



ASCE-41 Evaluation of a Reinforced-Concrete Building Damaged in the 2016 Meinong Earthquake

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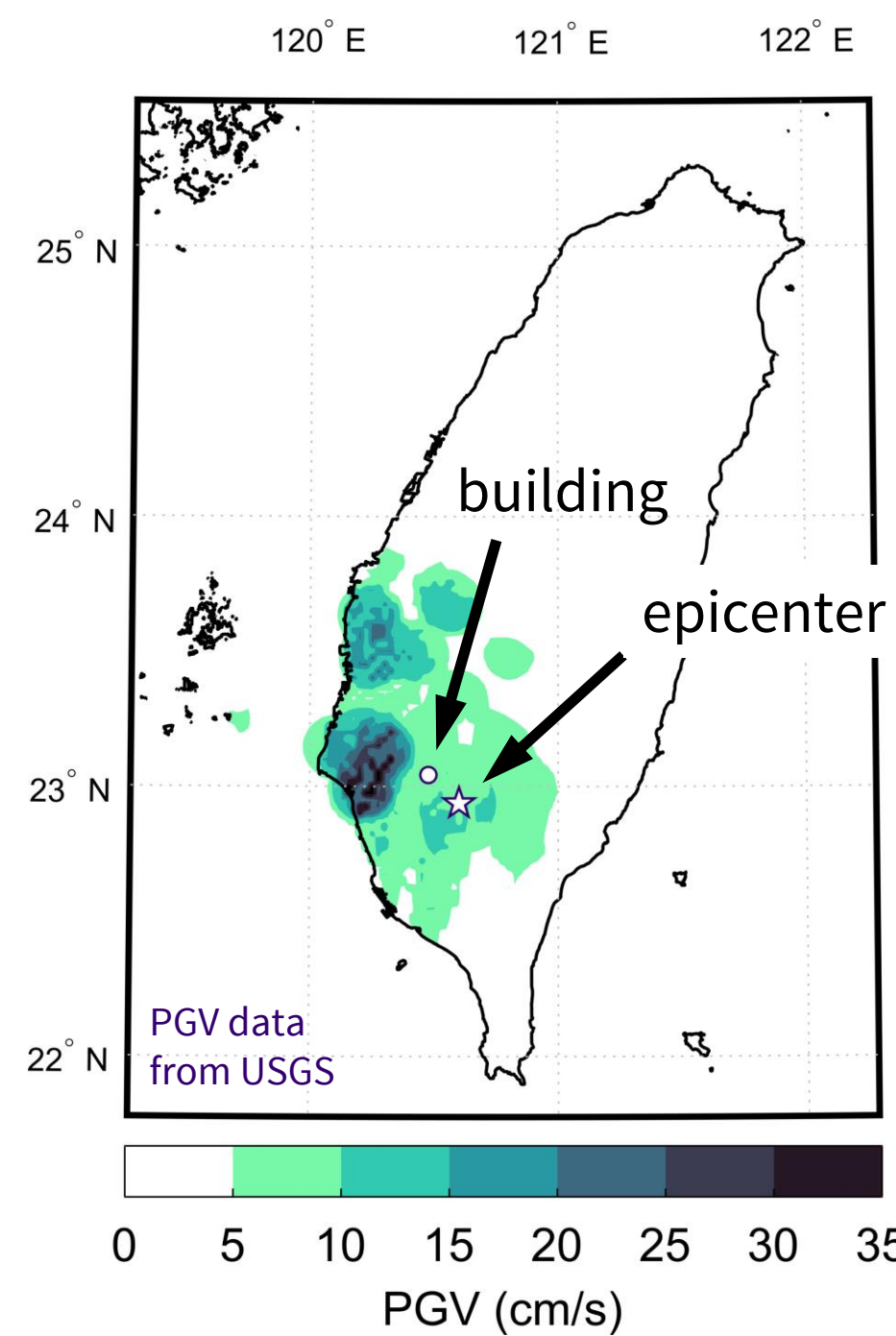
University of Washington – ATC-134 Project



