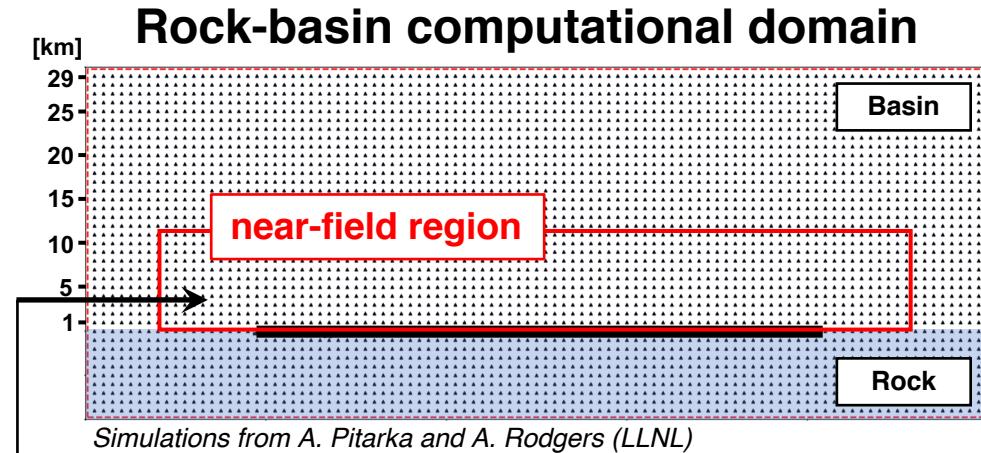
[Source: adapted from Ancheta et al. (2014)]

# Proposed 4-step methodology

## Four-step methodology and acceptance criteria

Application-oriented

- Step 1:** Selection of a population of *real records* consistent with the simulated scenarios
- Step 2:** Comparison of the *distribution of IMs* from the simulated records, real records, and GMPEs
- Step 3:** Comparison of the *distribution of simple proxies for building response*
- Step 4:** Comparison of the *distribution of Engineering Demand Parameters (EDPs)* for a realistic model of a structure.

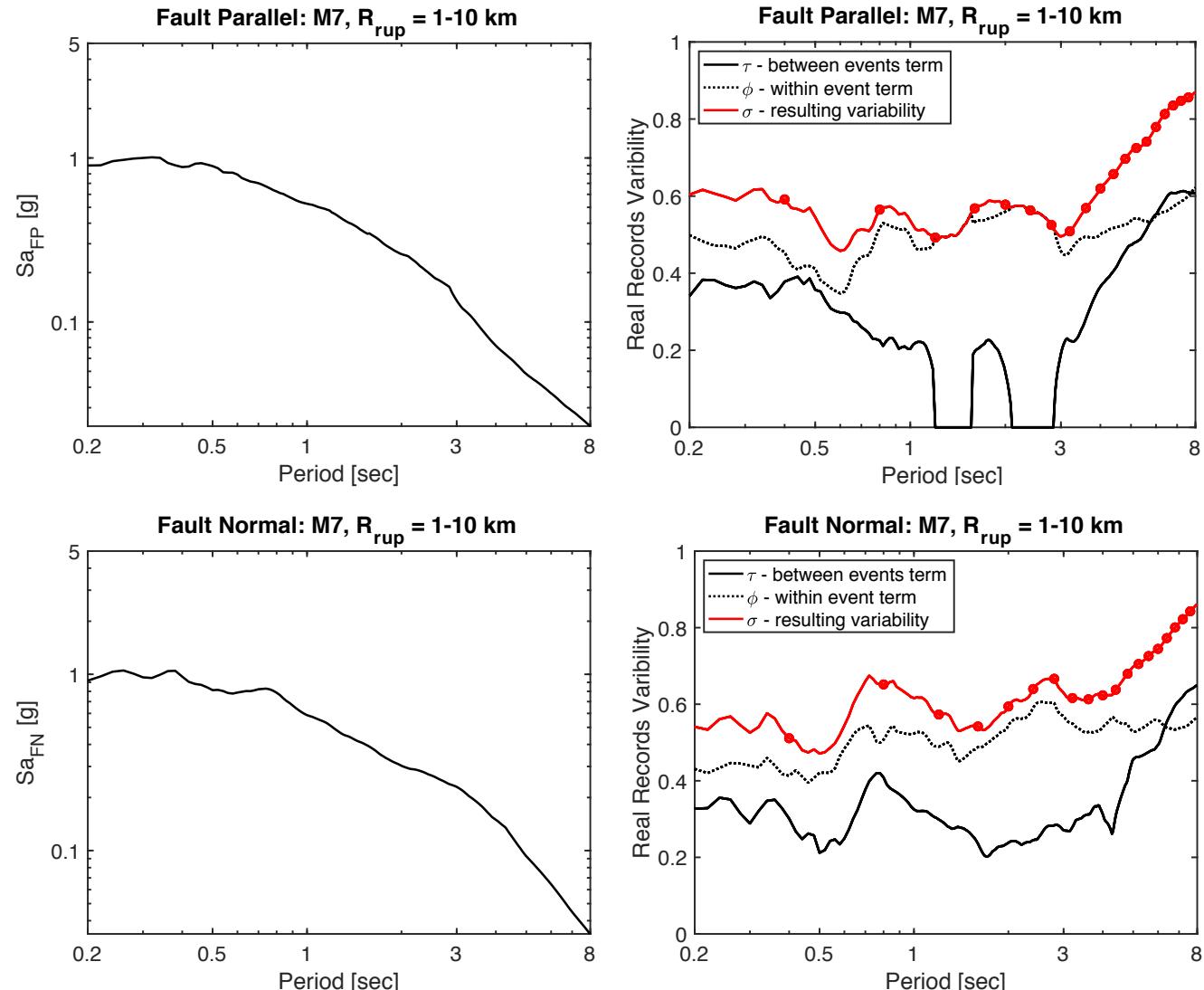


- Three  $M_w$  7 strike-slip earthquake events which differ for the characteristics of the rupture only (Pitarka et al., 2019)
- 40-km x 100-km
- Frequency resolution 5-Hz
- Average  $V_{s30}$  = 382-m/sec
- Flat topography
- 40-story Steel MRF ( $T_1$  = 3.76-sec)
- 2,490 building runs for each component (FN and FP)

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# Step 1 – Real records selection

