

Bayesian Inference for Mechanics-Based Digital Twinning of Bridges

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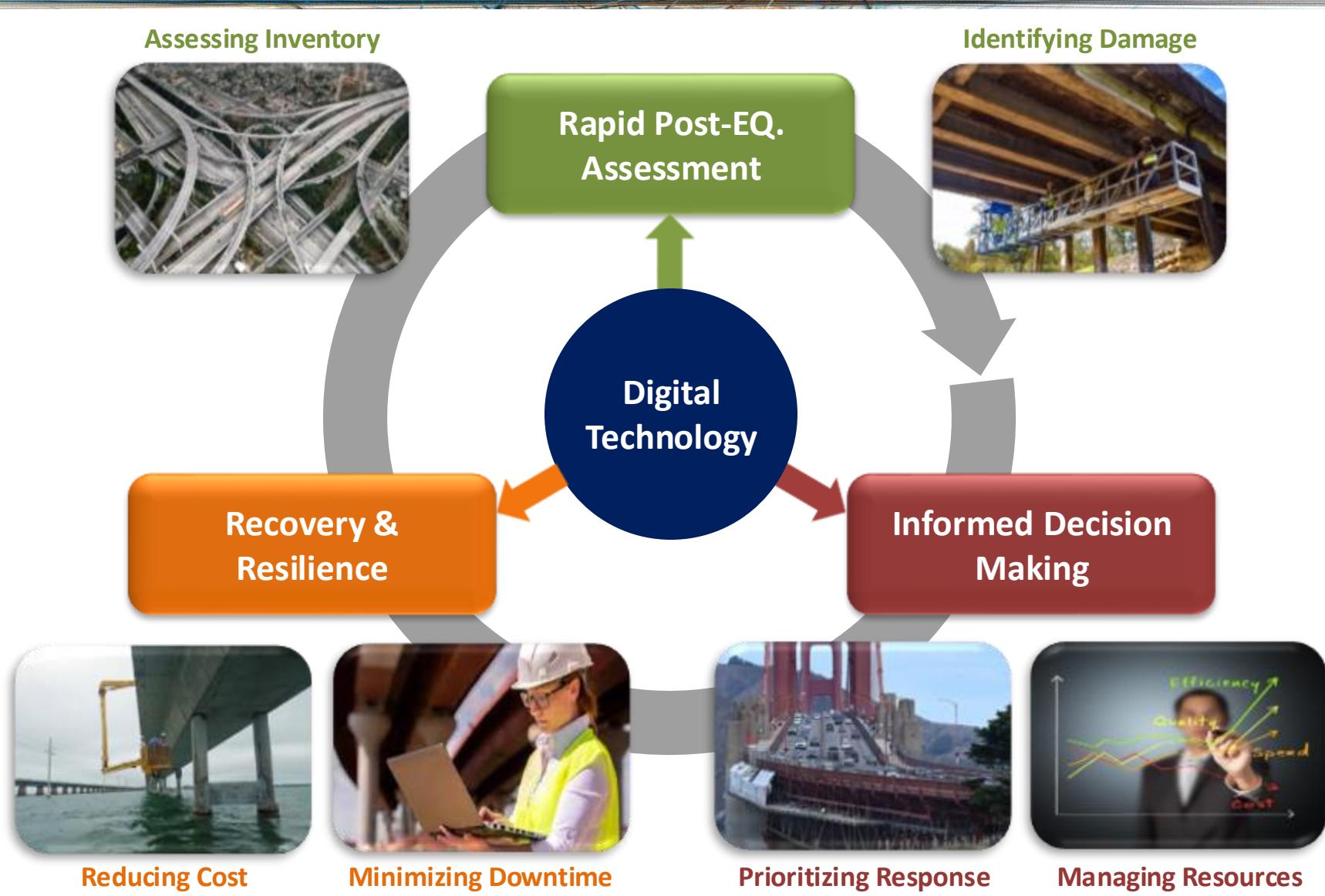
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Digital Technology for Infrastructure Monitoring



Available Post-Earthquake Monitoring Solutions

Visual Inspection

- # of bridges × inspection time × chaos
- Inspection complexity
- Hidden damage
- No system-level insight



Modal-Based SID

- Limited damage localization & quantification
- Based on ambient/ low-amplitude records



ShakeCast (USGS)

- Intensity-based metrics can be inaccurate!
- No/Limited damage localization & quantification