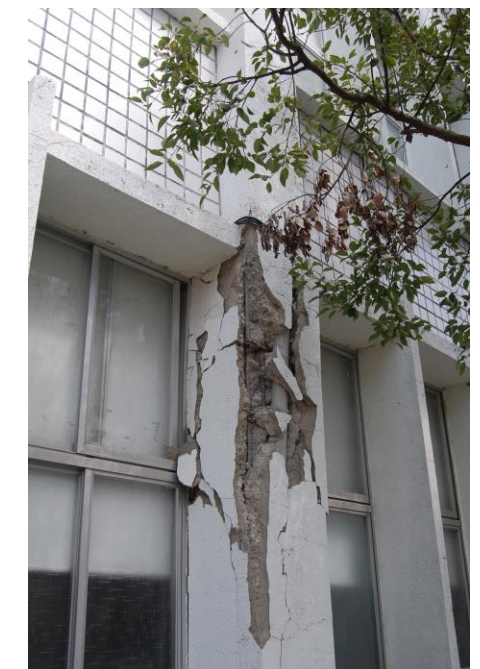
MOTIVATION AND OBJECTIVES

- > Effectiveness of current seismic performance evaluation procedures to identify structural deficiencies and predict damage is largely unknown
- > Primary objective: Benchmark ASCE 41-17 seismic performance evaluation procedures using a case-study building
- > Secondary objective: Develop new, robust approaches for implementing ASCE 41-17 modeling recommendations

EARTHQUAKE BACKGROUND AND OBSERVED DAMAGE

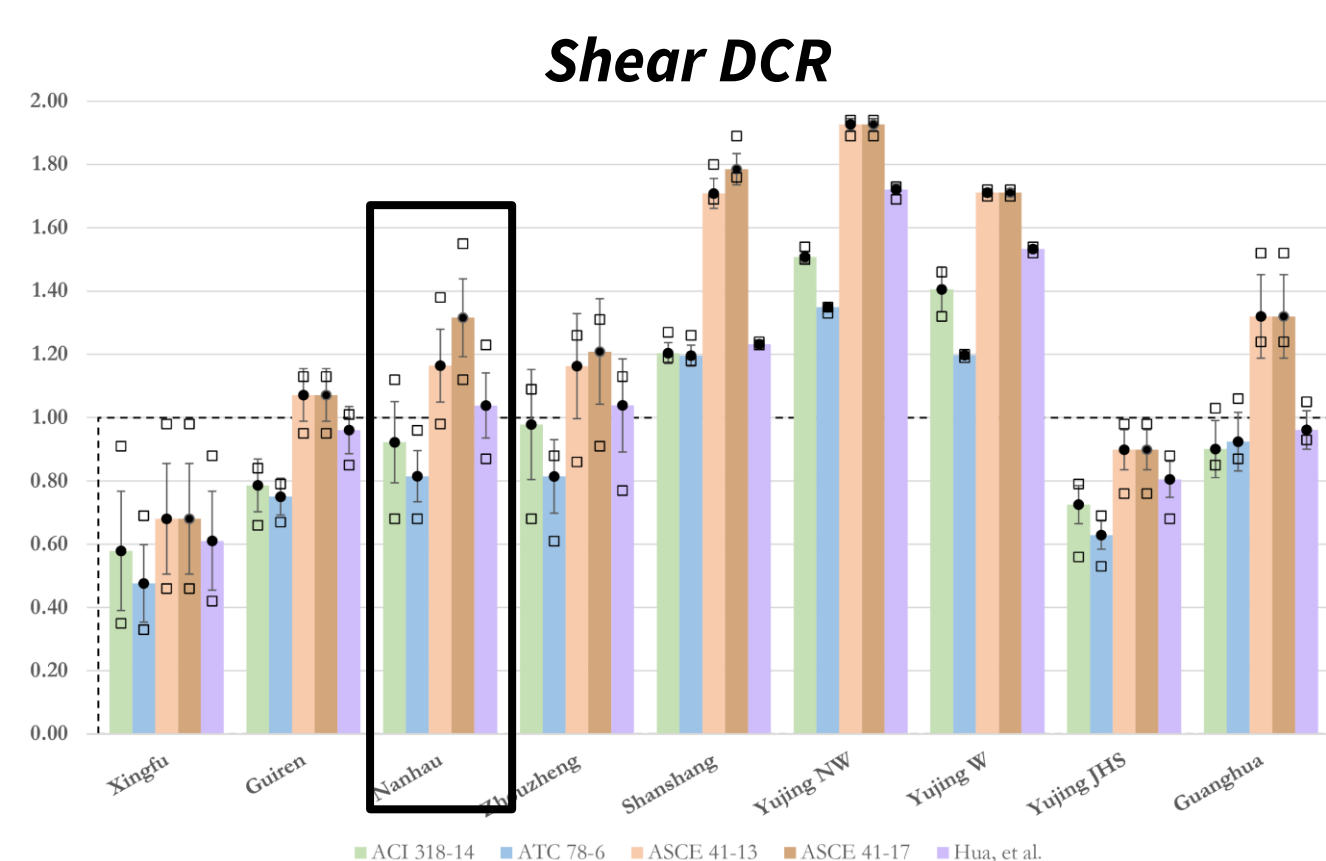


- > M6.4 earthquake occurred in southern Taiwan near the city of Tainan on February 6, 2016
- > Significant damage to reinforced-concrete buildings, particularly moment-resisting frames with masonry infill
 - > Several major collapses
 - > 3 district offices damaged, including Nanhua District Office (1967):



