



# OpenSees implementation of 3D embedded pile element for analysis of SSI problems

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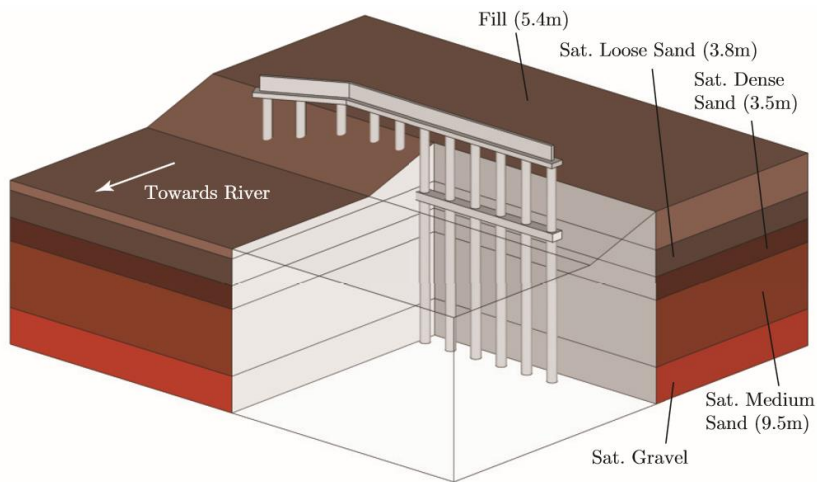
# Collaborators

- Dr. Katheryn Petek – Shannon & Wilson
- Dr. Chris McGann – Univ. of Canterbury
- **Dr. Alborz Ghofrani** – Golder & Associates
- Dr. Long Chen – Hart Crowser
- Dr. Domenico Gallese, Dr. Luigi Callisto – La Sapienza

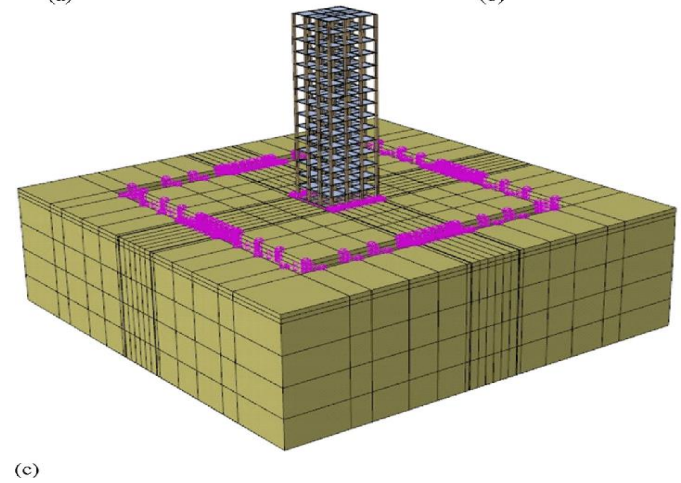
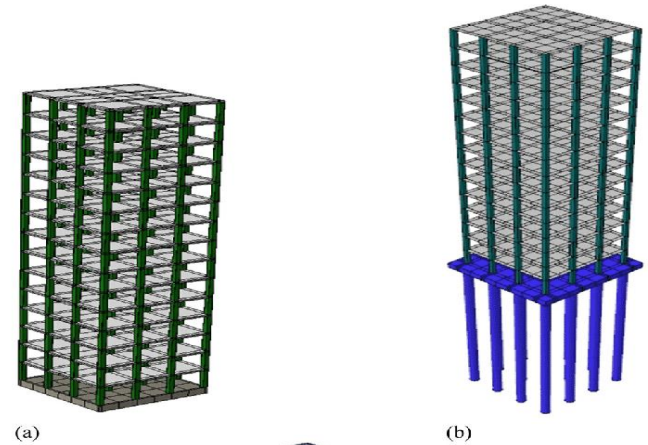
## Sponsors



# Motivation: Modeling complex SSI systems



**Bridge abutment**



**Building foundation**



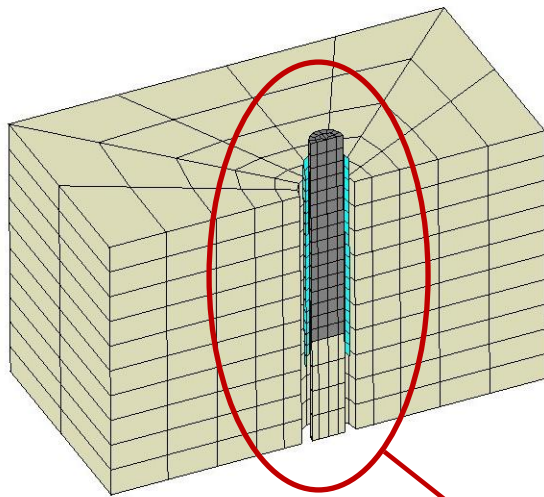
# Numerical Simulation needs 3D FEM Models

- Total or Effective stress analysis
  - Single phase formulation: brick elements
  - Multi-phase formulation: u-P formulation using brickUP elements
- Soil constitutive model
  - Capture nonlinear behavior of the soil
  - Capture contractive/dilative behavior
  - Capture cyclic mobility
- **Soil-Foundation Interaction**
  - Interface behavior
    - Frictional behavior?
    - Gap forming?
  - Take advantage of 1D beam elements

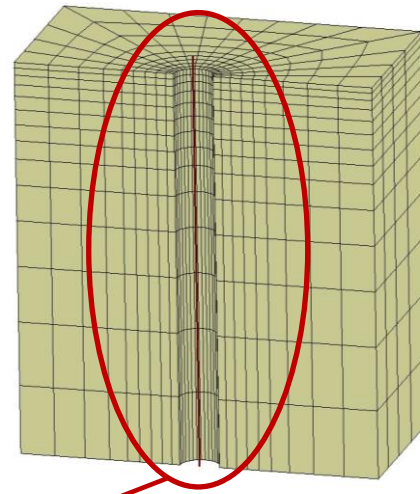
In particular, **3D dynamic FEM** analysis of soil-structure interaction problems requires advanced numerical methods