No.	Earthquake Name	Station Name	$M_w$	$R_{rup}$ (km)	V <sub>s30</sub> (m/s)
1	Imperial Valley-06 (1979)	EC County Center FF	6.53	7.31	192.1
2		EC Meloland Overpass FF		0.07	186.2
3		El Centro Array #4		7.05	208.9
4		El Centro Array #5		3.95	205.6
5		El Centro Array #6		1.35	203.2
6		El Centro Array #7		0.56	210.5
7		El Centro Array #8		3.86	206.1
8		El Centro Differential Array		5.09	202.3
9*	Morgan Hill (1984)	Coyote Lake Dam (SW Abut)	6.19	0.53	597.1
10*	Loma Prieta (1989)	Gilroy - Gavilan Coll.	6.93	9.96	729.7
11		LGPC		3.88	477.7
12	Landers (1992)	Lucerne	7.28	2.19	684.9
13	Northridge-01 (1994)	Jensen Filter Plant	6.69	5.43	373.1
14		Jensen Filter Plant Generator		5.43	525.8
15		Newhall - Fire Sta		5.92	269.1
16		Newhall - W Pico Canyon Rd.		5.48	285.9
17		Rinaldi Receiving Sta		6.50	282.3
18		Sylmar - Converter Sta		5.35	251.2
19		Sylmar - Converter Sta East		5.19	370.5
20		Sylmar - Olive View Med FF		5.30	440.5
21	Kobe, Japan (1995)	KJMA	6.90	0.96	312.0
22		Takarazuka		0.27	312.0
...	...	...		...	...
38	Chi-Chi, Taiwan (1999)	WGK	7.62	9.96	258.9
		<b>Median</b>	7.07 (mean)	2.88	365.7
		<b>StDev (In units)</b>	0.50 (linear)	1.16	0.42

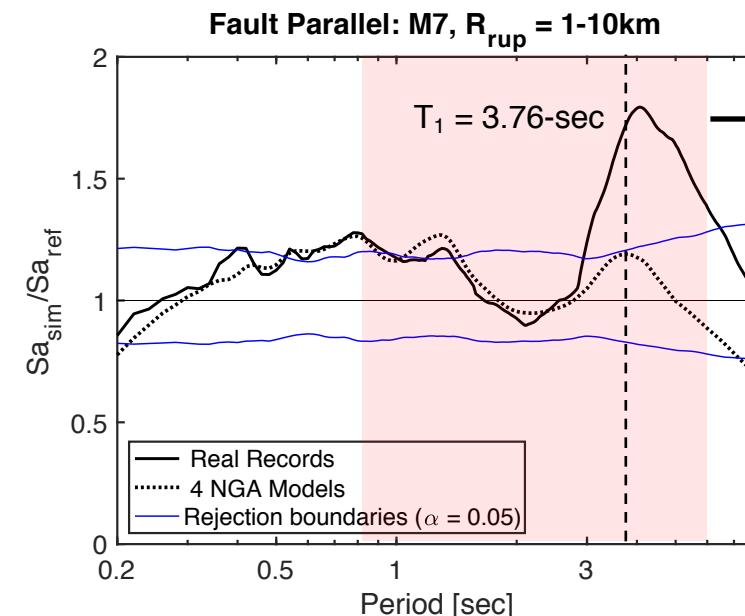
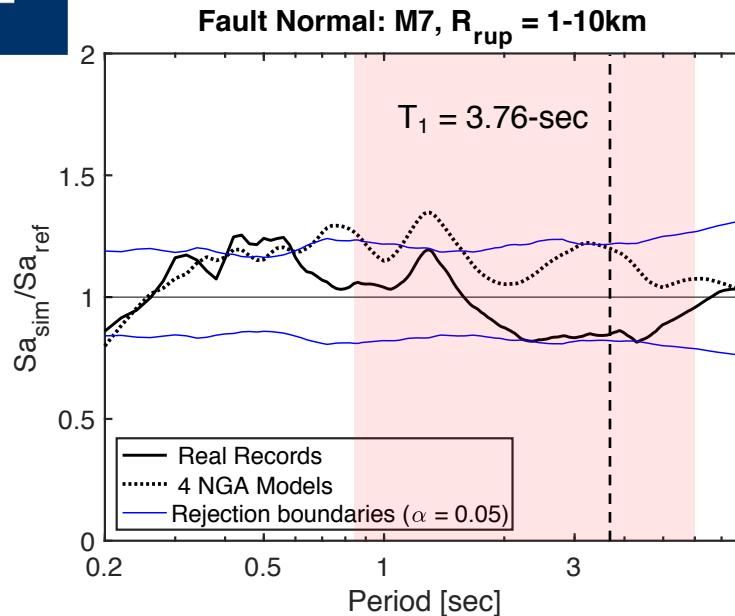


- Total of 38 real records resolved in FN and FP component (Baker and Shahi, 2011)

- The variability resulting from the uneven sampling of earthquakes was evaluated with a linear mixed-effects model

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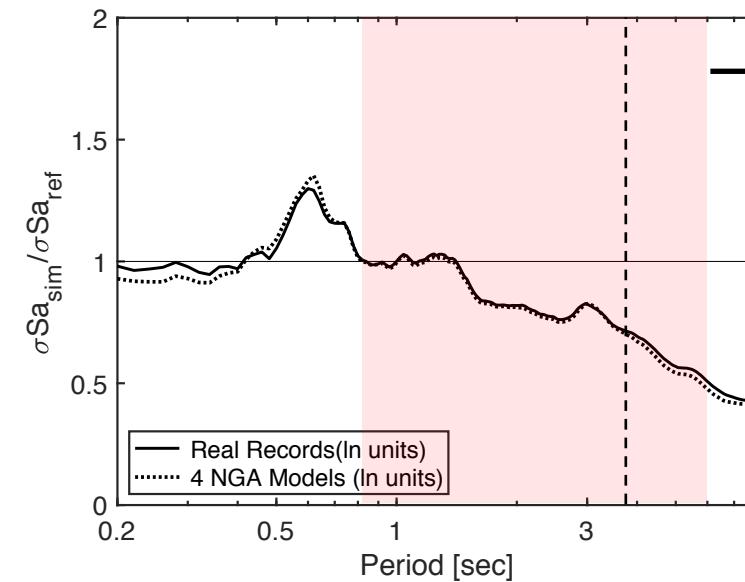
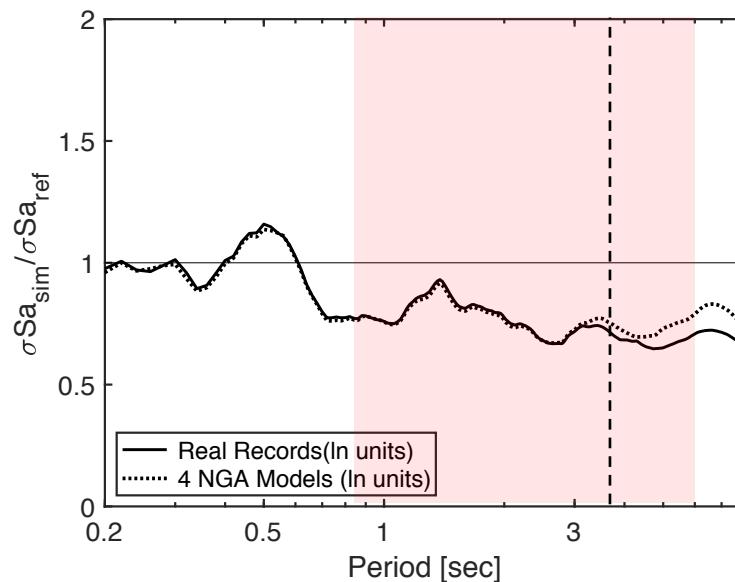
## Step 2 – Distribution of IMs for the two separate components