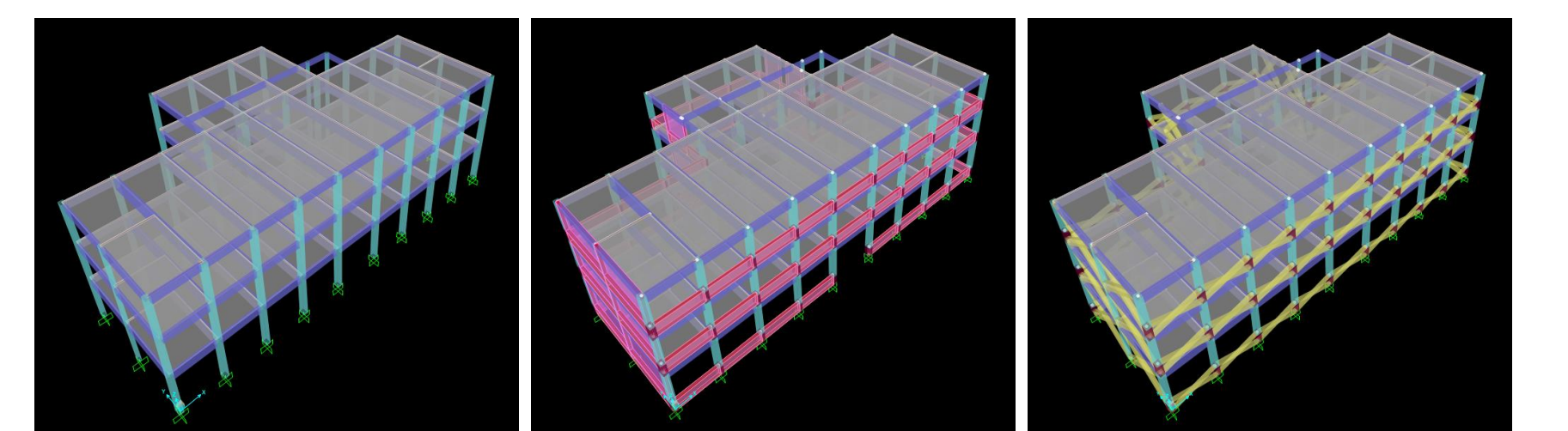
TIER 1 SCREENING

- > Checklist-based approach to determine if further evaluation is required
- > Typical deficiencies in damaged building stock:
 - > Column shear stress demand
 - > Strong column-weak beam condition
 - > Column-tie spacing