# Solid-solid and beam-solid contact

## Mesh difficulties/challenges



Solid-Solid Model



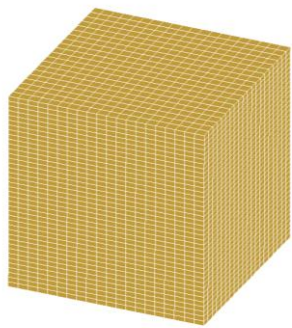
Beam-Solid Model



Embedded element

meshing challenges

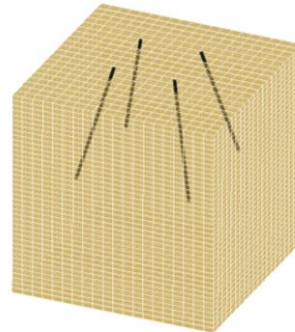
# Proposed approach: Embedded Elements



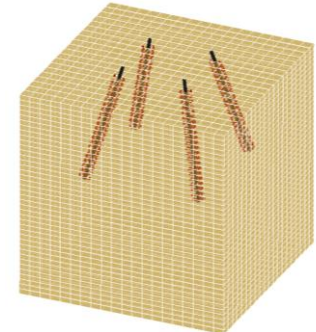
Regular FEM mesh



Beam elements



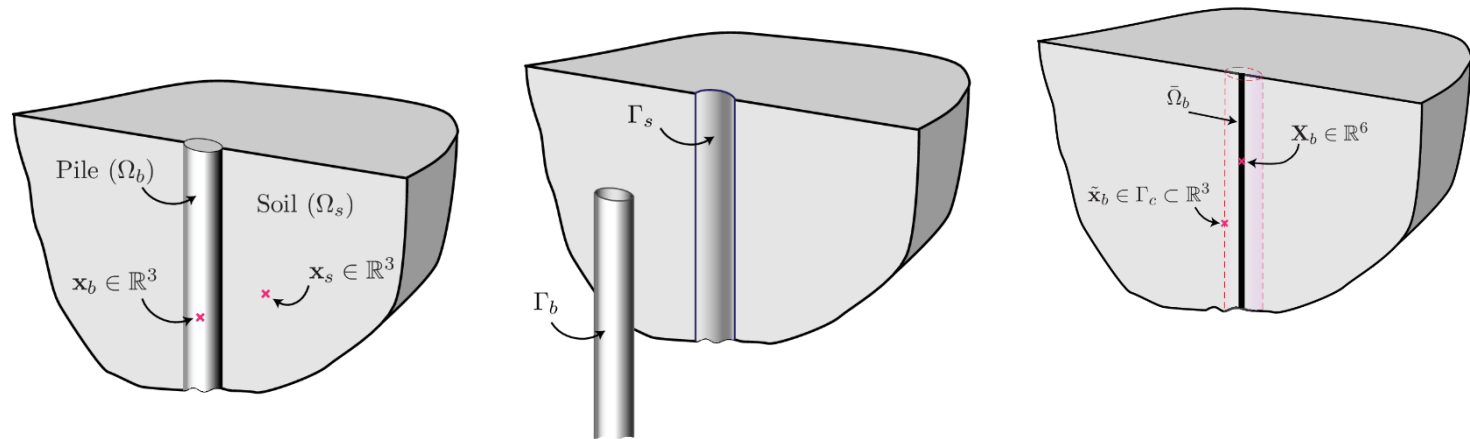
Embedded beam element



Embedded beam element  
with interface surface

# Embedded Elements

## Perfect Bonding Condition



Perfect bonding condition:  $\tilde{\mathbf{x}}_b(\gamma) - \tilde{\mathbf{x}}_s(\gamma) = 0 \quad \forall \gamma \in \Gamma_c, \forall t$

This constraint between the soil and an imaginary surface forms the fundamental component of the embedded element formulation

# Embedded Element

## Perfect Bonding Condition

Point Collocation Method  
(Interaction condition applied in a strong sense)

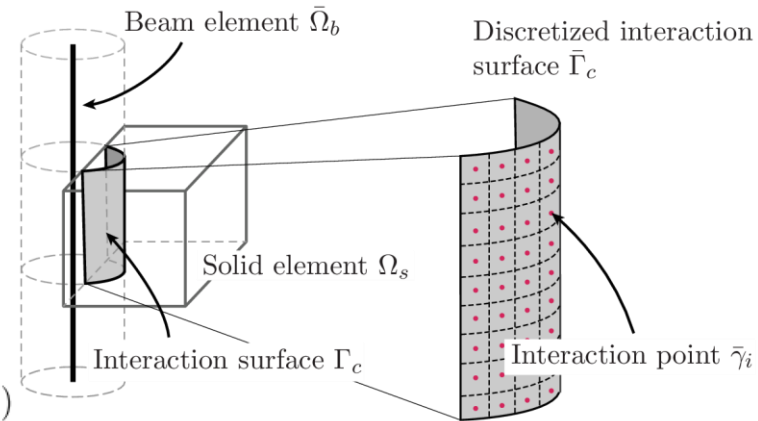
Lagrange Multipliers Method:

$$\delta W^{\text{internal}} = \delta W_{\text{system}}^{\text{internal}} + \underbrace{\sum_{\bar{\gamma} \in \bar{\Gamma}_c} \lambda \cdot (\delta \tilde{\mathbf{x}}_b - \delta \tilde{\mathbf{x}}_s)}_{\text{Virtual work of interaction forces}} + \underbrace{\sum_{\bar{\gamma} \in \bar{\Gamma}_c} \delta \lambda \cdot (\tilde{\mathbf{x}}_b - \tilde{\mathbf{x}}_s)}_{\text{Constraint enforcement}}$$

$\forall$  admissible  $\delta \tilde{\mathbf{x}}_b, \delta \tilde{\mathbf{x}}_s, \delta \lambda$ .

Penalty Method:

$$\delta W^{\text{internal}} = \delta W_{\text{system}}^{\text{internal}} + \sum_i \epsilon_p (\tilde{\mathbf{x}}_b - \tilde{\mathbf{x}}_s) \cdot (\delta \tilde{\mathbf{x}}_b - \delta \tilde{\mathbf{x}}_s) \quad \forall \text{ admissible } \delta \tilde{\mathbf{x}}_b, \delta \tilde{\mathbf{x}}_s$$





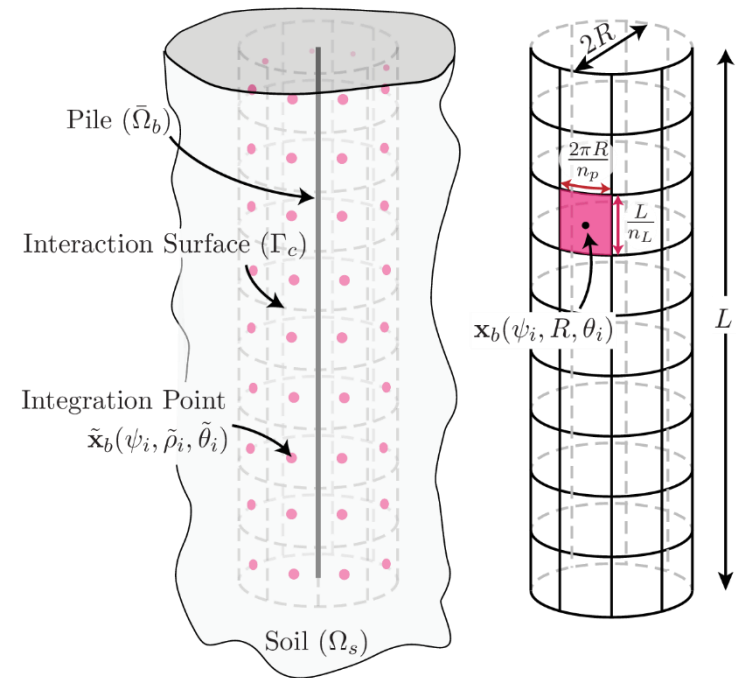
# Embedded Element (mortar)