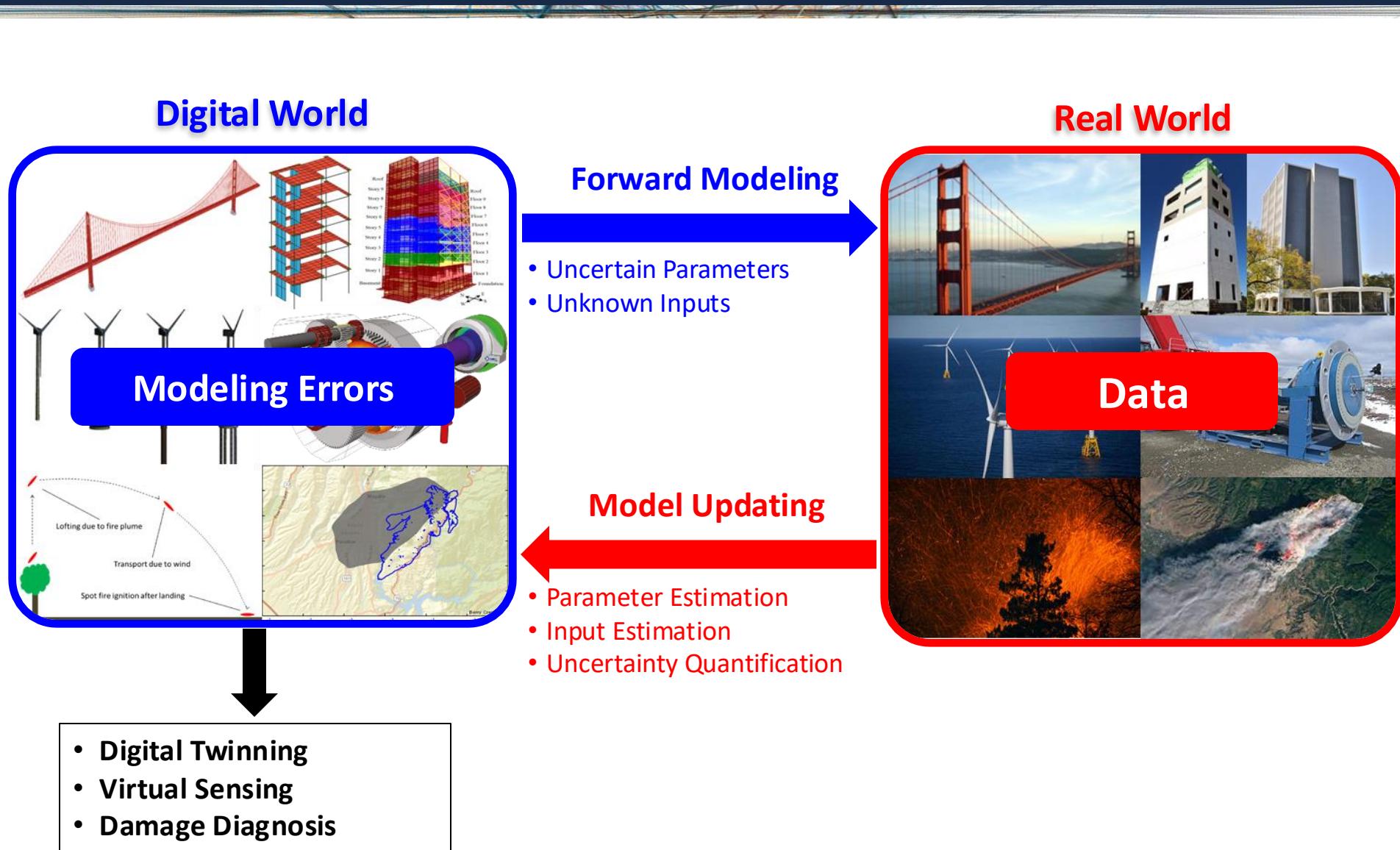


Point Monitoring

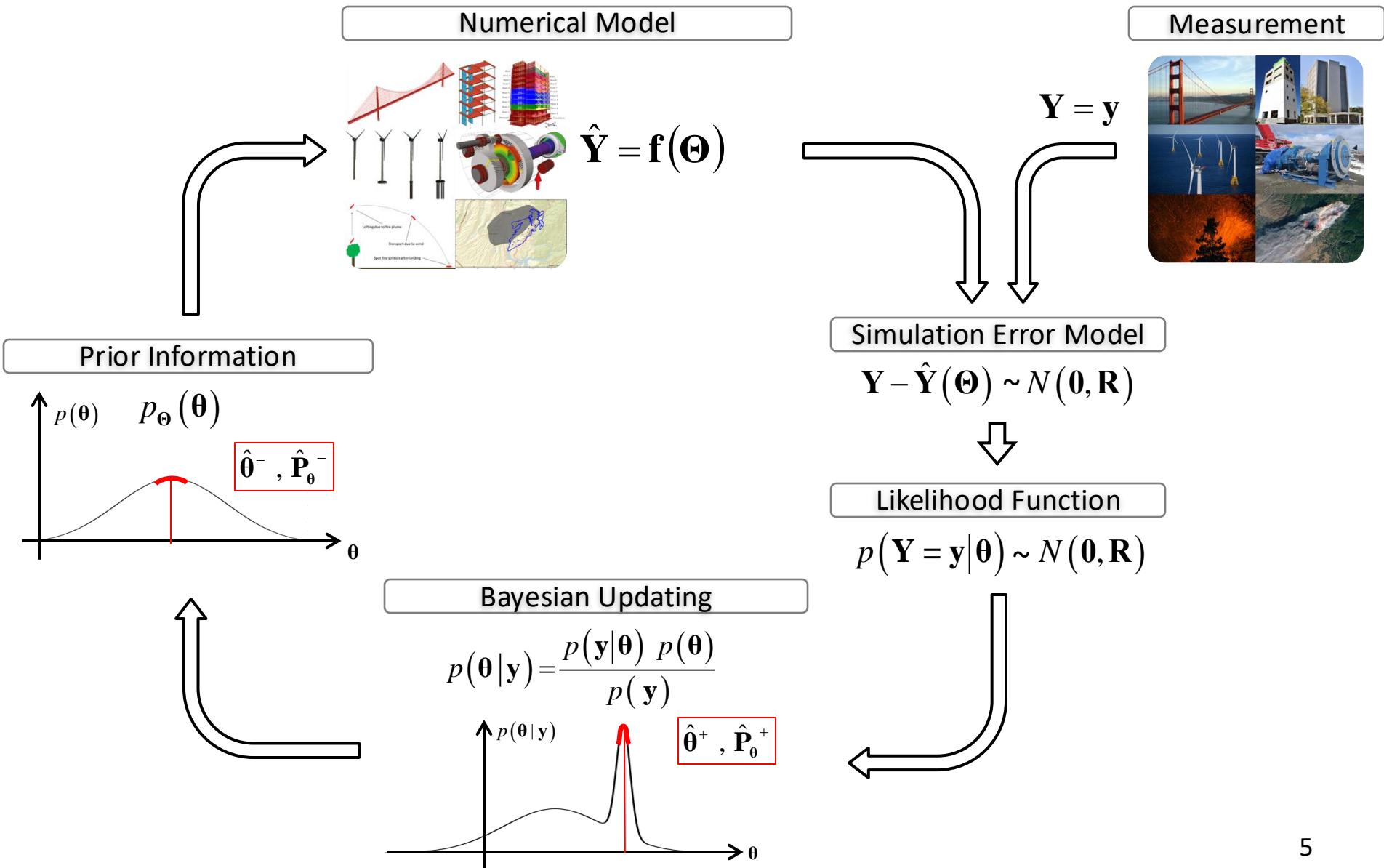
- Data not information!
- Require large number of sensors
- Maintenance and installation cost
- No system-level insight



Time-Domain Mechanics-based Model Updating



Bayesian Model Updating



First-Order Approximation: Kalman Filtering

Numerical Model

$$\hat{y} = \mathbf{f}(\hat{\theta}^-)$$

$$\hat{\mathbf{P}}_y = \left(\frac{\partial \mathbf{f}(\theta)}{\partial \theta} \Big|_{\theta=\hat{\theta}^-} \right) \hat{\mathbf{P}}_\theta \left(\frac{\partial \mathbf{f}(\theta)}{\partial \theta} \Big|_{\theta=\hat{\theta}^-} \right)^T$$

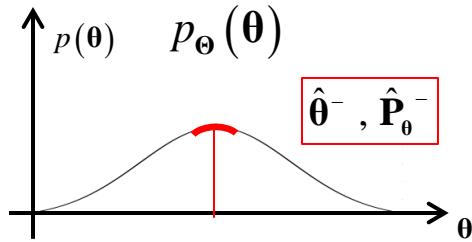
FE Response Sensitivity Matrix

Measurement

$$\mathbf{Y} = \mathbf{y}$$



Prior Information



Simulation Error Model

$$\mathbf{Y} - \hat{\mathbf{Y}}(\boldsymbol{\theta}) \sim N(\mathbf{0}, \mathbf{R})$$



Likelihood Function

$$p(\mathbf{Y} = \mathbf{y} | \boldsymbol{\theta}) \sim N(\mathbf{0}, \mathbf{R})$$