Overestimate of Sa amplitude with respect to real records

### Acceptance criteria

$$\mu_{lnSa,rec} \pm 1.96 \sqrt{\frac{\sigma_{lnSa,rec}^2}{n_{rec}} + \frac{\sigma_{lnSa,sim}^2}{n_{sim}}}$$



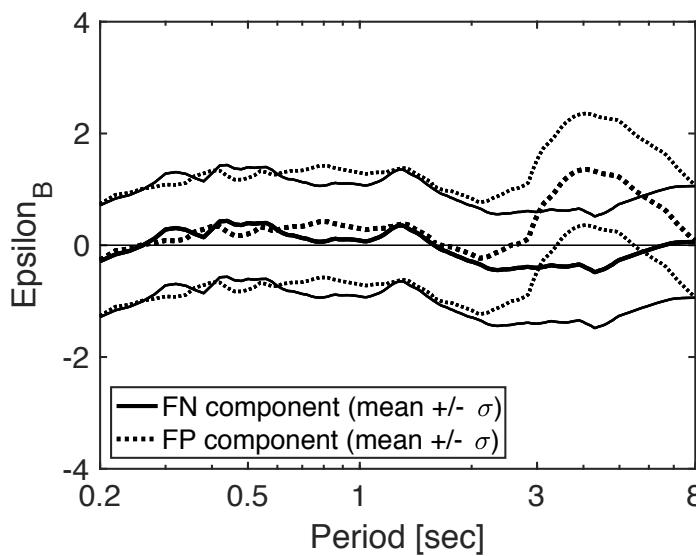
Underestimate of Sa variability with respect to both real records and GMPEs

# Step 3 – Distribution of Building Response Proxies

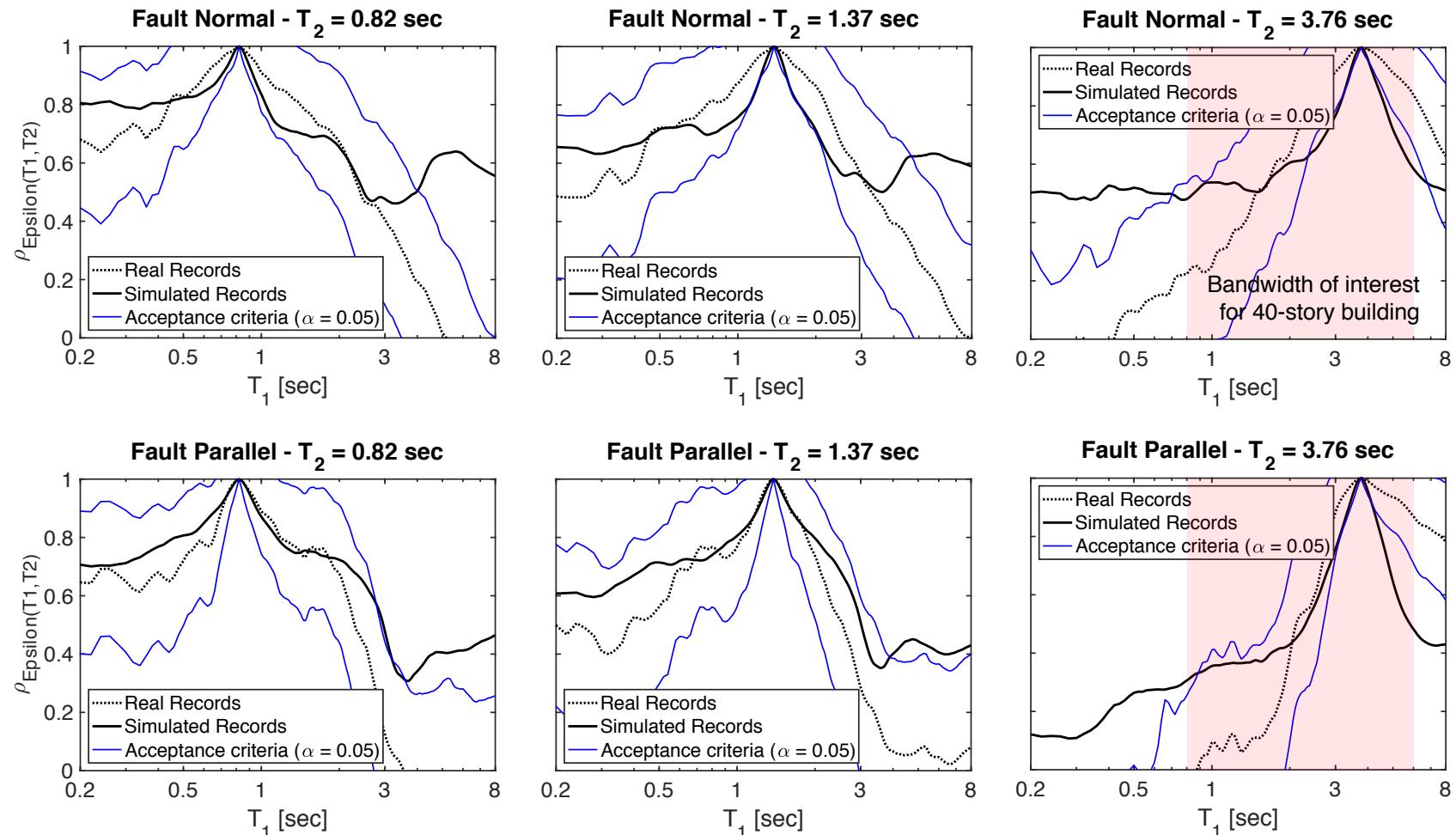
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- Inter-period correlation
- Ground-motion polarization
- Ground-motion significant duration