## Perfect Bonding Condition

Mortar Method

(Interaction condition applied in a weak sense)

$$\int_{\Gamma_c} \lambda(\gamma) \cdot (\tilde{\mathbf{x}}_b(\gamma) - \tilde{\mathbf{x}}_s(\gamma)) \, d\gamma = 0 \quad \forall t$$



Embedded Beam-Solid Interface element currently available in OpenSees (3.6.0)

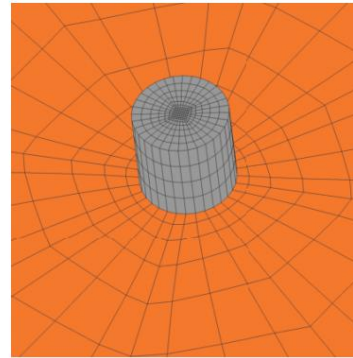
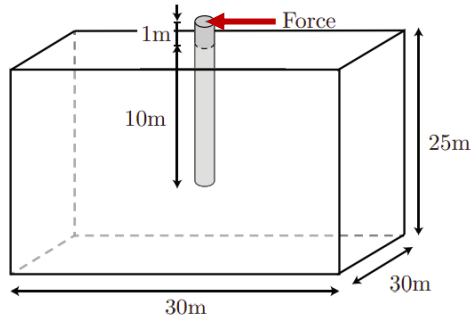