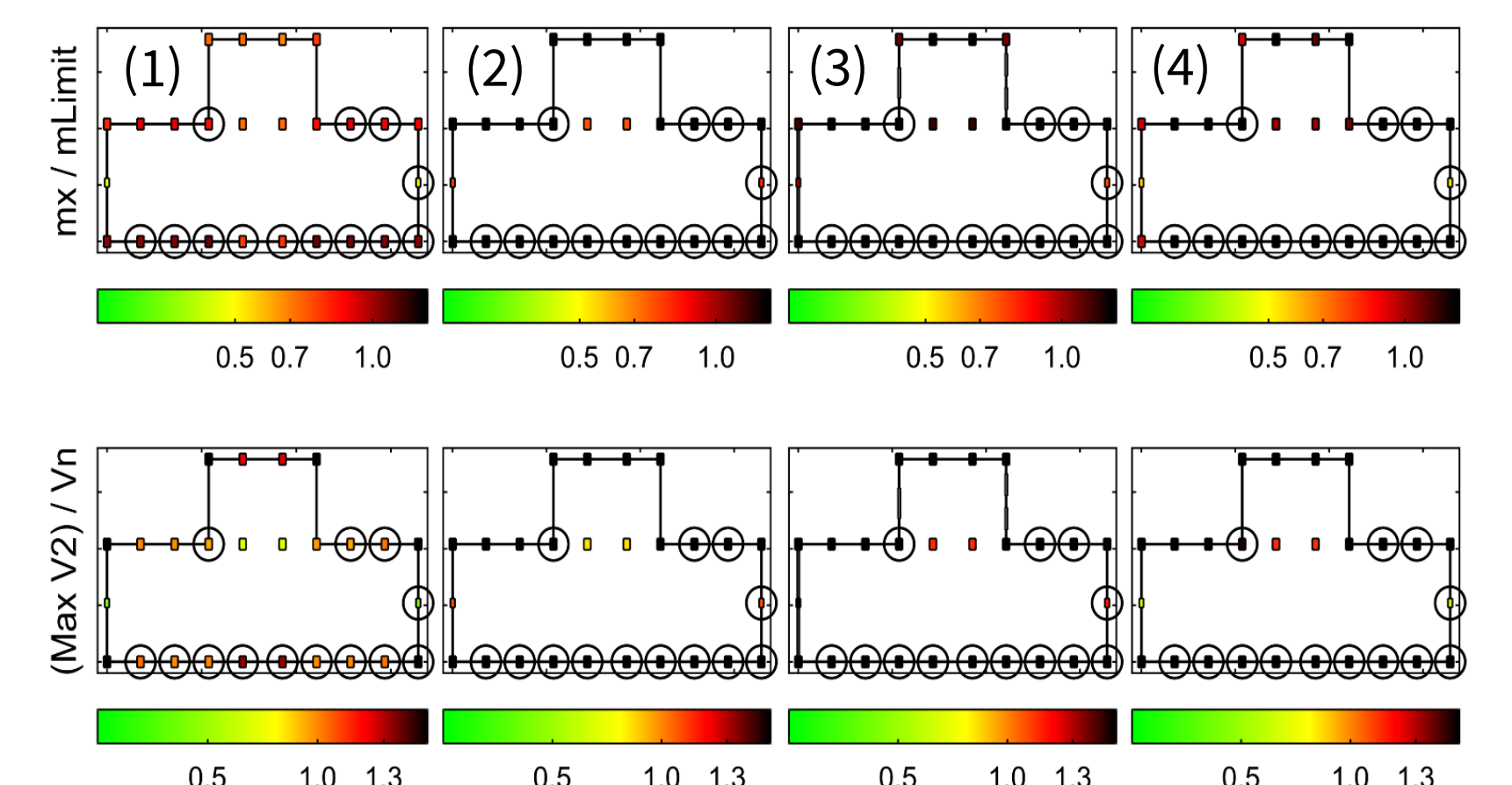
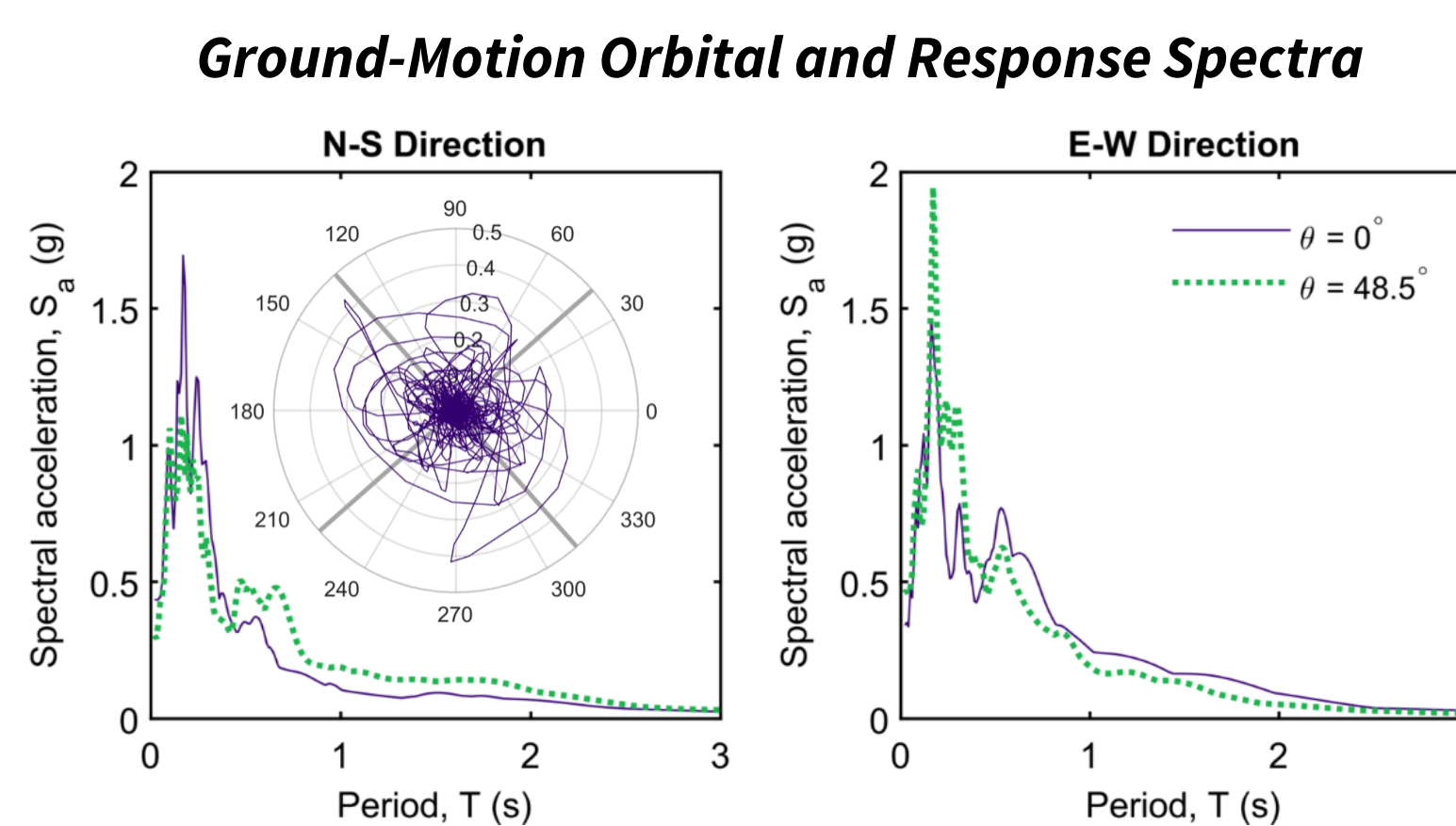