## Inter-period correlation



$$\epsilon_{Bi} = \frac{\ln[Sa_i(T)_{sim}] - \mu_{lnSa(T)_{rec}}}{\sigma_{lnSa(T)_{sim}}}$$

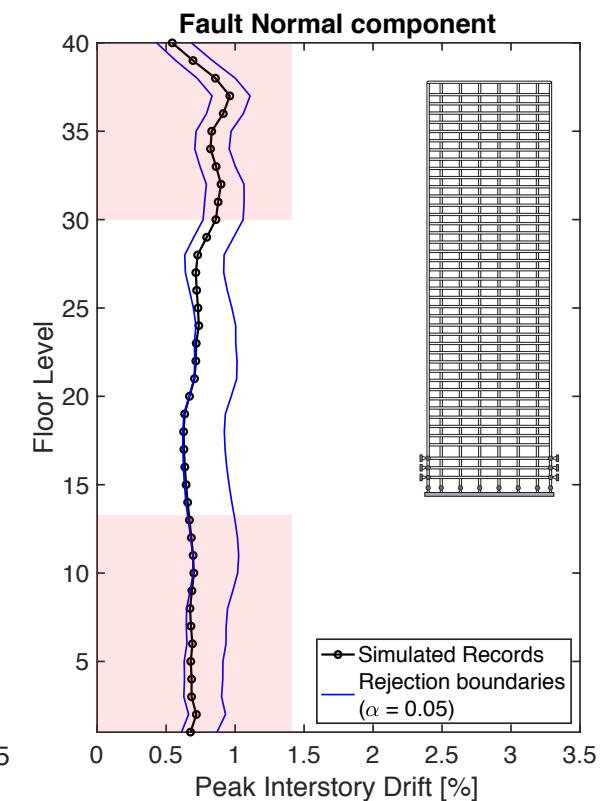
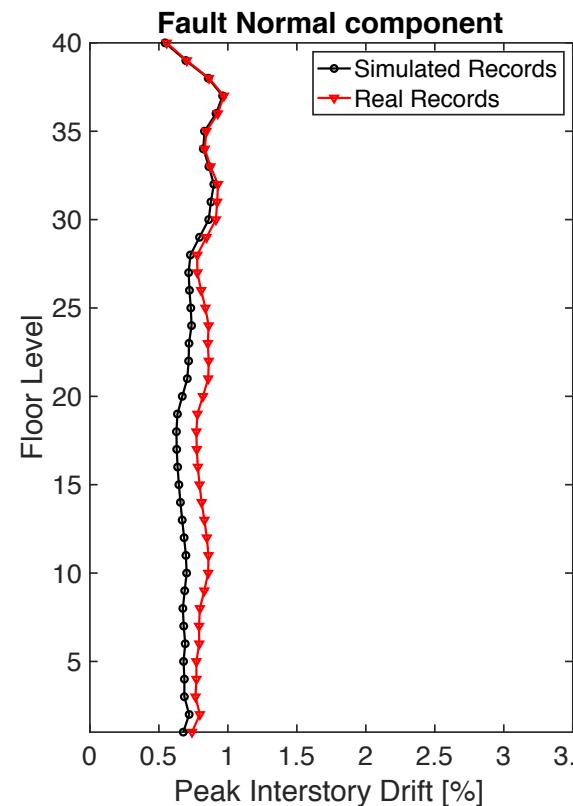
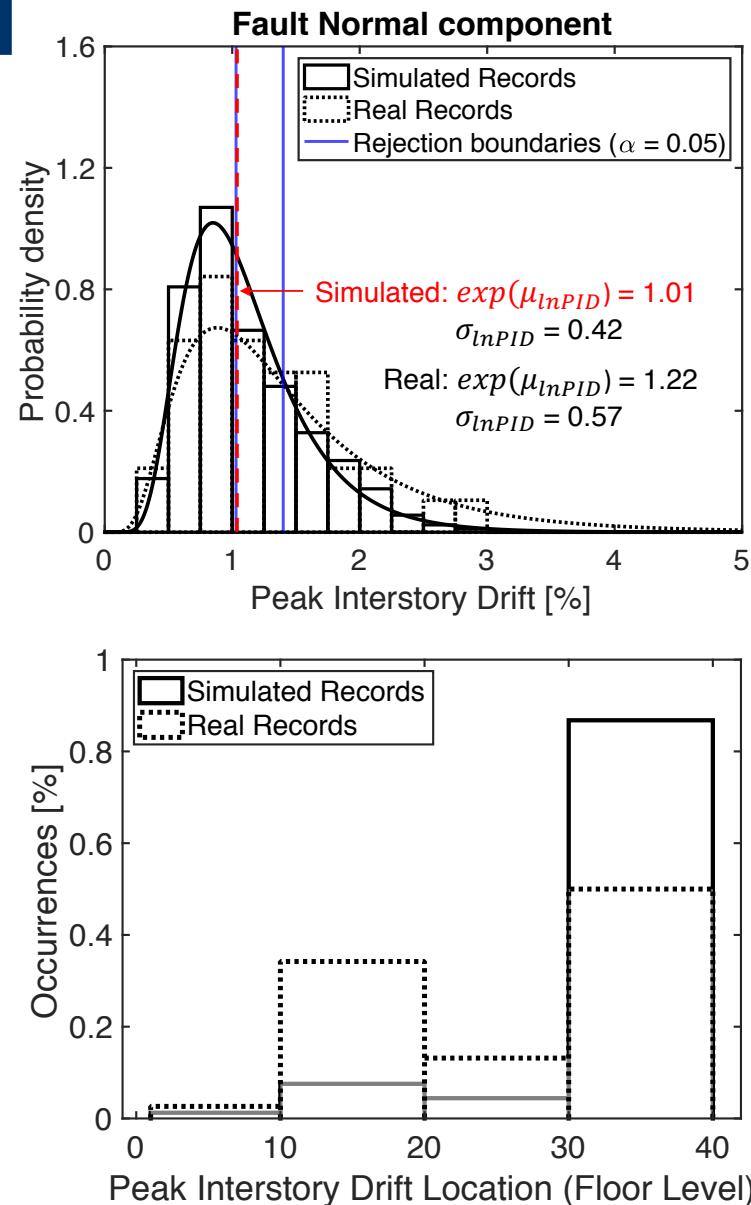


## Acceptance criteria

$$\rho_{rec(T_1, T_2)} \pm 1.96 \sigma_{\rho(T_1, T_2)}$$

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# Step 4 – Distribution of building response from FEMs