Bayesian Updating

$$p(\boldsymbol{\theta} | \mathbf{y}) = \frac{p(\mathbf{y} | \boldsymbol{\theta}) p(\boldsymbol{\theta})}{p(\mathbf{y})}$$

$$\frac{\partial p(\boldsymbol{\theta} | \mathbf{y})}{\partial \boldsymbol{\theta}} = 0 \Rightarrow \begin{cases} \hat{\boldsymbol{\theta}}^+ = \hat{\boldsymbol{\theta}}^- + K (\hat{\mathbf{y}}^+ - \hat{\mathbf{y}}(\hat{\boldsymbol{\theta}}^-)) \\ \hat{\mathbf{P}}_\theta^+ = (\mathbf{C}^T \mathbf{R}^{-1} \mathbf{C} + (\hat{\mathbf{P}}_\theta^-)^{-1})^{-1} \end{cases}$$



Unknown Input Excitation: Output-Only Model Updating

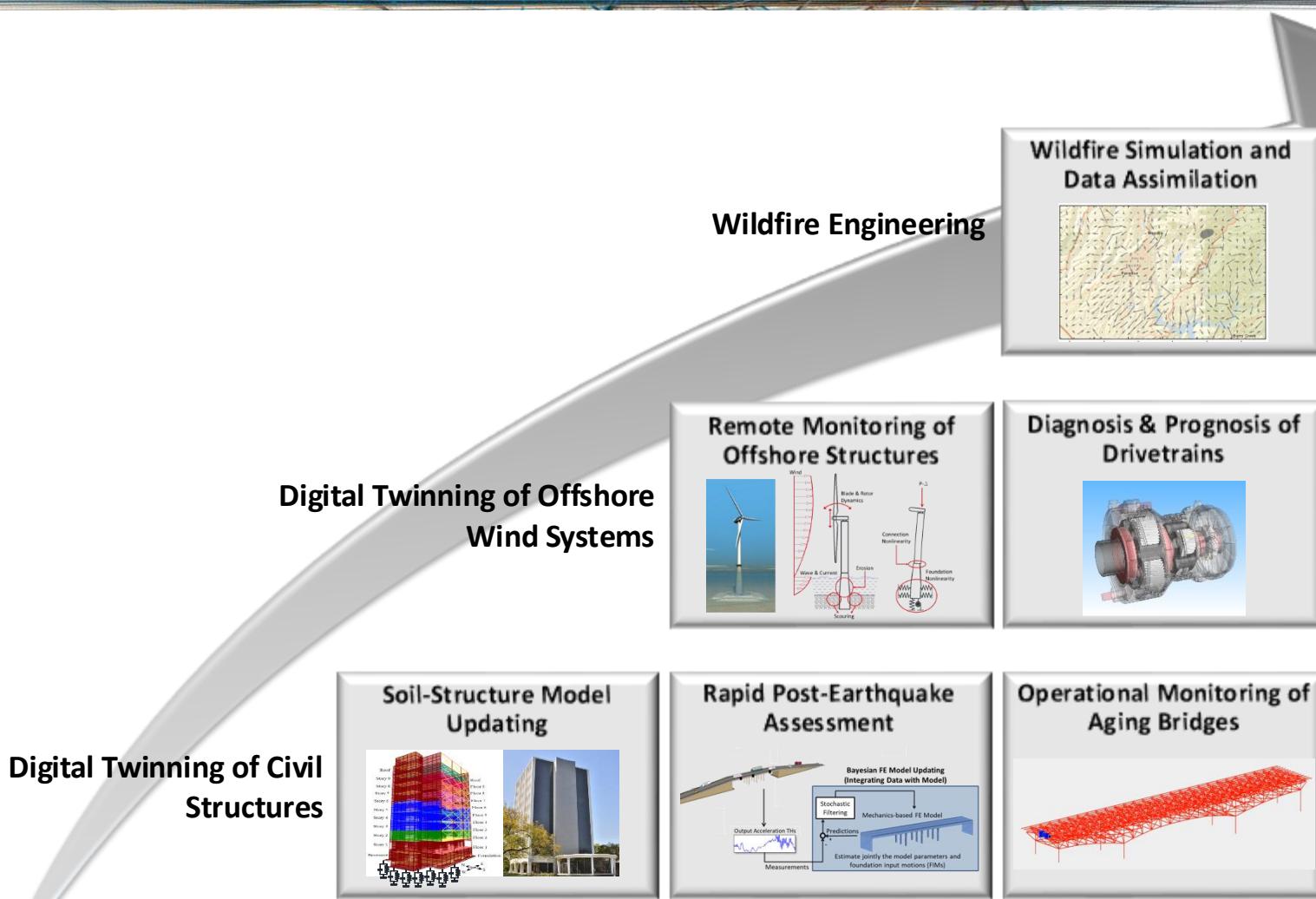


Problem Statement:

$$\mathbf{M}(\boldsymbol{\theta})\ddot{\mathbf{u}}_k(\boldsymbol{\theta}) + \mathbf{C}(\boldsymbol{\theta})\dot{\mathbf{u}}_k(\boldsymbol{\theta}) + \mathbf{r}_k(\mathbf{u}_{1:k}(\boldsymbol{\theta}), \boldsymbol{\theta}) = \mathbf{L}\mathbf{f}_{1:k}^{unknown}$$

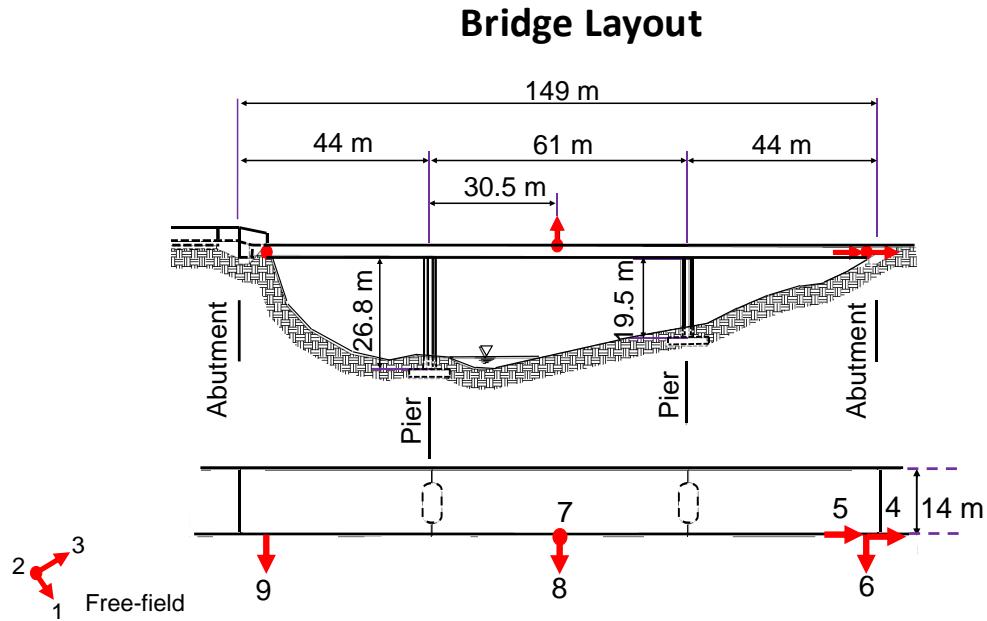
→ Find $\hat{\boldsymbol{\theta}}, \hat{\mathbf{f}}_{1:k}^{unknown} \mid \left[\hat{\boldsymbol{\theta}}, \hat{\mathbf{f}}_{1:k}^{unknown} \right] = \arg \max_{\boldsymbol{\theta} \in \Theta, \mathbf{f} \in \mathcal{F}} p(\boldsymbol{\theta}, \mathbf{f}_{1:k}^{unknown} \mid \mathbf{y}_{1:k})$