# Quasi Static Example

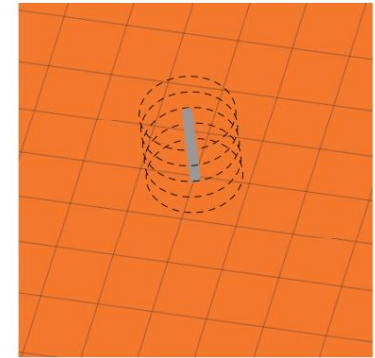


# Embedded Element

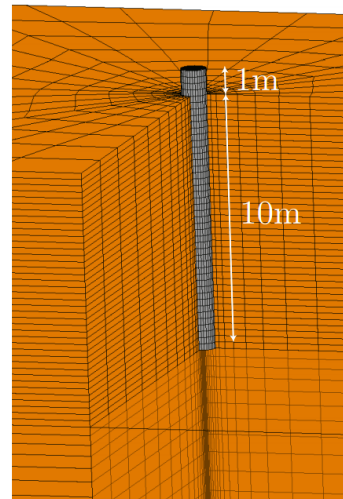
## Laterally loaded pile



3D Solid



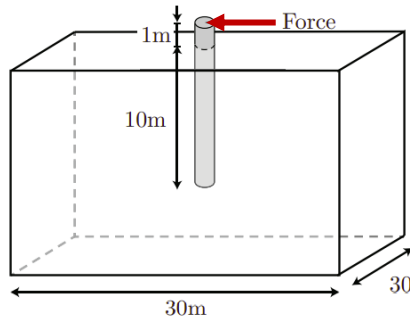
Embedded Interface



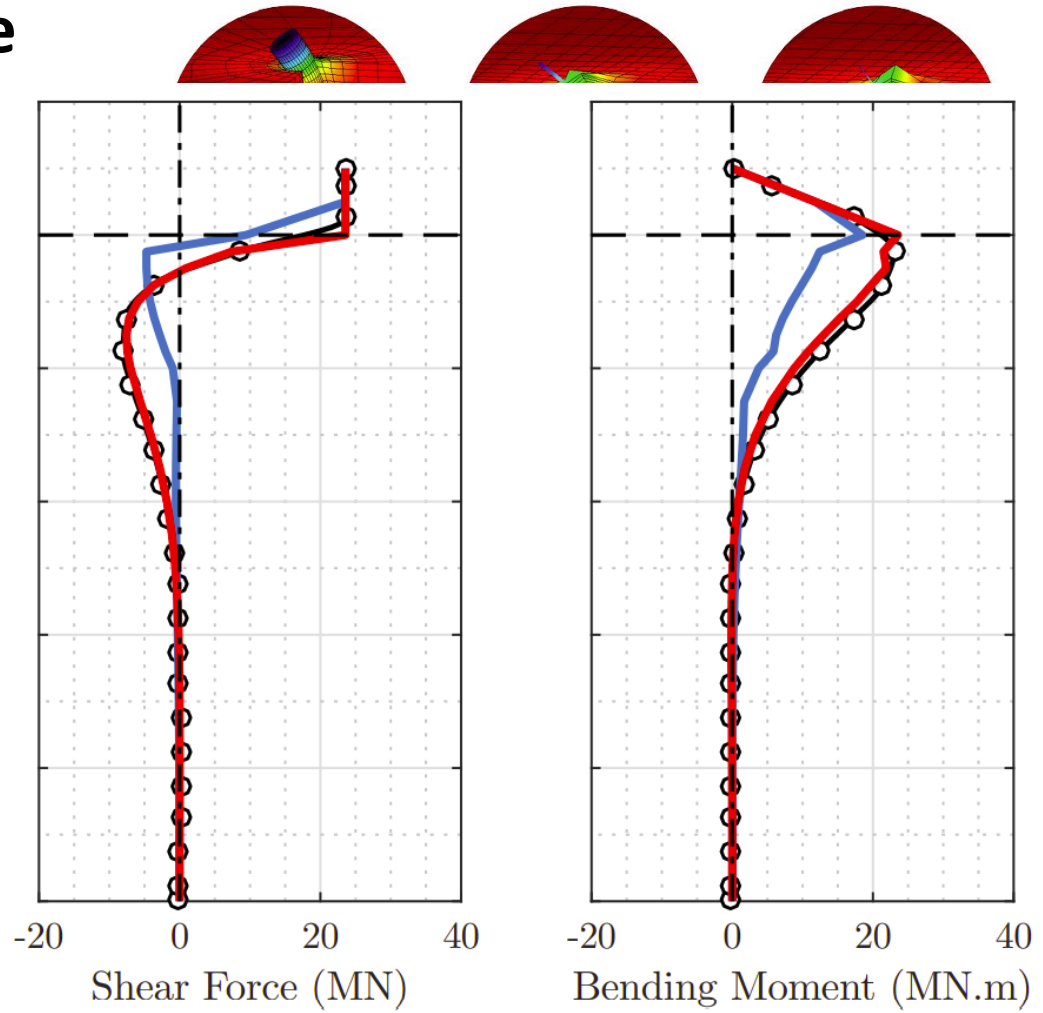
Close-up View of the Mesh

# Embedded Element

## Laterally loaded pile

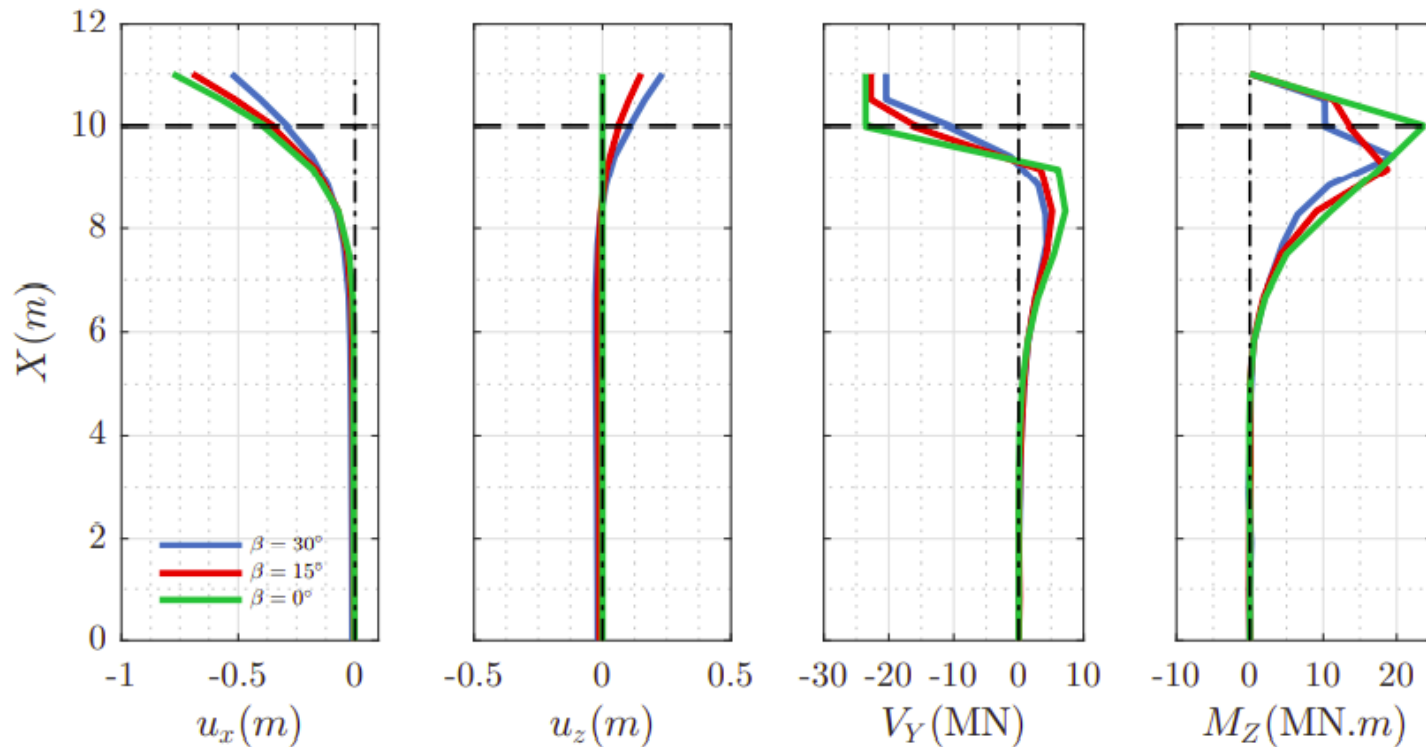
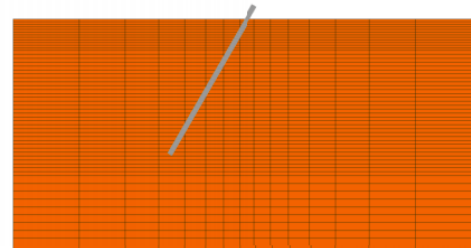
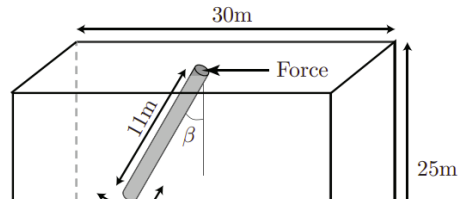