TIER 3 LINEAR-DYNAMIC EVALUATION

- > Analyses performed in SAP2000 using four model variations
- > Ground motion is closest to building and captures forward-directivity effects
- > Results:
 - > Variation in response of models is not significant
 - > Predicted damage modes inconsistent with observations

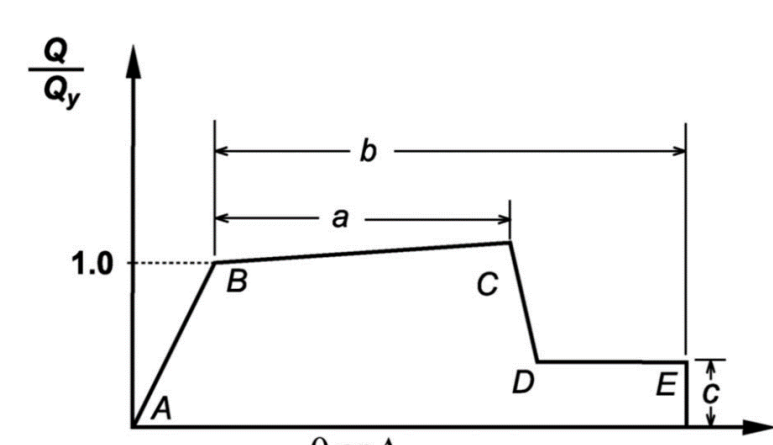


(1) Bare frame (2) Infill offsets (3) Infill Shell elements (4) Infill diagonal struts



TIER 3 NONLINEAR-DYNAMIC EVALUATION

- > ASCE-41 backbone curve represents column plastic-hinge moment-rotation behavior including degradation due to shear or flexure-shear failure modes