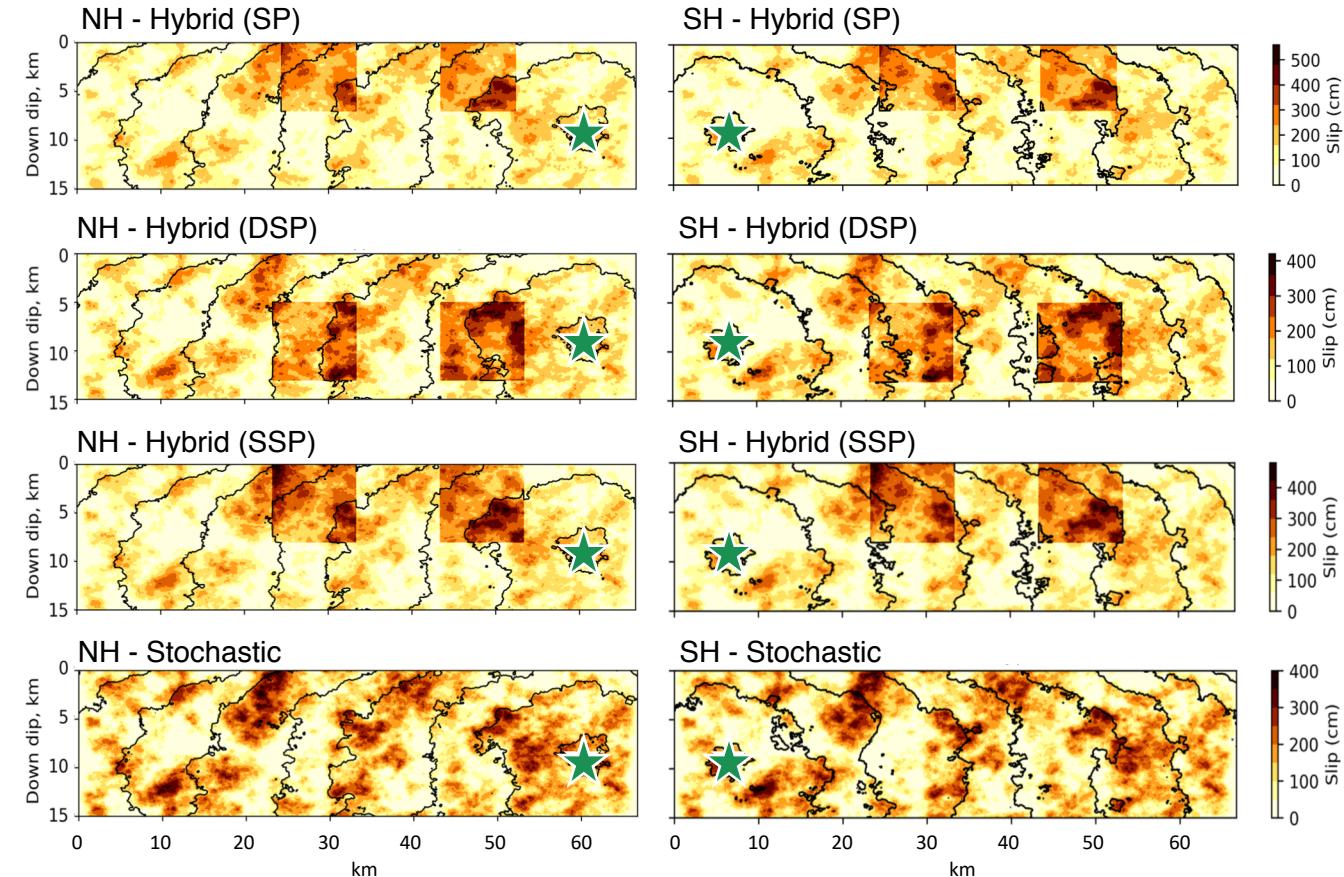
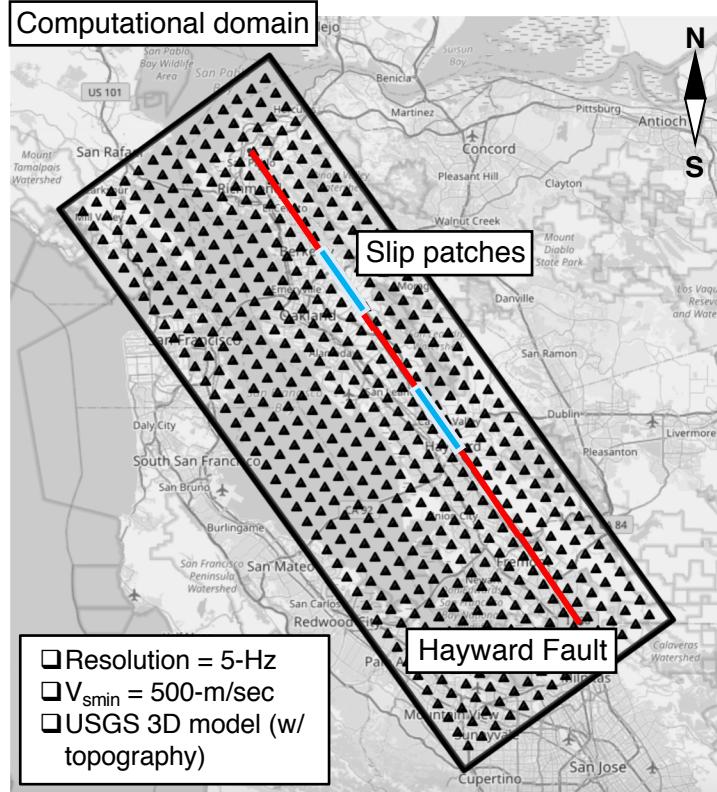
## Acceptance criteria

$$(\mu_{lnPID})_{rec,i} \pm 1.96 \sqrt{\frac{\sigma_{lnPID,rec,i}^2}{n_{rec}} + \frac{\sigma_{lnPID,sim,i}^2}{n_{sim}}}$$

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# The San Francisco Bay Area Case Study

