

National Science Foundation





NHERI@UC San Diego: Facility Description and Capabilities

Koorosh Lotfizadeh, Ph.D. Department of Structural Engineering, UC San Diego





2023 PEER Annual Meeting

August 24-25, 2023 University of California, Berkeley



Outline

- Overview of Englekirk Structural Engineering Center
- Large High-Performance Outdoor Shake Table (LHPOST)
- Six-Degree-of-Freedom (6-DOF) Upgrade of LHPOST to LHPOST6
 - Design and Description of the Upgrade
 - Performance of the LHPOST6
- Instrumentation and Data Acquisition System
- New Research Opportunities Made Possible by LHPOST6

NHERI Operations Personnel

NHERI@UC San Diego Organization Chart



Overview: Englekirk Structural Engineering Center (ESEC)

Englekirk Structural Engineering Center



Large High-Performance Outdoor Shake Table (LHPOST)

IAS Accreditation



CERTIFICATE OF ACCREDITATION

This is to attest that

ENGLEKIRK STRUCTURAL ENGINEERING CENTER (UCSD) 10201 POMERADO ROAD SAN DIEGO, CALIFORNIA 92131 U.S.A.

Testing Laboratory TL-1065

has met the requirements of AC89, *IAS Accreditation Criteria for Testing Laboratories*, and has demonstrated compliance with ISO/IEC Standard 17025:2017, *General requirements for the competence of testing and calibration laboratories*. This organization is accredited to provide the services specified in the scope of accreditation.

Effective Date May 31, 2023



Ley nather

President

Visit www.iasonline.org for current accreditation information.

Large High-Performance Outdoor Shake Table (LHPOST)

History



San Diego

1-DOF Large High-Performance Outdoor Shake Table (LHPOST)





Performance Characteristics of LHPOST in Past 1-DOF Configuration (2004 – 2019)					
Designed as a 6-DOF shake table, but built as a 1-DOF system to meet funding available					
Stroke	±0.75m				
Platen Size	40 ft × 25 ft (12.2 m × 7.6 m)				
Peak Velocity	1.8 m/sec				
Peak Acceleration	4.7g (bare table condition); 1.2g (4.0MN/400 tonf rigid payload)				
Frequency Bandwidth	0-33 Hz				
Horizontal Actuators Force Capacity	6.8 MN (680 tonf)				
Vertical Payload Capacity	20 MN (2,000 tonf)				
Overturning Moment Capacity	50 MN-m (5,000 tonf-m)				

Tracking Performance of LHPOST (1-DOF)



Use of LHPOST in Combination with Large Soil Boxes



Laminar soil shear box: $6.7m (L) \times 3.0m (W) \times 4.7m (H)$

Stiff soil confinement box: 10.0m (L) \times 4.6 or 5.8m (W) \times 7.6m (H)

- To investigate the seismic response of soil-foundation-structural systems.
- To complement centrifuge tests in order to validate computational models.
- To study the performance of bridge abutments, earth retaining walls, slope stability in hillside construction, and underground structures.
- To investigate **soil liquefaction** and its effect on the seismic response of soil-foundationstructural systems.

Select Set of Shake Table Tests on LHPOST (1-DOF)

































August 24-25, 2023

University of California San Diego

Six-Degree-of-Freedom (6-DOF) Upgrade of LHPOST to LHPOST6

Hydraulic Power System of LHPOST6



Accumulator Bank of LHPOST6



- Accumulator bank
 - > 75 bottles total, 15 skids with 5 bottles each
 - > 130 gallons per bottle
 - 3000 psi minimum Nitrogen pressure in each bottle in idle condition
- Pressure changes throughout the day with ambient temperature fluctuations
- Wireless real-time monitoring of pressure and temperature in each bottle
 - Equipped with wireless Sensonode Gold by Parker
 - Data captured by wireless gateway and passed to SQL server
 - Web-based user interface for local or remote monitoring

Accumulator Bank of LHPOST6



LHPOST6



Performance Characteristics of LHPOST6

Performance Characteristics of LHPOST6

Uniaxial performance characteristics of the LHPOST6 Sinusoidal motions - Bare table condition - Centered rigid payload of 4.9 MN (1,100 kips)

Platen size	12.2 m × 7.6 m (40 ft × 25 ft)						
Frequency Bandwidth	0 – 33 Hz						
Vertical Payload Capacity	20 MN (4,500 kip)					
	Sinusoidal motions - Bare table condition		Sinusoidal motions - Centered rigid payload of 4.9 MN (1,100 kips)				
	Horizontal X (E-W)	Horizontal Y (N-S)	Vertical Z (-)	Horizontal X (E-W)	Horizontal Y (N-S)	Vertical Z (-)	
Peak Translational Displacement	±0.89 m (±35 in)	±0.38 m (±15 in)	±0.127 m (±5 in)	±0.89 m (±35 in)	±0.38 m (±15 in)	±0.127 m (±5 in)	
Peak Translational Velocity	3.0 m/sec (118 in/sec)	2.0 m/sec (80 in/sec)	0.45 m/sec (17 in/sec)	3.0 m/sec (118 in/sec)	2.0 m/sec (80 in/sec)	0.55 m/sec (21 in/sec)	
Peak Translational Acceleration	(5.8 g) ⁽¹⁾ 3.7 g ⁽²⁾	(4.7 g) ⁽¹⁾ 1.85 g ⁽²⁾	-3.4 g +31.1 g ⁽¹⁾ +11.9 g ⁽³⁾	(1.6 g) ⁽¹⁾ 1.0 g ⁽²⁾	(1.25 g) ⁽¹⁾ 0.50 g ⁽²⁾	-1.64 g +7.5 g ⁽¹⁾ +2.5 g ⁽²⁾	
Peak Translational Force	10.6 MN ⁽¹⁾ (2,380 kip) ⁽¹⁾ 6.8 MN ⁽²⁾ (1,530 kip) ⁽²⁾	8.38 MN ⁽¹⁾ (1,890 kip) ⁽¹⁾ 3.4 MN ⁽²⁾ (765 kip) ⁽²⁾	-4.3 MN ⁽⁴⁾ +57.0 MN ⁽⁵⁾ (+12,800 kip) ⁽⁵⁾ +22.9 MN ⁽⁶⁾ (+5,150 kip) ⁽⁶⁾	10.6 MN ⁽¹⁾ (2,380 kip) ⁽¹⁾ 6.8 MN ⁽²⁾ (1,530 kip) ⁽²⁾	8.38 MN ⁽¹⁾ (1,890 kip) ⁽¹⁾ 3.4 MN ⁽²⁾ (765 kip) ⁽²⁾	-4.3 MN ⁽⁴⁾ +57.0 MN ⁽⁵⁾ (+12,800 kip) ⁽⁵⁾ +22.9 MN ⁽⁶⁾ (+5,150 kip) ⁽⁶⁾	
Peak Rotation	2.22 deg ⁽⁷⁾	1.45 deg ⁽⁷⁾	3.8 deg	2.22 deg (7)	1.45 deg ⁽⁷⁾	3.8 deg	
Overturning Moment Capacity	32.0 MN-m (23,600 kip-ft)	35.0 MN-m (25,800 kip-ft)		45.1 MN-m (33,200 kip-ft)	50.0 MN-m (36,900 kip-ft)		