- Full 3D Model
- Strong Form
- Mortar/Weak Form



# Embedded Element

## Battered pile response





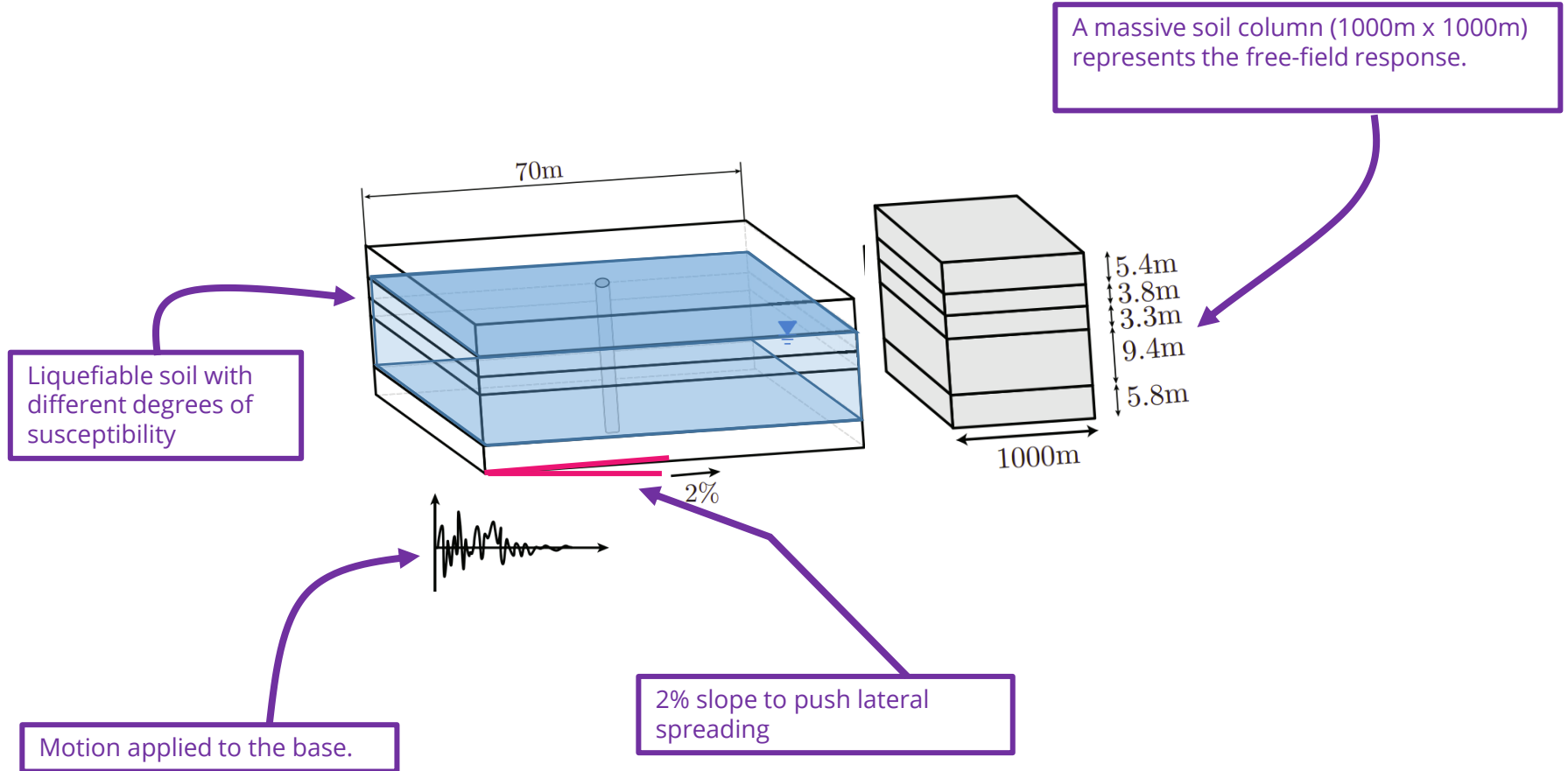
# Dynamic Example





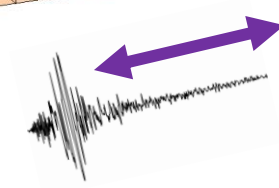
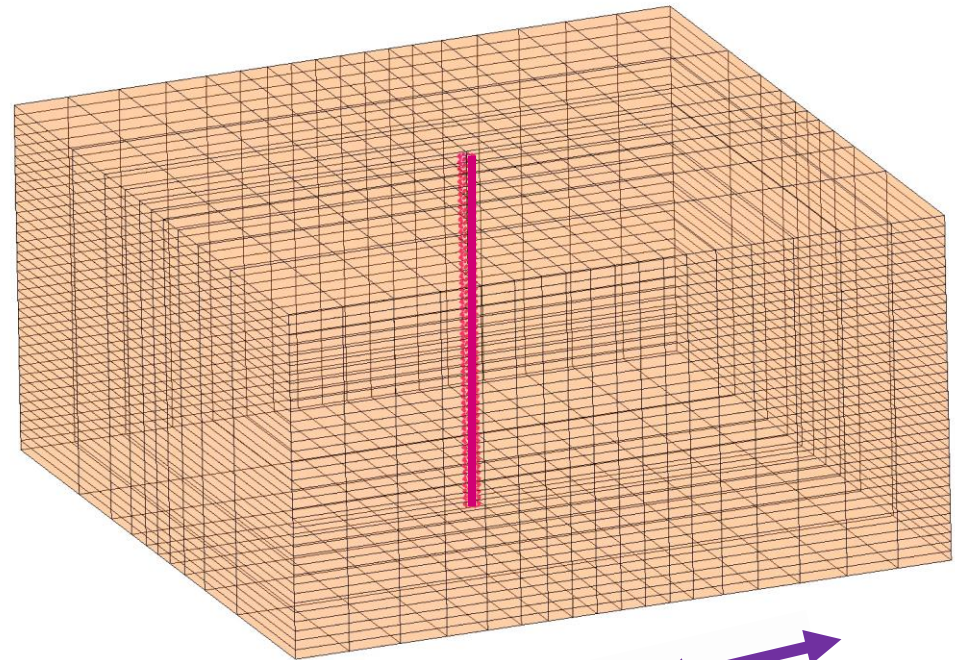
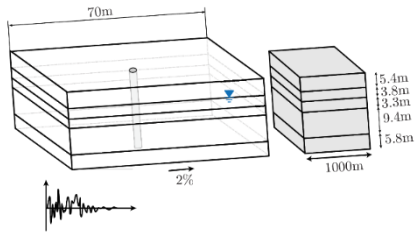
# Dynamic Examples

## Lateral Spreading



# Dynamic Examples

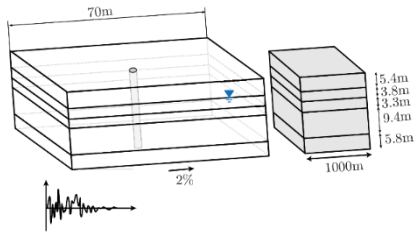
## Lateral Spreading



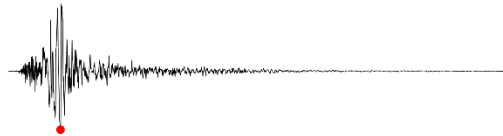
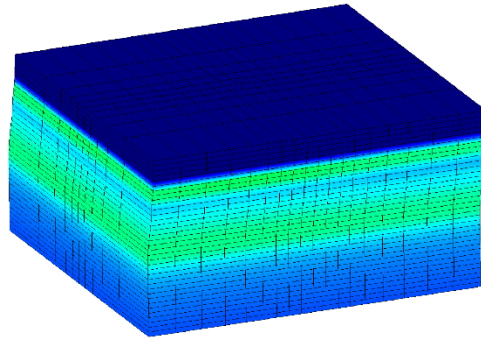
**Soil-Pile interaction  
compatible displacement**

# Dynamic Examples

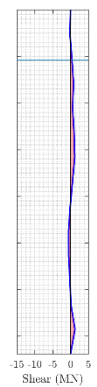
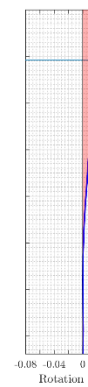
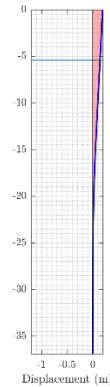
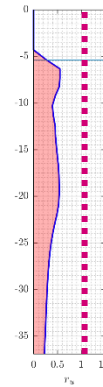
## Lateral Spreading