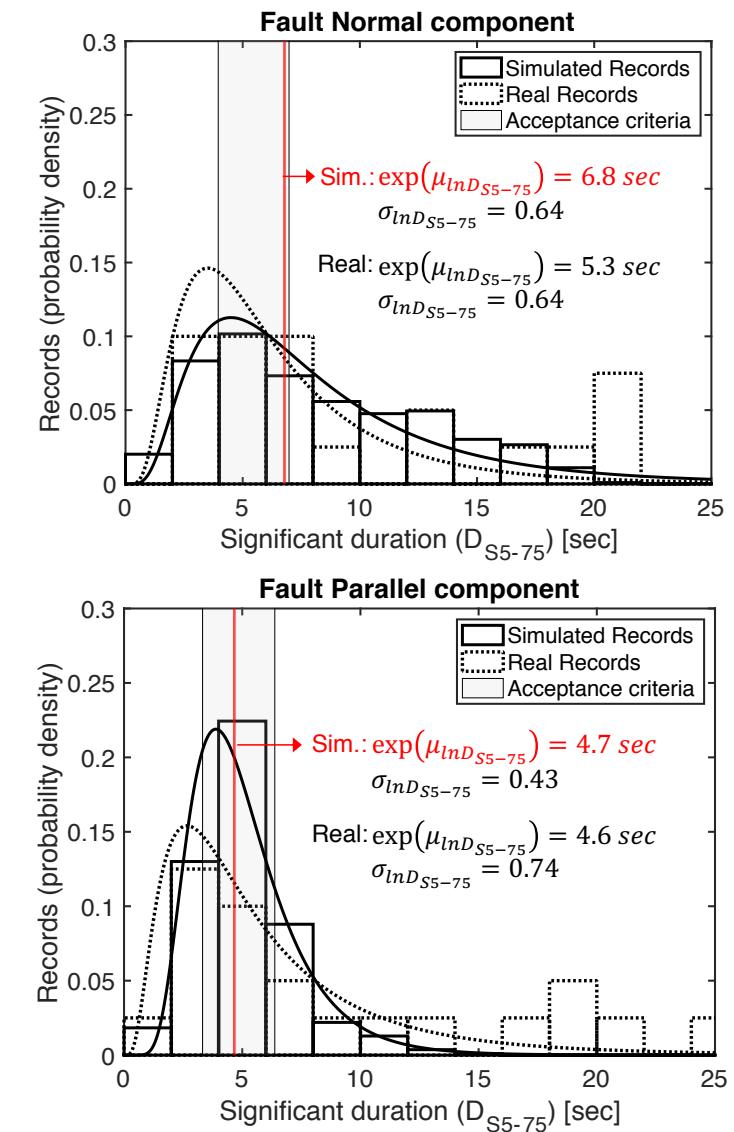
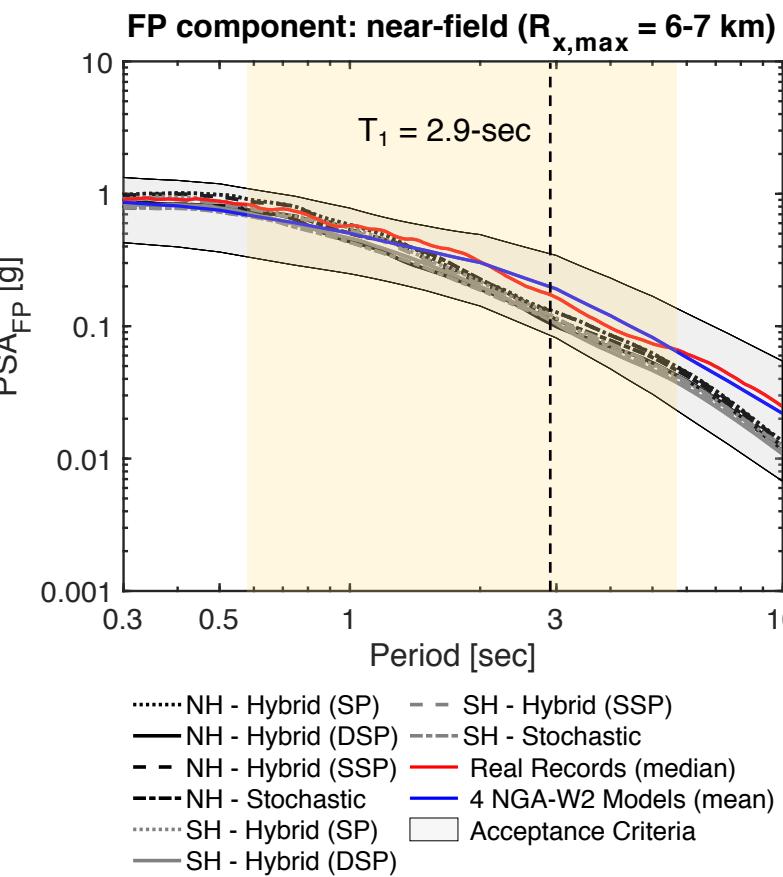
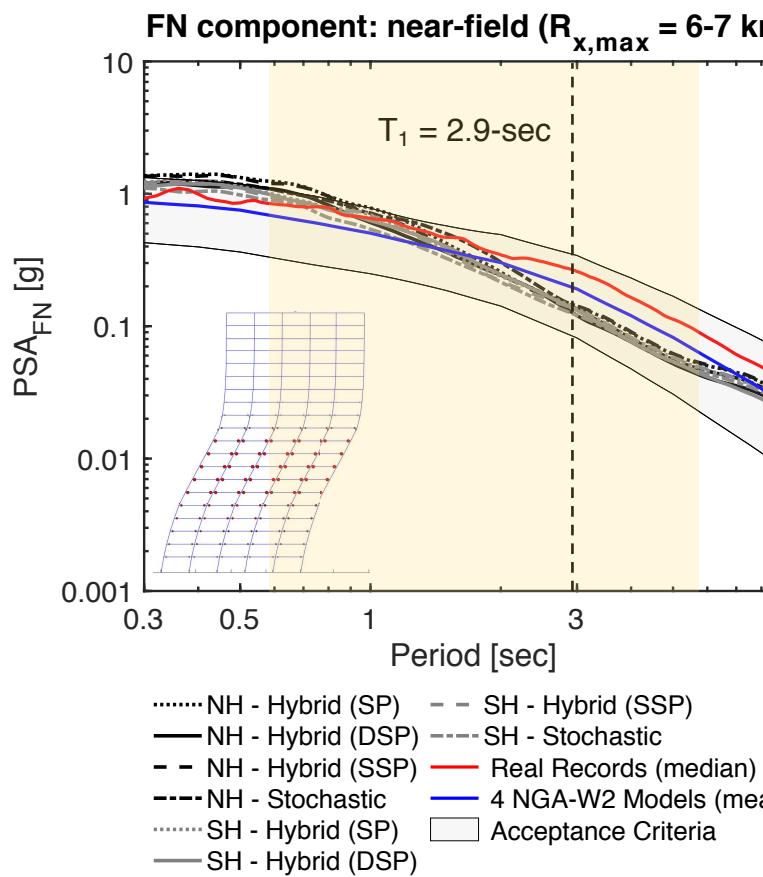
The same validation approach was extended to a real domain representing the San Francisco Bay Area to simulate 8  $M_w$  7 Hayward Fault earthquakes.