Bayesian Model Updating Applications



Output-Only Model Updating Using Seismic Records

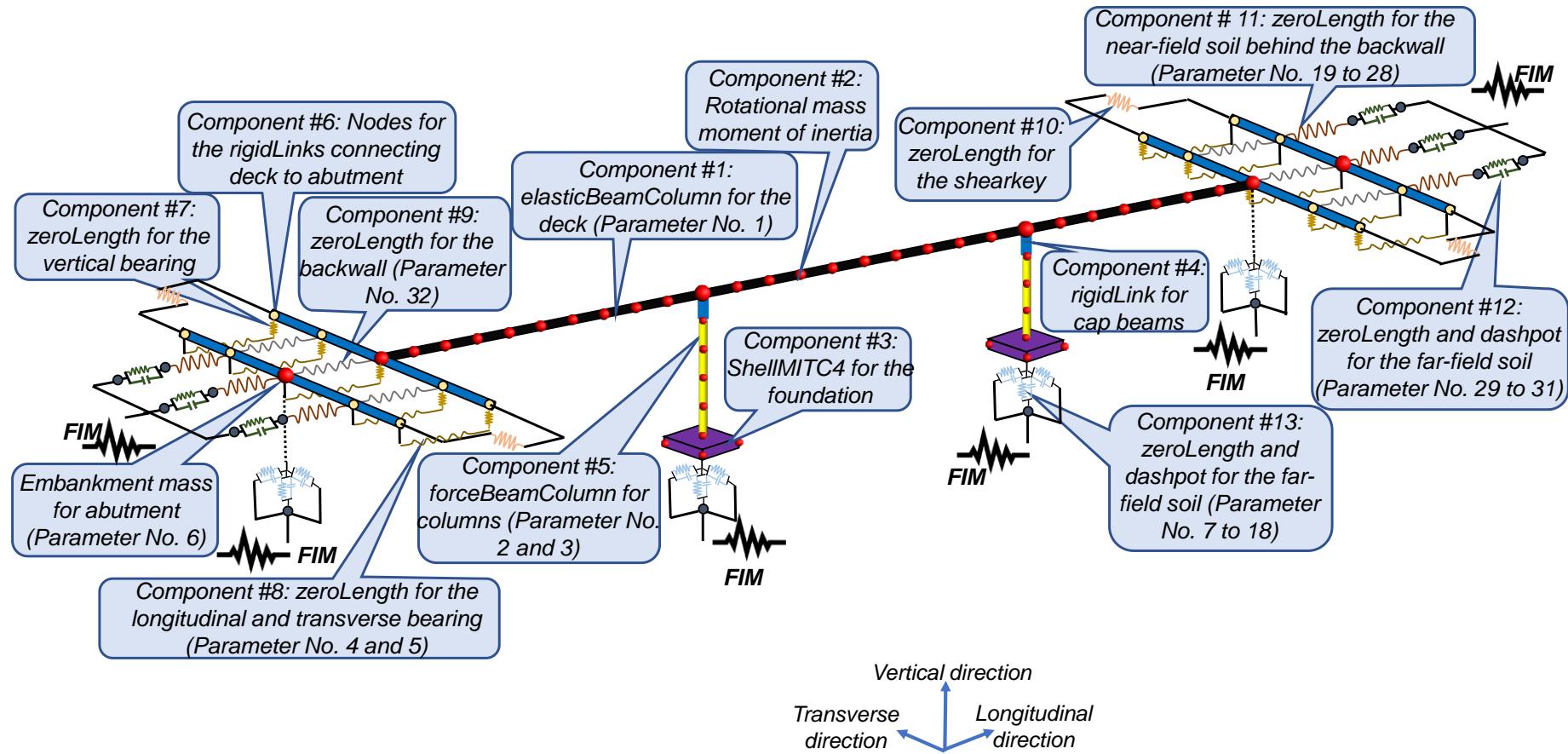
San Roque Canyon (SRC) Bridge
(Santa Barbara, CA)



Recorded Earthquakes at Bridge Station

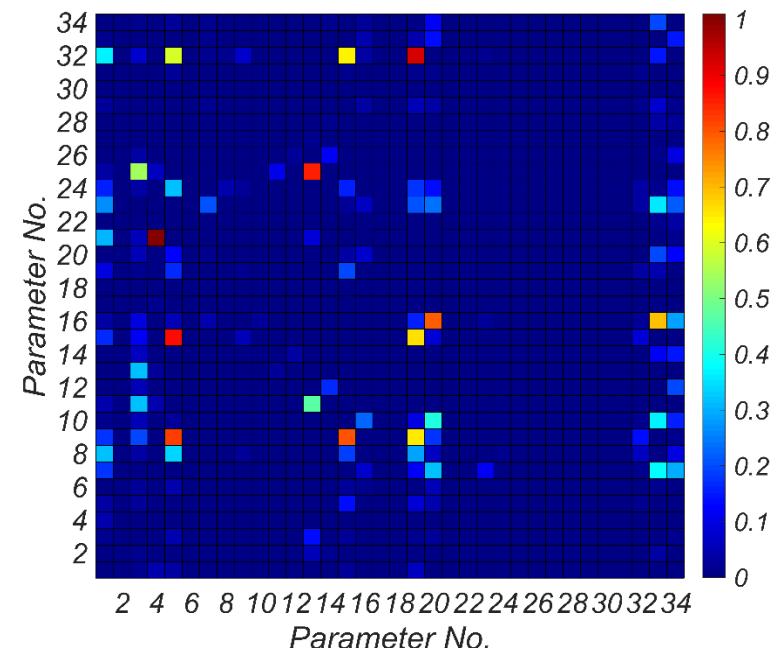
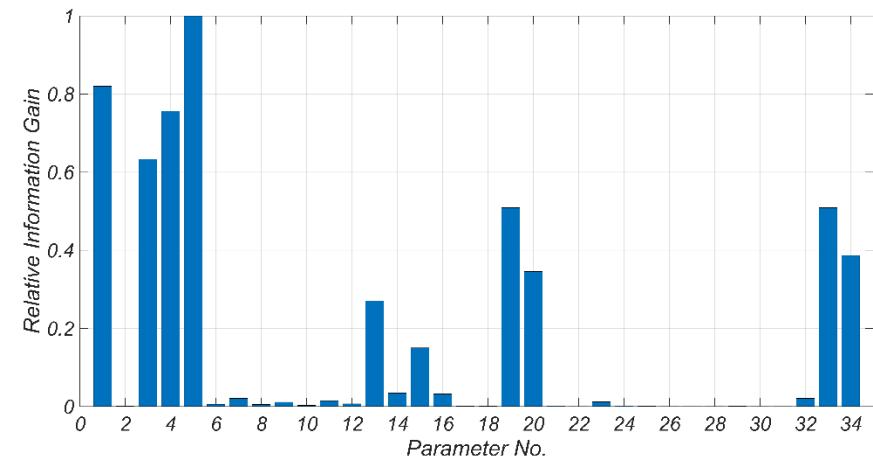
No.	Earthquake	Date	Distance (km)	PGA (g)	PSA in transverse direction (g)	PSA in vertical direction (g)	PSA in longitudinal direction (g)
1	San Simeon	12/22/2003	187.0	0.015	0.045	0.042	0.022
2	Isla Vista	05/09/2004	27.2	0.016	0.026	0.047	0.013
3	Isla Vista	05/29/2013	18.0	0.041	0.060	0.150	0.040
4	Montecito	04/23/2017	9.5	0.022	0.024	0.045	0.014
5	Santa Cruz	04/05/2018	67.9	0.016	0.021	0.058	0.019