- (1) Peak acceleration controlled by the actuator force capacities in the control zero-position of the table.
- (2) Acceleration limit controlled by the reaction mass until further studies.
- (3) Acceleration limit controlled by the design strength of the steel honeycomb platen.
- (4) Assuming a pressure of 125 psi in the chamber of each vertical actuator and accounting for the hold-down forces in the control zero-position of the table.
- (5) Peak force controlled by the vertical actuator force capacities and accounting for the hold-down forces in the control zero-position of the table.
- (6) Force limit controlled by the design strength of the steel honeycomb platen and accounting for the hold-down forces in the zero control position of the table.
- (7) Due to kinematics of the piston seals of the vertical actuators.

August 24-25, 2023

University of California San Diego

Target vs. Achieved Tri-Axial Ground Motion - 1995 M6.9 Kobe, Japan, Takatori Station







AC-156 Compatible Earthquake, Tri-Axial Ground Motion



1978, M7.4 Tabas, Iran, Tri-Axial Ground Motion



Synthetic 6-DOF Ground Motion



1989 Loma Prieta Earthquake, MCER Level, XYZ (5/17/2023)



Instrumentation and Data Acquisition

Instrumentation and Data Acquisition

> Objectives

- Provide quality management system
- Provide nationally and internationally recognized testing data and reports
- Maintain a calibrated sensor and equipment inventory
- Documentation
 - Documentation master log file
 - General documentation
 - Standard operation procedures
 - In-house calibration procedures
 - Sensory inventory
 - Equipment inventory
 - > Calibration reports



Accelerometer linearity



Accelerometers



Reference equipment



Displacement transducers

University of California San Diego

Instrumentation and Data Acquisition

- Instrumentation available:
 - 251 MEMS-Based Accelerometers (±5g and ±10g)
 - 305 Linear Displacement Transducers (1 to 20 in)
 - > 154 String Potentiometer Displacement Transducers (2 to 120 in)
 - 28 Inclinometers (±15 deg)
 - 4 Load Jacks
 - 31 Load Cells (up to 20,000 lbs)
 - > 32 Soil Pressure Transducers
- ➢ GNSS System:
 - > 10 Receivers Operating at 100 Hz
- > Cameras:
 - Drones (DJI Phantom 4 Pro)
 - GoPro Cameras (4K and 1080p)
 - End-to-end Live Video Streaming Production System



University of California San Diego

New Research Opportunities Made Possible by LHPOST6

New Research Opportunities Made Possible by LHPOST6

- Investigate the combined effect of realistic near-field translational and rotational earthquake ground motions applied as dynamic excitation to full 3D and large/full-scale structural, geotechnical, or soil-foundationstructural systems, including:
 - Effects of SSI (both kinematic and inertial)
 - Non-linear soil and structural behavior
 - Soil liquefaction
 - Seismic compression



Geometric interpretation of how horizontal translation and rocking can contribute to the total drift in a simple building during passage of a Rayleigh wave [Trifunac, 2009]

Van Den Einde, L., Conte, J.P., Restrepo, J.I., Bustamante, R., Halvorson, M., Hutchinson, T.C., Lai, C.T., Lotfizadeh, K., Luco, J.E., Morrison, M.L. and Mosqueda, G., 2021. *NHERI@ UC San Diego 6-DOF large high-performance outdoor shake table facility. Frontiers in Built Environment*, 6, p.580333.

For More Information About NHERI@UC San Diego LHPOST6

> Join us at our annual NHERI@UC San Diego User/Researcher Training Workshop

- December 14-15, 2023
- Registration begins soon
- Visit us on the web:
 - DesignSafe: <u>ucsd.designsafe-ci.org</u>
 - UCSD: <u>nheri.ucsd.edu</u>

> Contact one of the NHERI@UC San Diego team members:

- Koorosh Lotfizadeh, <u>klotfiza@ucsd.edu</u>
- Joel Conte, jpconte@ucsd.edu
- John McCartney, <u>mccartney@ucsd.edu</u>
- Machel Morrison, <u>mmorrison@ucsd.edu</u>
- Jose Restrepo, jrestrepo@ucsd.edu
- Lelli Van Den Einde, <u>lellivde@ucsd.edu</u>

Thank You