$t \approx 4 \text{ s}$

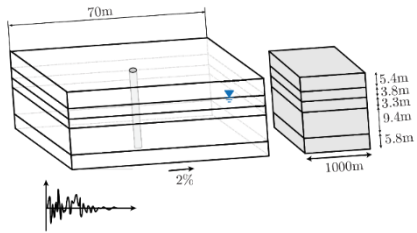


Excess PWP Ratio ( $r_u = \frac{u_{\text{excess}}}{\sigma_{v0}}$ )

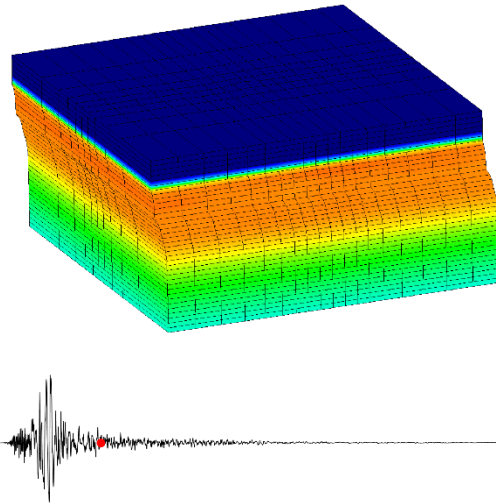


# Dynamic Examples

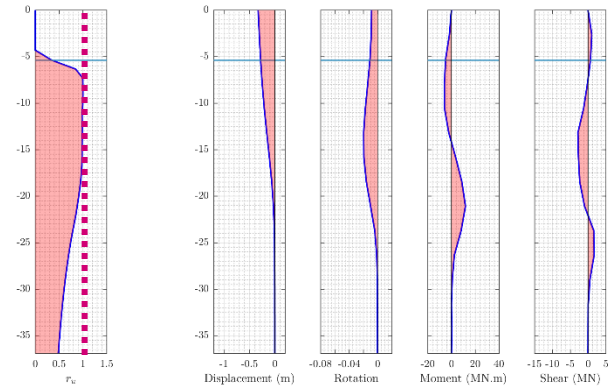
## Lateral Spreading



$t \approx 8 \text{ s}$

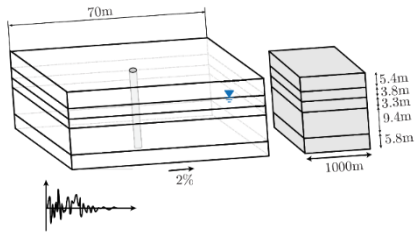


Excess PWP Ratio ( $r_u = \frac{u_{\text{excess}}}{\sigma_{v0}}$ )

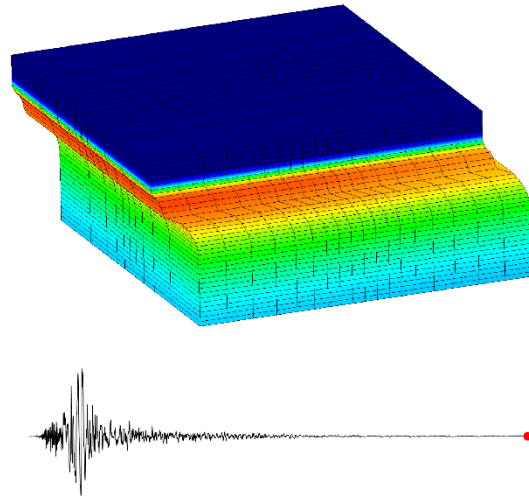


# Dynamic Examples

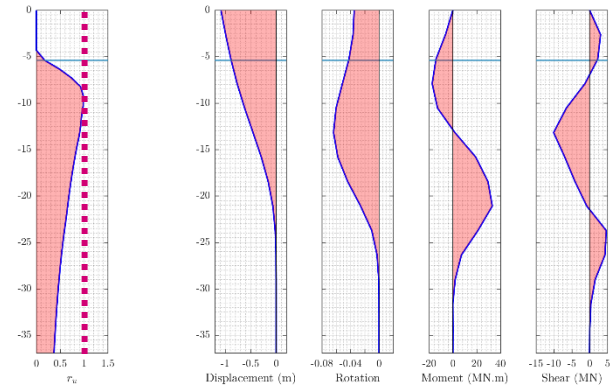
## Lateral Spreading



$t \approx 40 \text{ s}$



Excess PWP Ratio ( $r_u = \frac{u_{\text{excess}}}{\sigma_{v0}}$ )

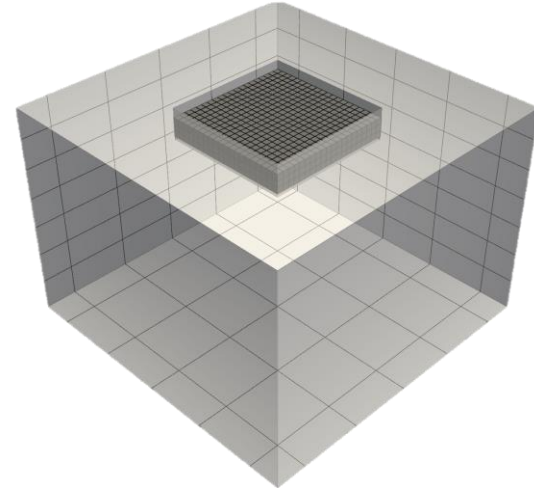
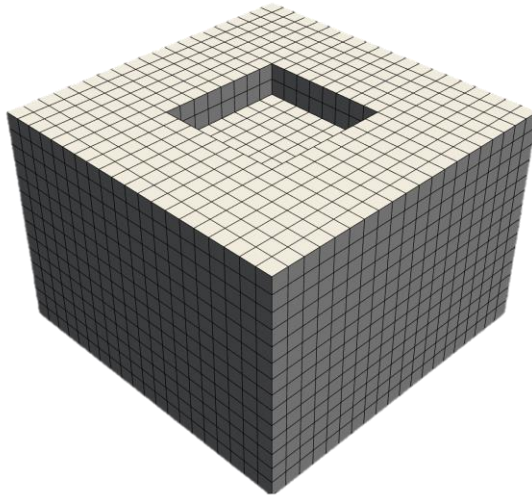