Finite Element Model

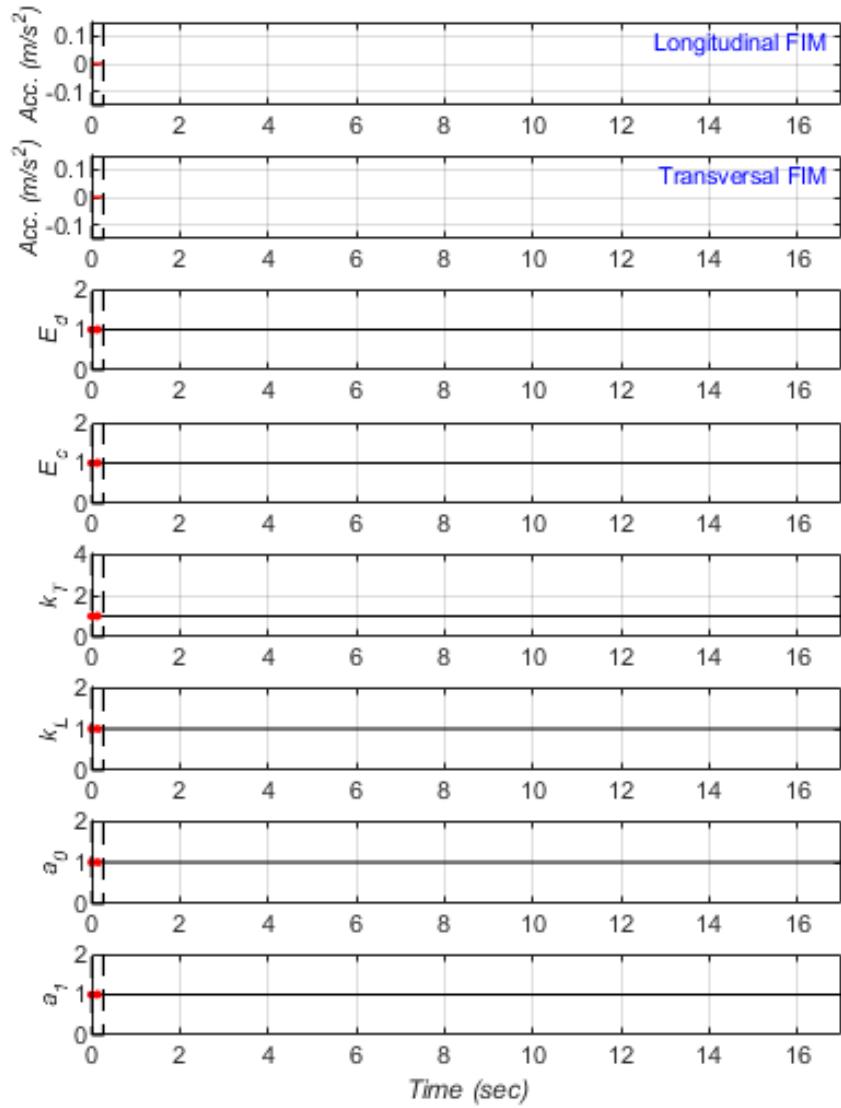
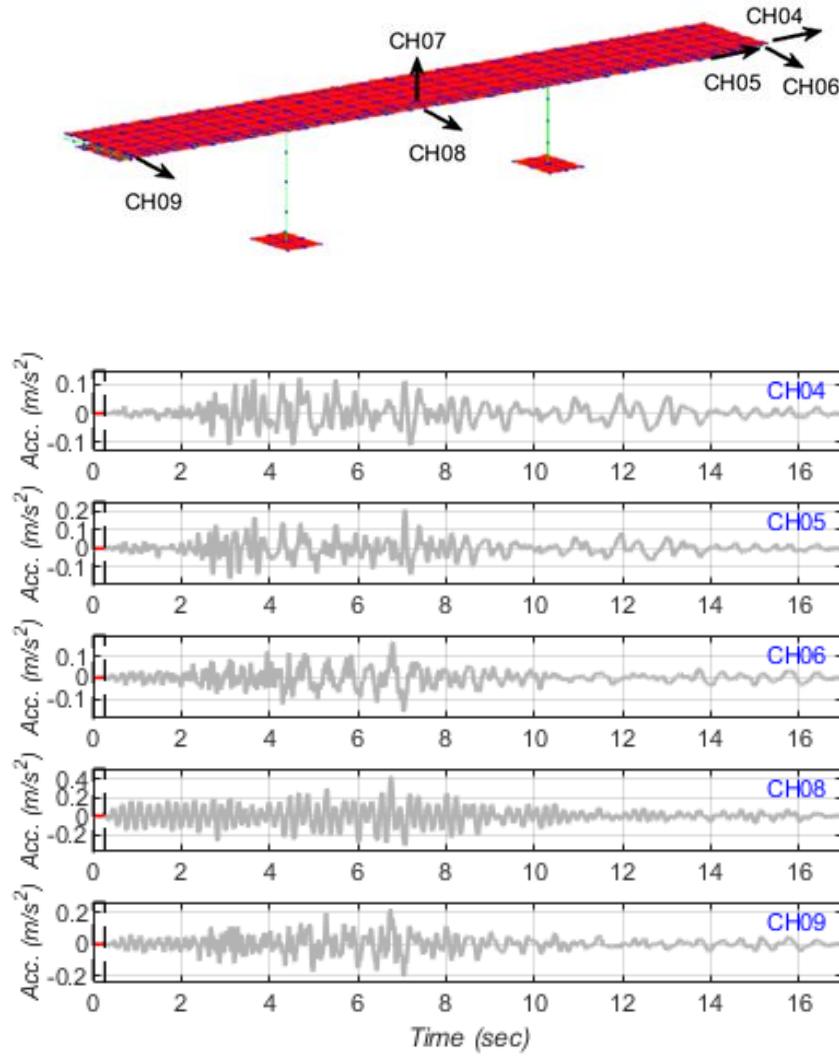