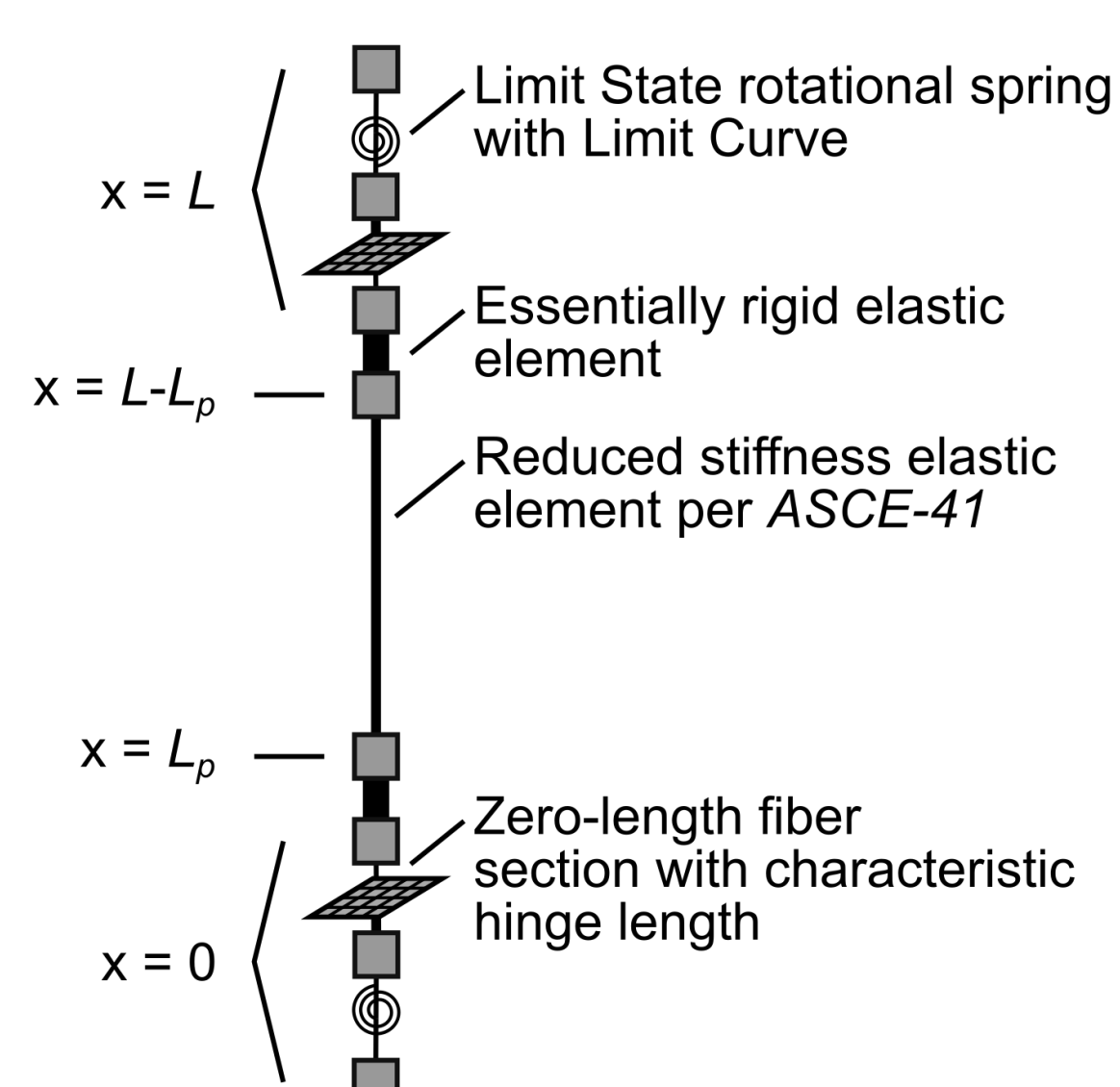
IO 0.15a
LS 0.5b
CP 0.7b

Parameter	Expression
a (rad)	$0.042 - 0.043 \frac{N_{UD}}{A_g f'_{CE}} + 0.63 \rho_t - 0.023 \frac{V_{yE}}{V_{colOE}} \geq 0.0$
b (rad)	$0.5 \left(5 + \frac{N_{UD}}{A_g f'_{CE}} \frac{1}{\rho_t} \frac{f'_{CE}}{f_{yt}} \right) - 0.01 \geq a$
c	$0.24 - 0.4 \frac{N_{UD}}{A_g f'_{CE}} \geq 0.0$

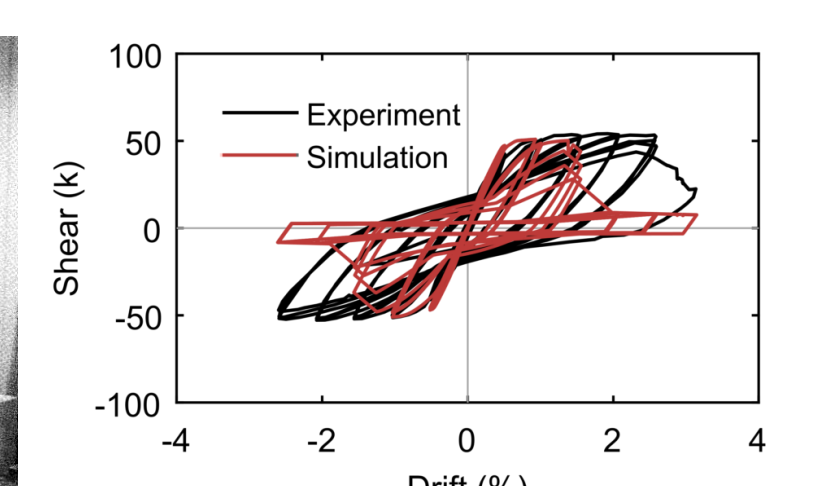
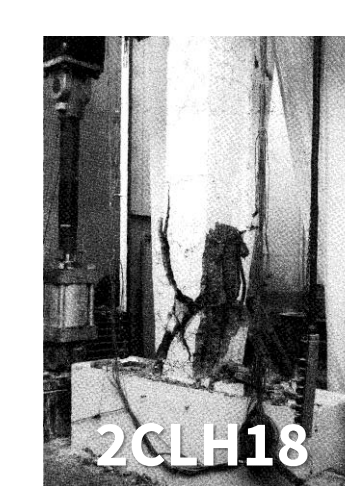
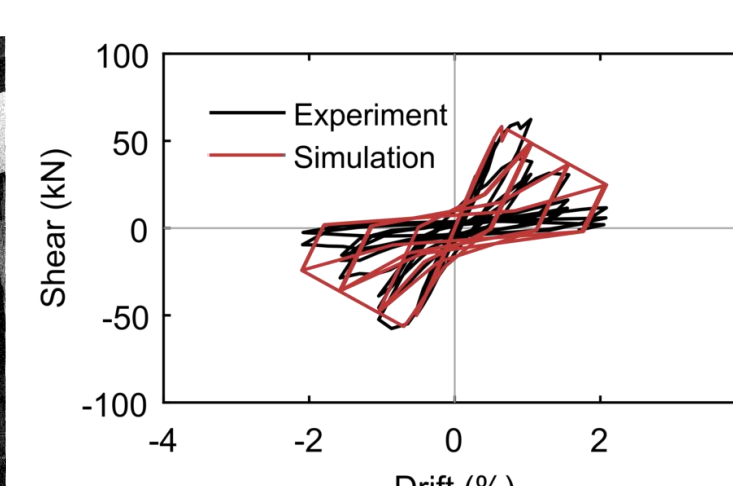
Highlighting indicates time-dependent variables