# Building Foundation

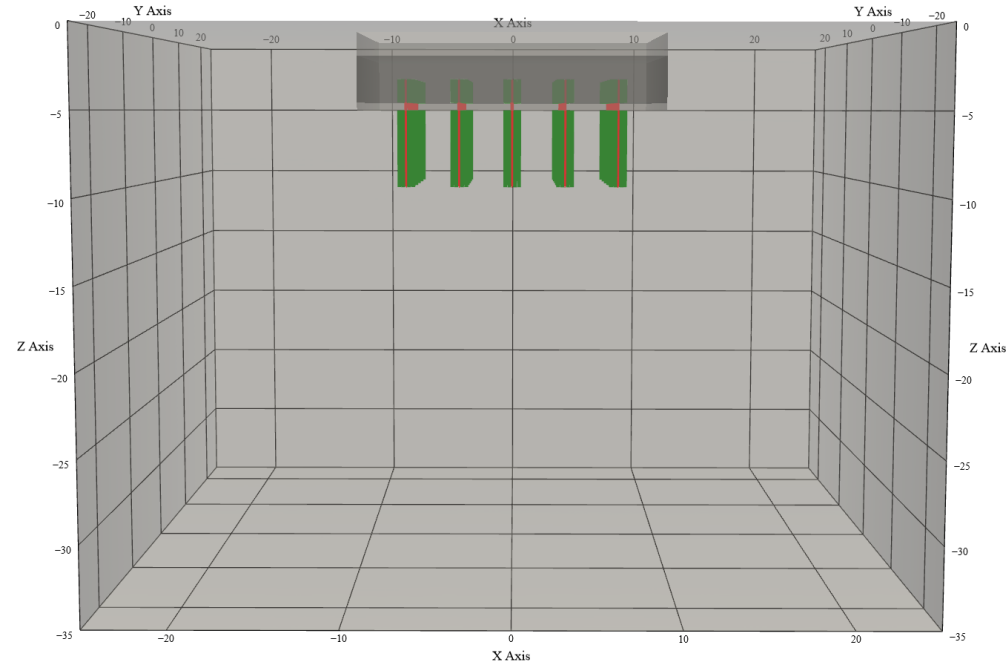
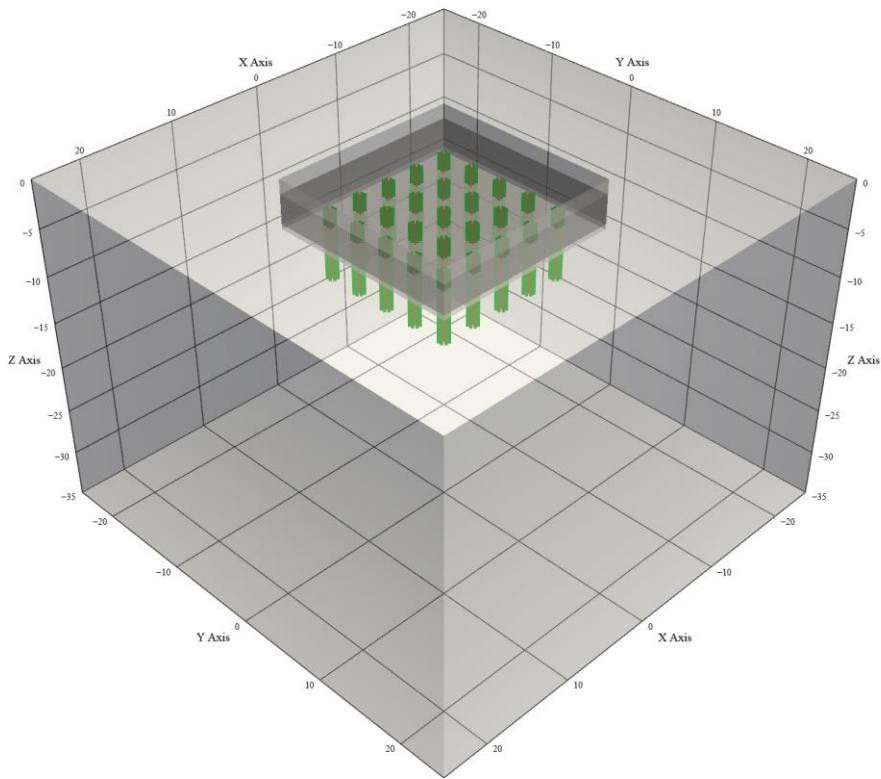