Uniqueness of Solution: Identifiability Analysis

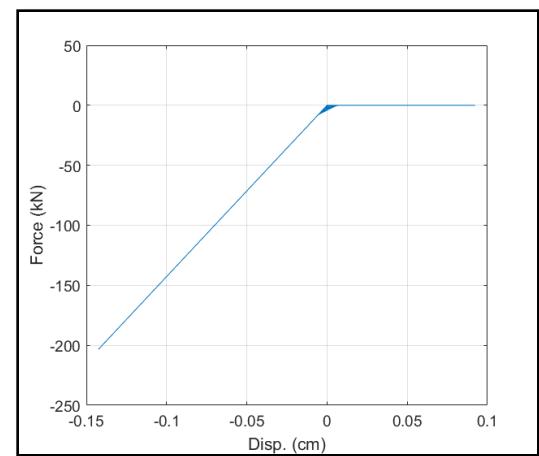
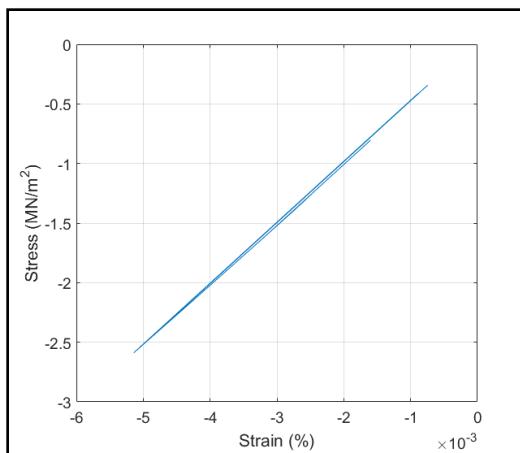
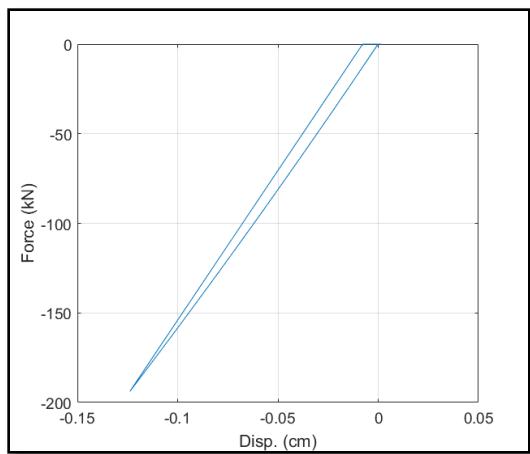
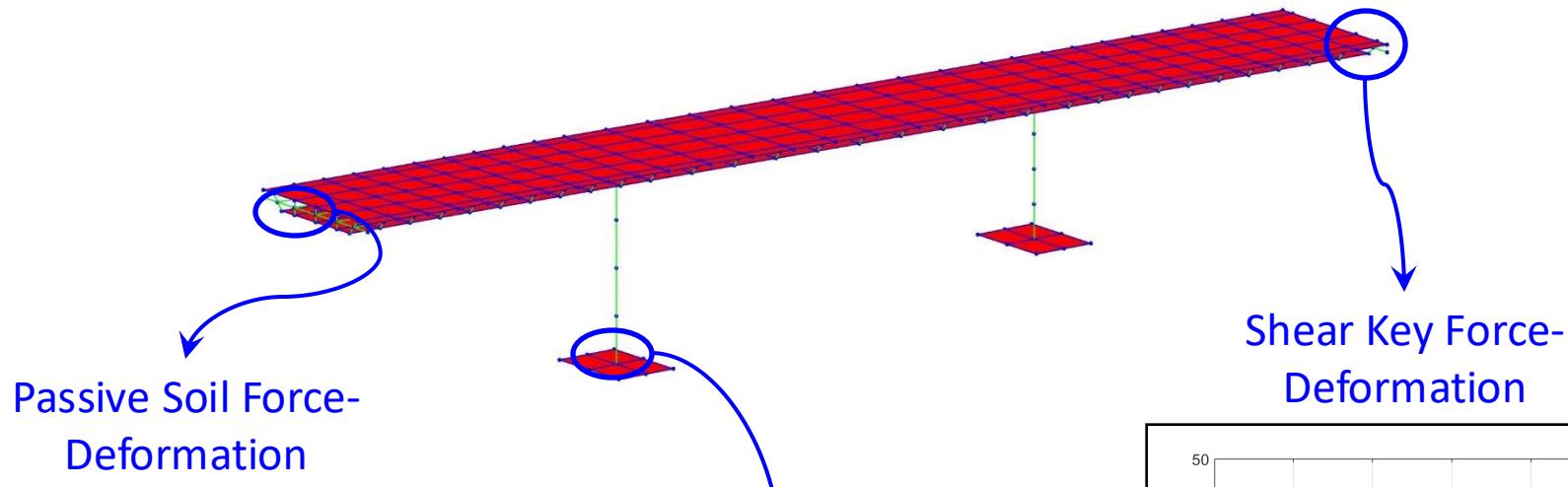
No.	Description	No.	Description
1	Elastic modulus of deck	18	Rotational soil-foundation damping coefficient under pier about the vertical axis
2	Compressive strength of column	19	Longitudinal soil-foundation stiffness under abutment
3	Initial elastic modulus of column	20	Longitudinal soil-foundation damping coefficient under abutment
4	Transverse elastomeric shear stiffness of bearing pad	21	Transverse soil-foundation stiffness under abutment
5	Longitudinal elastomeric shear stiffness of bearing pad	22	Transverse soil-foundation damping coefficient under abutment
6	Embankment mass for abutment	23	Vertical soil-foundation stiffness under abutment
7	Vertical soil-foundation stiffness under pier	24	Vertical soil-foundation damping coefficient under abutment
8	Vertical soil-foundation damping coefficient under pier	25	Rotational soil-foundation stiffness under abutment about its longitudinal axis
9	Longitudinal soil-foundation stiffness under pier	26	Rotational soil-foundation damping coefficient under abutment about the longitudinal axis
10	Longitudinal soil-foundation damping coefficient under pier	27	Rotational soil-foundation stiffness under abutment about the vertical axis
11	Transverse soil-foundation stiffness under pier	28	Rotational soil-foundation damping coefficient under abutment about the vertical axis
12	Transverse soil-foundation damping coefficient under pier	29	Far-field soil-embankment stiffness in longitudinal direction
13	Rotational soil-foundation stiffness under pier about the longitudinal axis	30	Far-field soil-embankment radiation damping coefficient in the longitudinal direction
14	Rotational soil-foundation damping coefficient under pier about the longitudinal axis	31	Far-field soil-embankment material damping coefficient in the longitudinal direction
15	Rotational soil-foundation stiffness under pier about the transverse axis	32	Soil-backwall initial stiffness in the longitudinal direction
16	Rotational soil-foundation damping coefficient under pier about the transverse axis	33	Mass proportional Rayleigh damping coefficient
17	Rotational soil-foundation stiffness under pier about the vertical axis	34	Stiffness proportional Rayleigh damping coefficient