- > New rotation limit curve developed in OpenSees after Elwood [1] to allow for use of fiber sections while complying with ASCE 41-17

Beam-Column Element Assembly



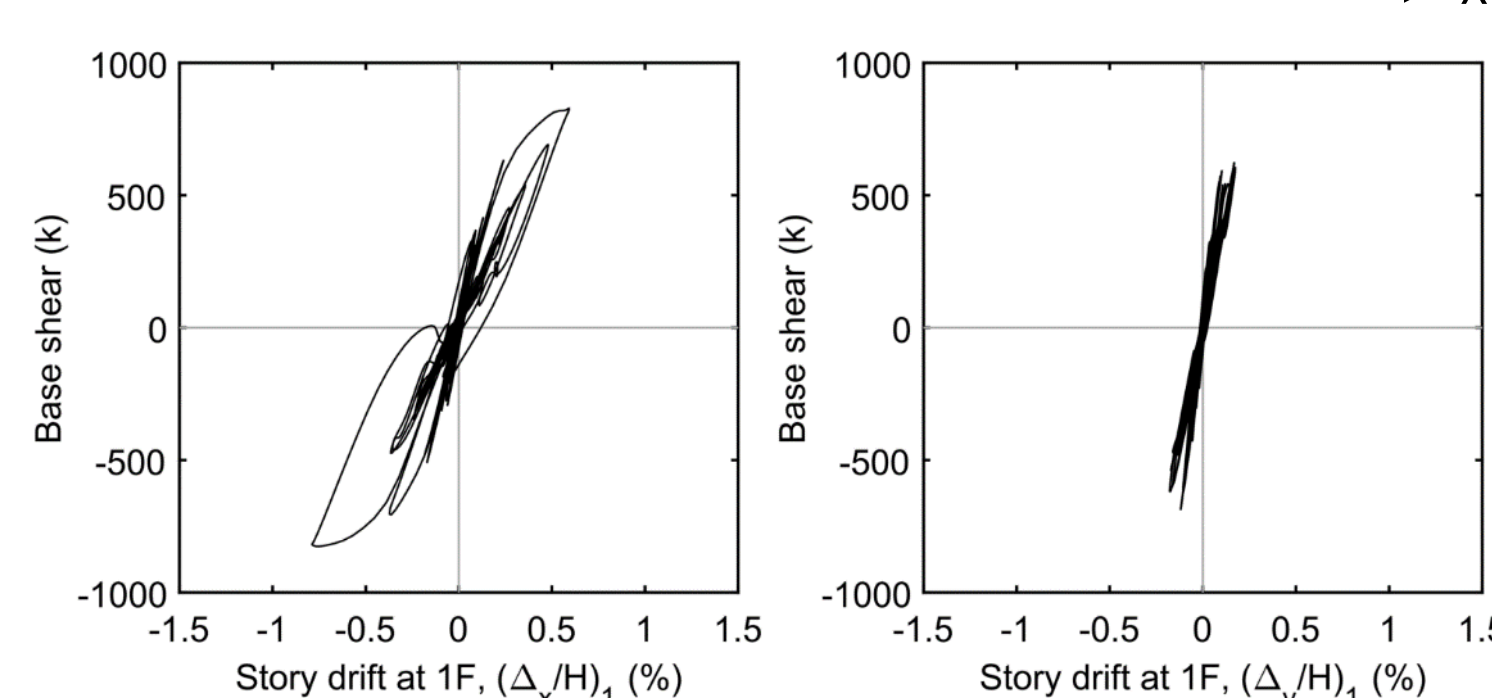
- > Model validation using column tests from Lynn et al. [1]