# Building Foundation

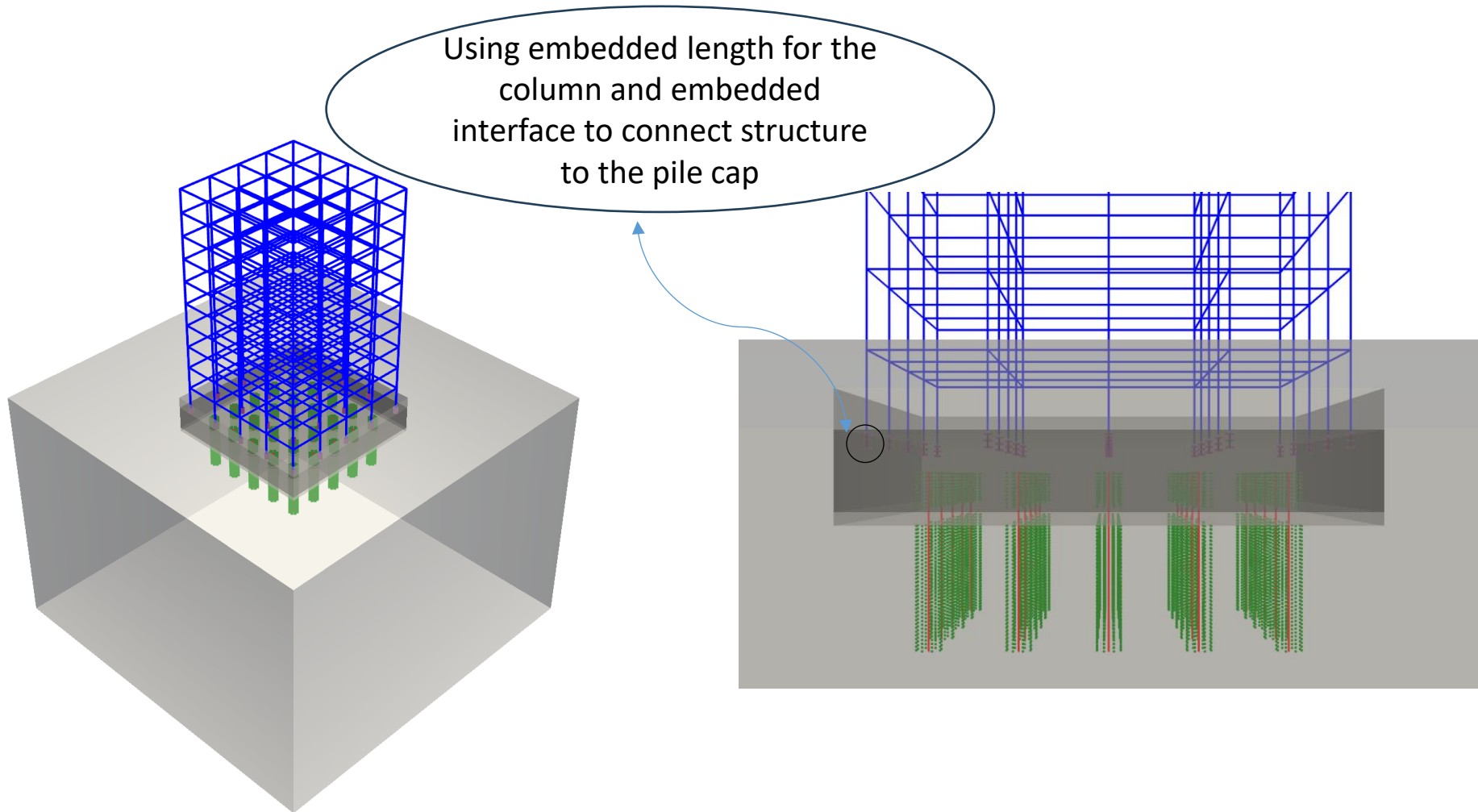




# Building Foundation Mat on pile foundation

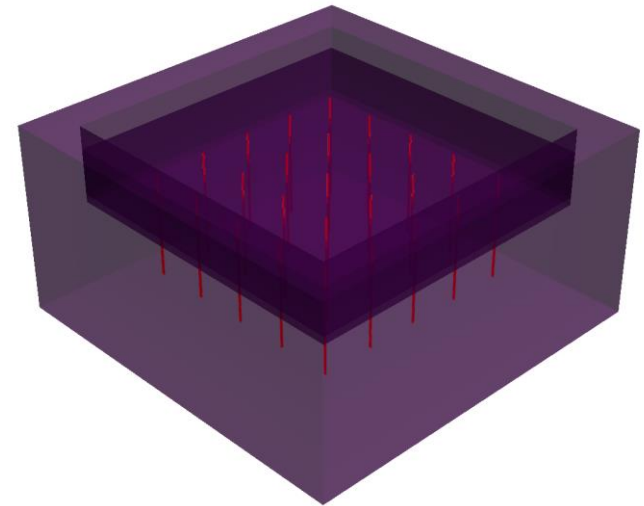
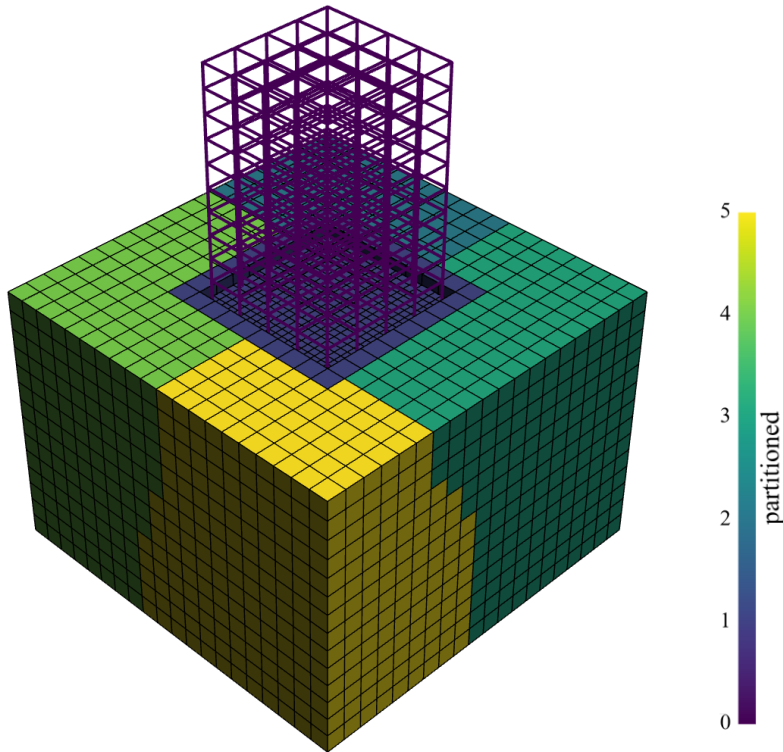


# Building Foundation Structure connection



# Building Foundation

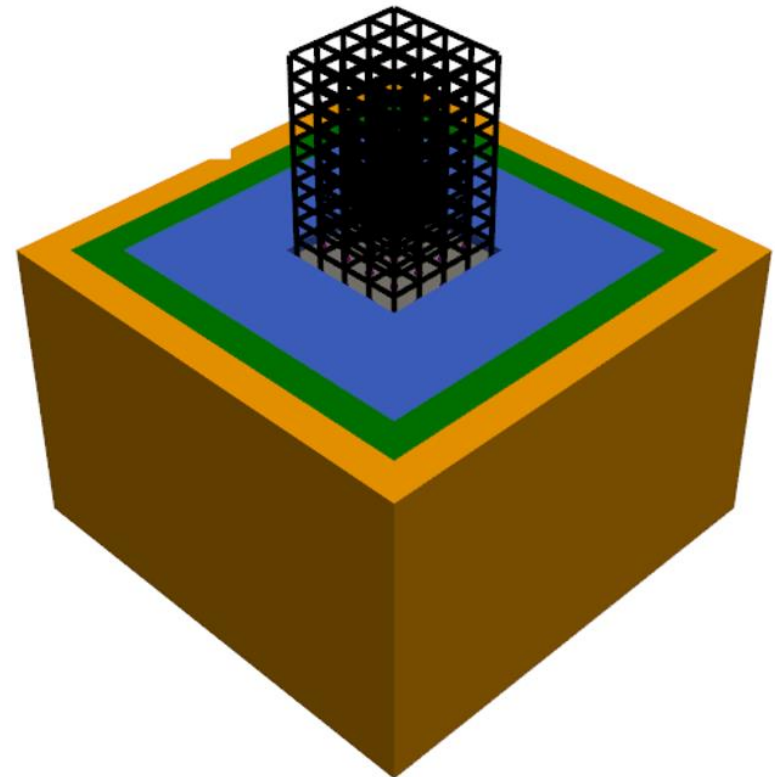
## Distributed computing



The only challenge is that the interface nodes and their associated brick elements should be kept on a same processor in parallel processing analysis

# Building Foundation Dynamic analysis

- Structure
- Soil Layer
- Foundation
- Domain Reduction Layer
- Perfectly Matched Layer





# Concluding Remarks

- **Soil Structure Interaction (SSI) analysis continues to be an important and challenging problem to tackle numerically.**
- **Conventional and embedded contact formulations useful to represent SSI.**
- **Mortar embedded interface element effectively applies the interaction condition.**
- **Preliminary results show the potential of the proposed embedded element implemented in OpenSees.**
- **Future work includes more validation and verification studies, and simulation of complex building and bridge foundation systems.**



Thank you!!