San Simeon Earthquake Record

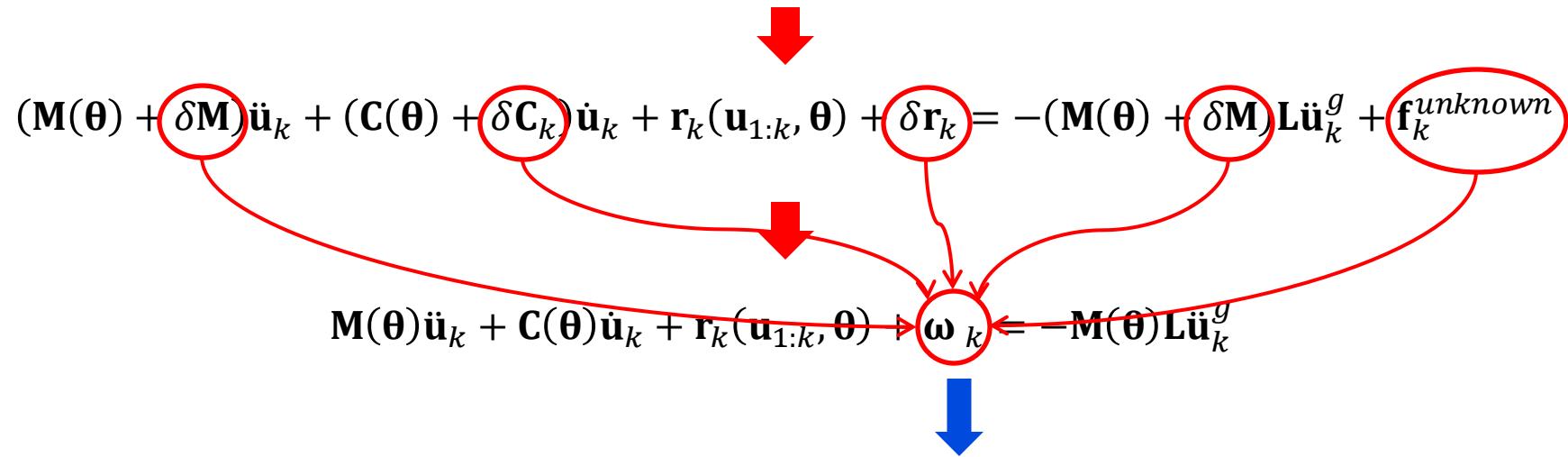


Virtual Sensing



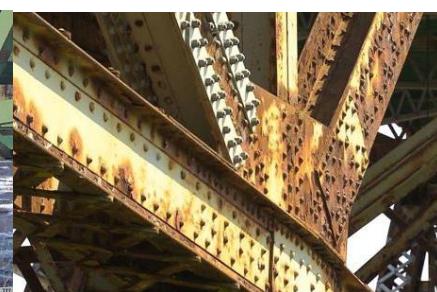
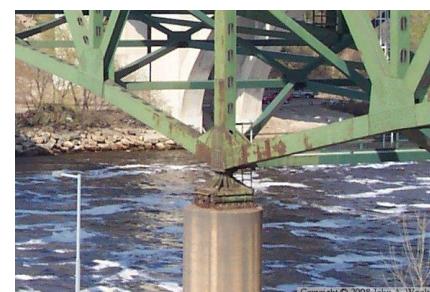
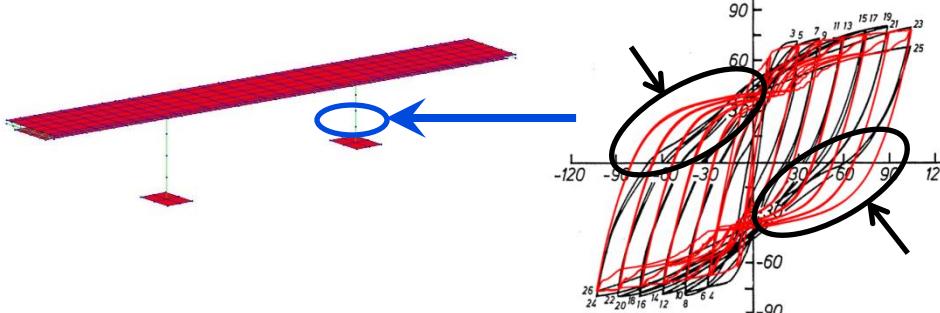
Limitation: Modeling Error or Model-Form Uncertainty

$$\mathbf{M}(\theta)\ddot{\mathbf{u}}_k + \mathbf{C}(\theta)\dot{\mathbf{u}}_k + \mathbf{r}_k(\mathbf{u}_{1:k}, \theta) = -\mathbf{M}(\theta)\mathbf{L}\ddot{\mathbf{u}}_k^g$$