Simulations by Arthur Rodgers and Arben Pitarka

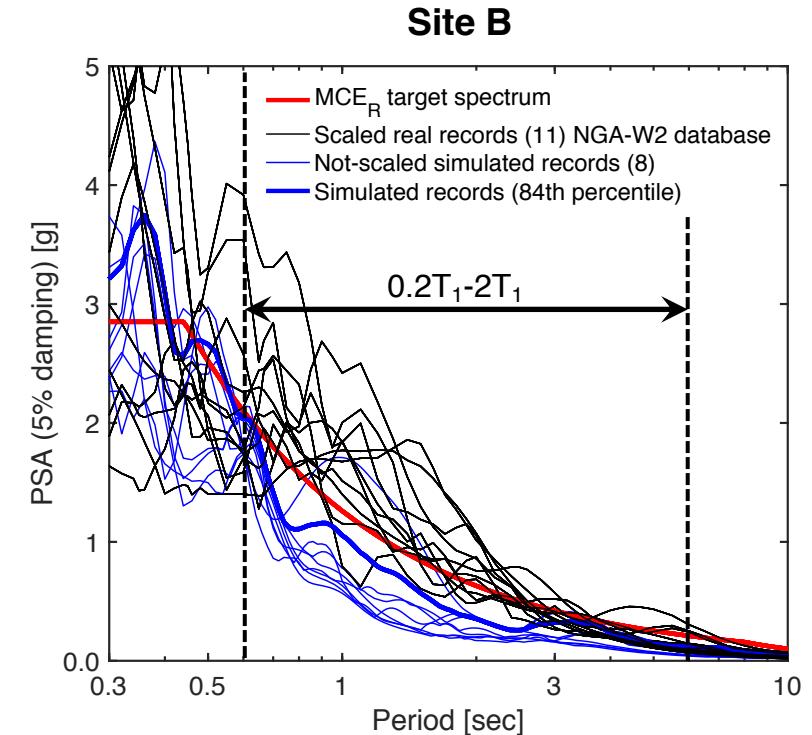
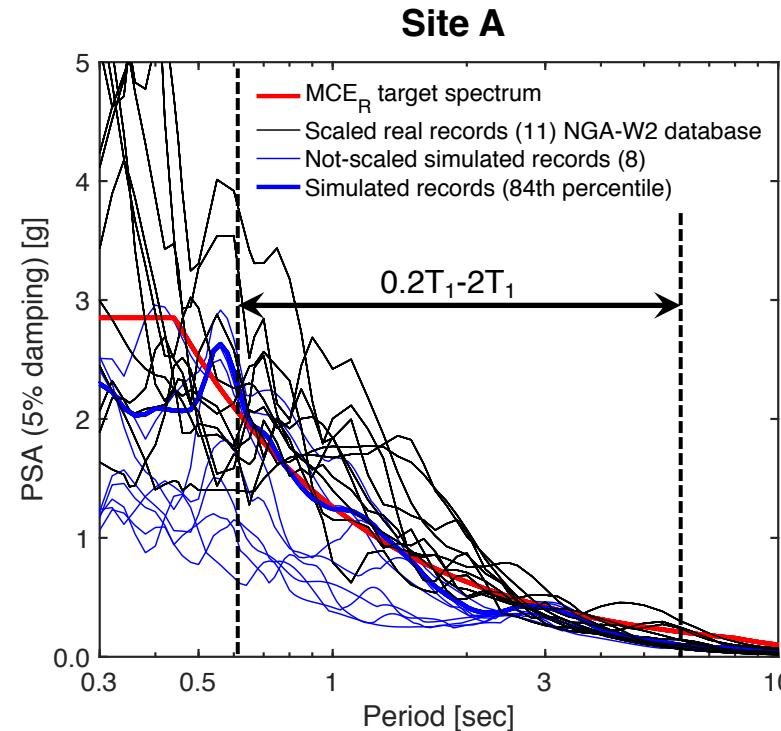
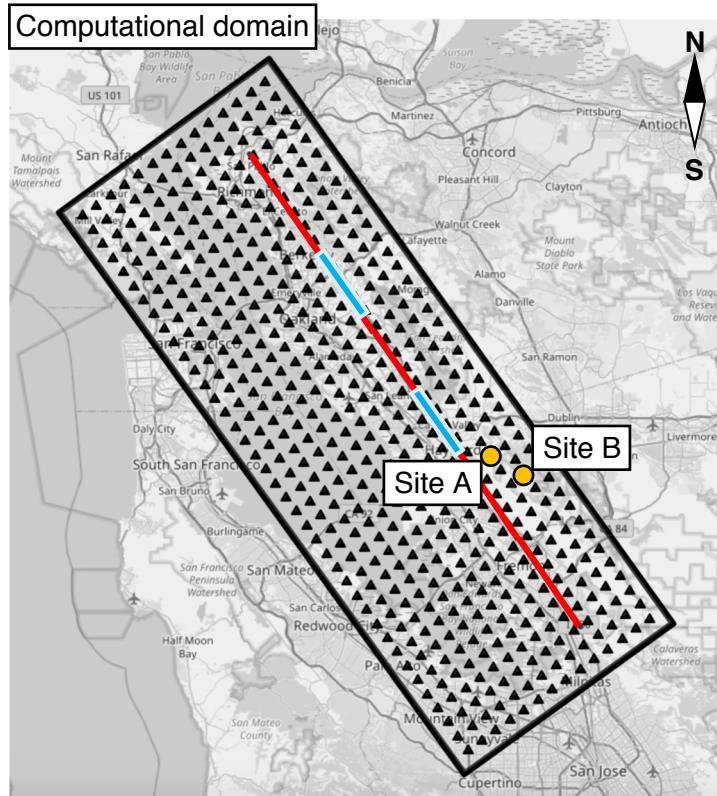
# SFBA ground-motion validation (snapshot)

## PSA and ground-motion significant duration



# Simulation-Based Site-Specific Analysis

Can simulated ground motions enable true site-specific analyses?