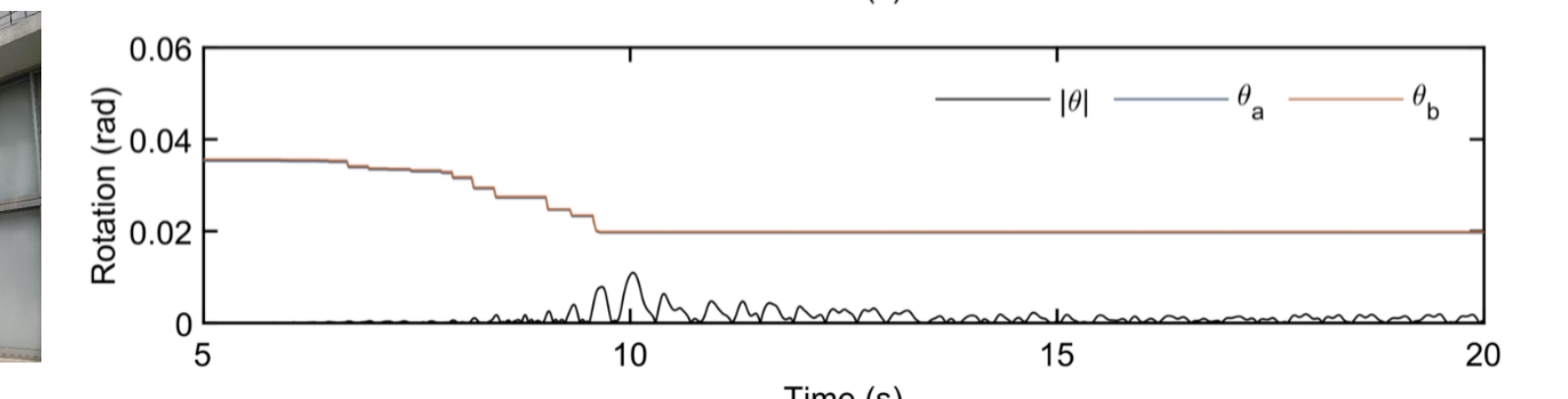
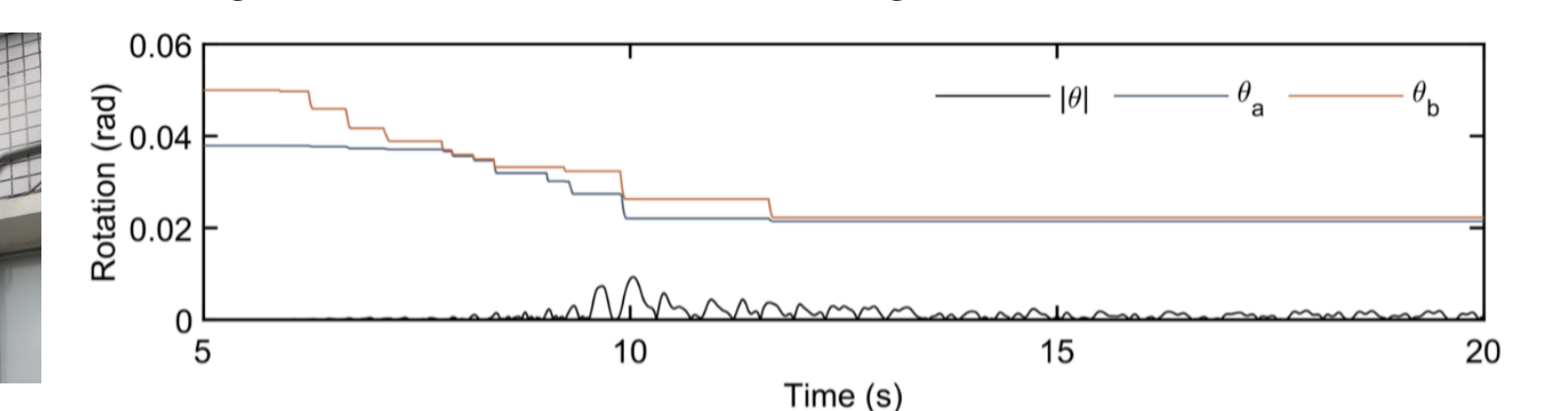
- > Results:

- > Columns yield but do not sustain shear or flexure-shear degradation
- > Acceptance criteria for life safety exceeded in several cases
- > In contrast to linear analysis but in concert with post-earthquake reconnaissance, predicted damage only in longitudinal (X) direction of building

First-Story Hysteretic Response



Hinge Rotation and Modeling Parameter Evolution



REFERENCES

- [1] Elwood, K. J. (2004). "Modelling failures in existing reinforced concrete columns." *Canadian Journal of Civil Engineering*, 31, 846-859.
- [2] Lynn, A. C., Moehle, J. P., Mahin, S. A., and Holmes, W. T. (1996). "Seismic evaluation of existing reinforced concrete building columns." *Earthquake Spectra*, 12(4), 715-739.

ACKNOWLEDGMENTS

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