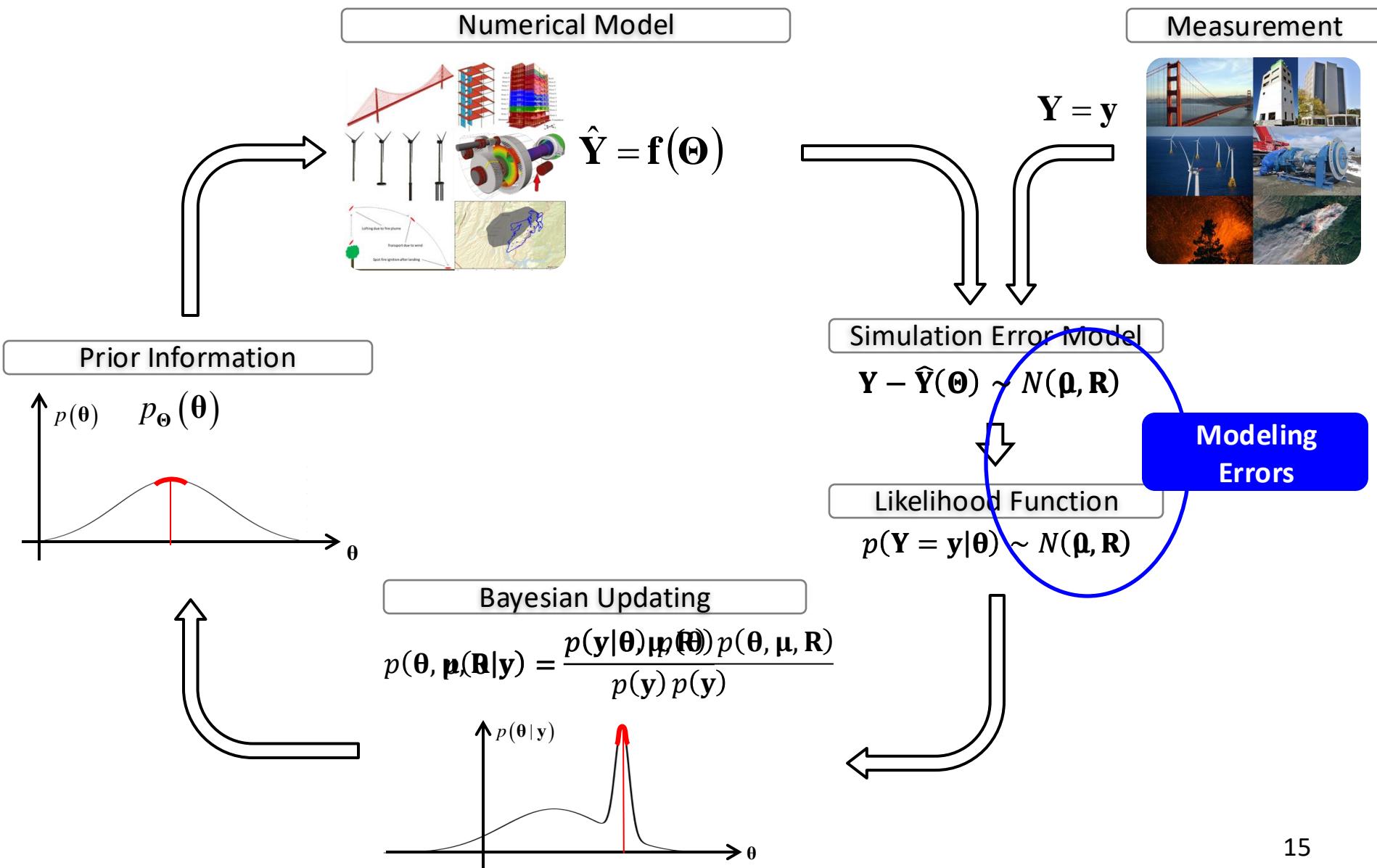


ω_k : Modeling errors lumped at the structural level

 Jointly estimate θ and higher statistics of ω_k
@ measurement locations

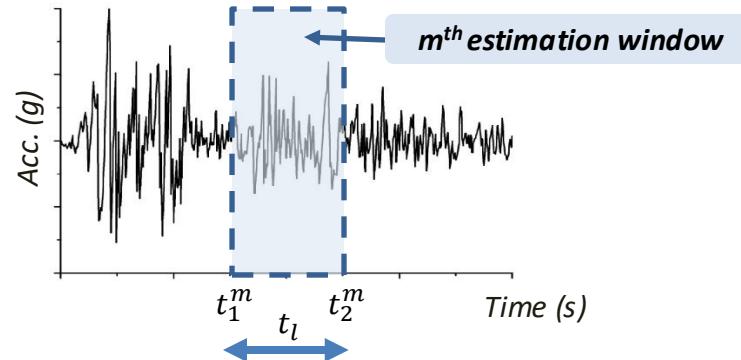


Adaptive Bayesian Inference for Model Updating



Joint Parameter, Input, and Noise Estimation

$$p(\Psi_m, \mu_m, R_m | y_{t_1:t_2}) = \frac{p(y_{t_1:t_2} | \Psi_m, \mu_m, R_m) p(\Psi_m, \mu_m, R_m)}{p(y_{t_1:t_2})}$$



$$\{\hat{\Psi}_m^+, \hat{\mu}_m^+, \hat{R}_m^+\} = \underset{\Psi_m, \mu_m, R_m}{\operatorname{argmax}} p(\Psi_m, \mu_m, R_m | y_{t_1^m:t_2^m})$$

$$\{\hat{\Psi}_m^+\} = \underset{\Psi_m}{\operatorname{argmax}} p(\Psi_m | \mu_m, R_m, y_{t_1^m:t_2^m})$$

$$\hat{\Psi}_m^+ = \hat{\Psi}_m^- + K_m (y_{t_1^m:t_2^m} - h_{t_1^m:t_2^m}(\hat{\Psi}_m^-) - \hat{\mu}_{t_1^m:t_2^m}^+)$$

$$P_{\Psi,m}^+ = P_{\Psi,m}^- - K_m P_{yy,m} K_m^T$$

$$\{\hat{\mu}_m^+, \hat{R}_m^+\} = \underset{\mu_m, R_m}{\operatorname{argmax}} p(\mu_m, R_m | y_{t_1^m:t_2^m})$$

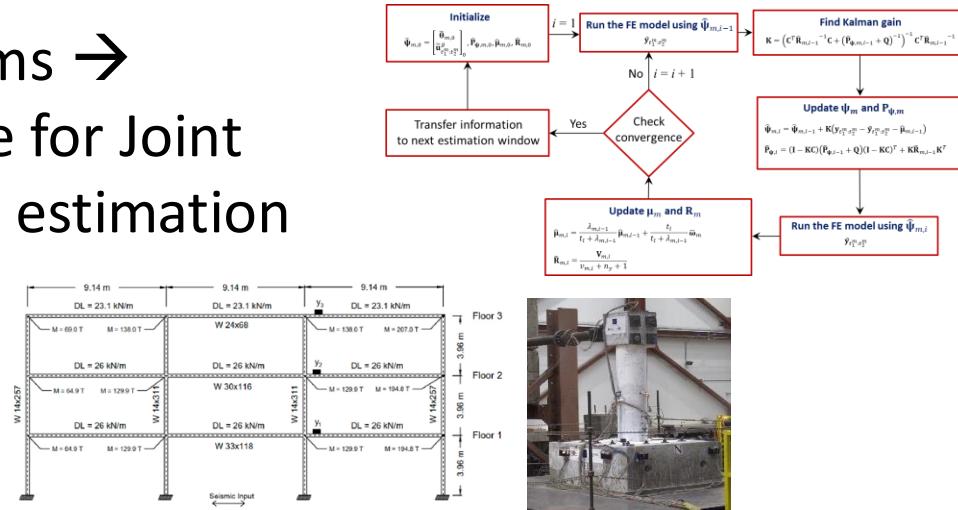
$$\hat{\mu}_m^+ = \frac{\lambda_m^-}{t_l + \lambda_m^-} \hat{\mu}_m^- + \frac{t_l}{t_l + \lambda_m^-} \bar{\omega}_m$$

$$\hat{R}_m^+ = \frac{V_m^+}{v_m^+ + n_y + 1}$$

Fixed-Point Iterations

PEER Project Summary

- Advancing existing algorithms → Adaptive Bayesian inference for Joint parameter, input, and noise estimation
- Verification & Validation



- Real-world application (BRACE² project)
- Open-source codes for HPC environment
 - OpenSees integration
 - Nested parallelization
- Educational & support materials

CGS CSMIP-89324
Rio Dell - Hwy 101/Painter St. Overpass





Thank you!