Soil class C:  $V_s = 637\text{-m/sec}$

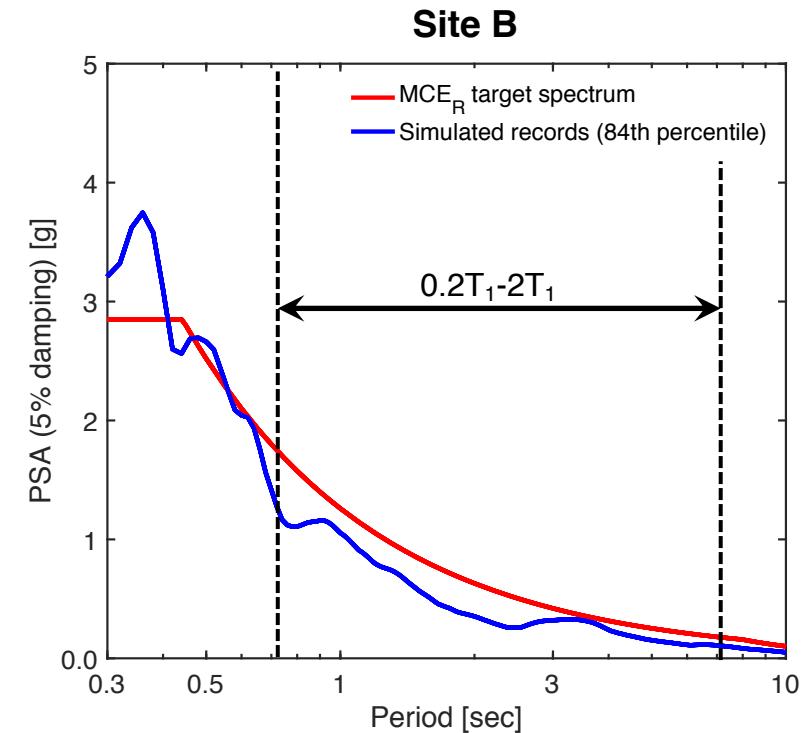
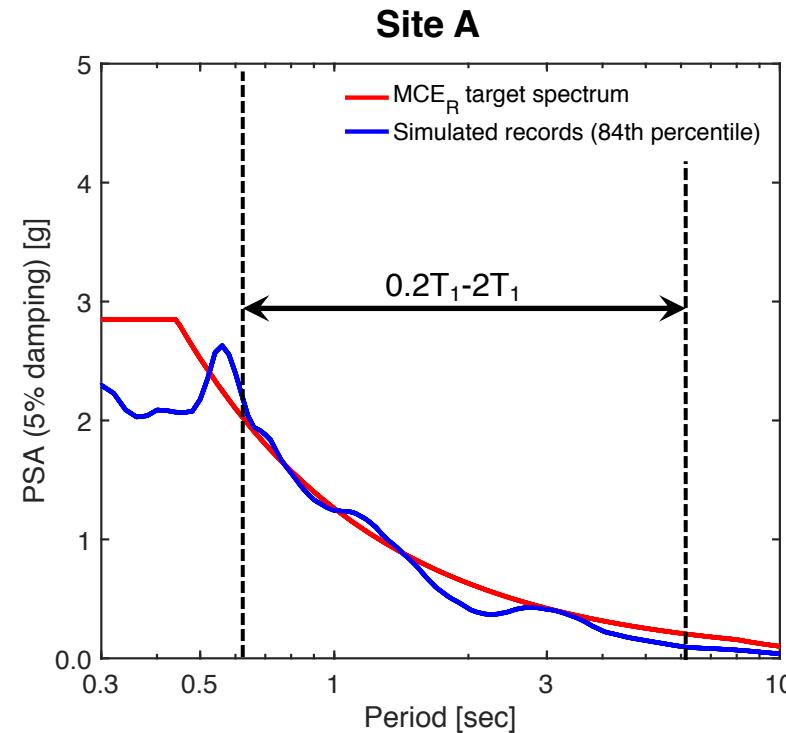
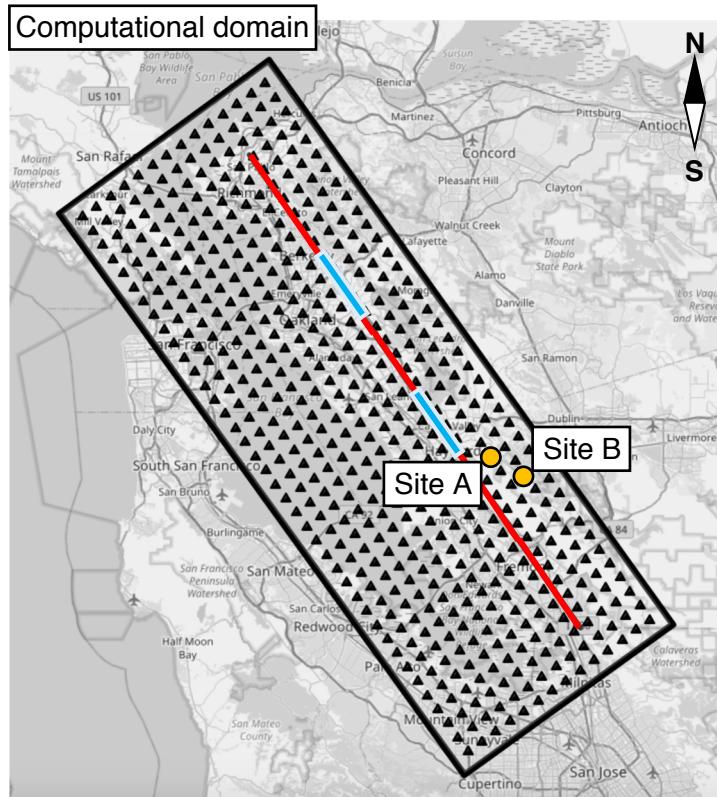
Scale factor: <5

$M_w \sim 7.2$ ,  $R_{rup} = 4$  to 5-km

20-story RC-MRF:  $T_1 = 2.9\text{-sec}$

# Simulated Ground-Motion Selection

How do we select simulated ground motions?



# Concluding remarks

- ❑ Current research is **expanding the proposed 4-step methodology** to explicitly incorporate ground-motion features affecting the response of long-period structures (e.g., pulse-like components).
- ❑ Current efforts are extending the site-specific analyses to the entire San Francisco Bay Area region to **investigate the effect of the site-specificity** enabled by physics-based ground-motion simulations **on structural design and assessment** at the regional scale for multiple building typologies.
- ❑ Future work will **further investigate the ground-motion variability** deriving from purely uncorrelated ruptures where multiple parameters are made to vary (e.g., randomization of the slip distribution seed, hypocenter, rupture speed, risetime, etc.).

**Thank you!**