

PACIFIC EARTHQUAKE ENGINEERING RESEARCH CENTER

Conditional Ground-Motion Model for Peak Ground Velocity for Active Crustal Regions

Norman A. Abrahamson

University of California, Berkeley

Sarabjot Bhasin

Duke University

PEER Report 2020/05

Pacific Earthquake Engineering Research Center
Headquarters, University of California at Berkeley

October 2020

Disclaimer

The opinions, findings, and conclusions or recommendations expressed in this publication are those of the author(s) and do not necessarily reflect the views of the study sponsor(s), the Pacific Earthquake Engineering Research Center, or the Regents of the University of California.

Conditional Ground-Motion Model for Peak Ground Velocity for Active Crustal Regions

Norman A. Abrahamson

University of California, Berkeley

Sarabjot Bhasin

Duke University

PEER Report No. 2020/05

Pacific Earthquake Engineering Research Center

Headquarters, University of California, Berkeley

October 2020

ABSTRACT

Conditional models for the horizontal and vertical peak ground velocity (PGV), given the pseudo-spectral acceleration [$PSA(T)$] values, are developed for active crustal regions. The period of the $PSA(T)$ used in the conditional model, T_{PGV} , is magnitude dependent, which captures the effect of the magnitude dependence of the earthquake source corner frequency on the PGV . Conditional models can be used to estimate the PGV given a design spectrum and are applicable for magnitudes between 3.0 and 8.5, and for distances up to 200 km. The conditional PGV models can also be combined with appropriate GMMs for $PSA(T)$ to develop traditional GMMs for PGV that are consistent with the more complex scaling included in the $PSA(T)$ model. Unlike previous conditional PGV models, the slope on the $\ln[PSA(T)]$ term is allowed to be different from unity. With this feature, an appropriate aleatory standard deviation of the resulting $\ln(PGV)$ can be computed, avoiding the over-prediction of the aleatory standard deviation of the PGV seen in previous conditional PGV models.

ACKNOWLEDGMENTS

We thank Jeff Bayless for providing early access to his empirical FAS model for California. This work was conducted as part of the 2018 summer internship program of the College Preparatory School's STEM program. We thank Dr. Campodonico for her work organizing the STEM program and for arranging this internship. Finally, we thank Professors Pedro Arduino and Filip Filippou for providing the Latex templates for PEER reports

Any opinions, findings, and conclusions or recommendations expressed in this material are those of the authors and do not necessarily reflect those of the sponsoring agencies or the Pacific Earthquake Engineering Research Center and the Regents of the University of California.

CONTENTS

ABSTRACT	iii
ACKNOWLEDGMENTS	v
TABLE OF CONTENTS	vii
LIST OF TABLES	ix
LIST OF FIGURES	xi
1 INTRODUCTION	1
1.1 Previous Conditional Models for <i>PGV</i>	3
2 DATASETS	7
3 CONDITIONAL <i>PGV</i> MODELS	11
3.1 Physical Basis for the <i>PGV</i> Model	11
3.2 Development of the Conditional <i>PGV</i> Model	11
3.3 Evaluation of Residuals	14
3.4 Model Application	15
4 CONVERTING CONDITIONAL GMMS TO TRADITIONAL GMMS	29
4.1 Median Model	29
4.2 Aleatory Variability	30
5 CONCLUSIONS	37
REFERENCES	39

LIST OF TABLES

3.1	Response spectral period with highest correlation to PGV by magnitude bin. . . .	17
3.2	Conditional PGV model coefficients for crustal earthquakes.	17
3.3	Coefficients for PGA -based and $PSA(T = 1)$ -based models for PGV for crustal earthquakes	18
4.1	Standard deviation for unconditional $\ln(PGV)$ for crustal earthquakes, horizontal component.	31

LIST OF FIGURES

2.1	Magnitude-distance distribution of the selected dataset for crustal earthquakes. . . .	8
2.2	Distribution of V_{S30} for small and large magnitudes.	9
3.1	Horizontal velocity FAS for different magnitudes for crustal earthquakes at a distance of 30 km and for a site with $V_{S30} = 400$ m/sec from the Bayless and Abrahamson (2019) model. The circles show the period with the highest correlation between $\ln(PGV)$ and $\ln[PSA(T)]$	19
3.2	Horizontal velocity FAS for M6 at different rupture distances for a site with $V_{S30} = 400$ m/sec from the Bayless and Abrahamson (2019) model.	19
3.3	Example of the relation between the $\ln(PGV)$ and $\ln[PSA(T = 1.5)]$ for crustal earthquakes with magnitudes between 6.5 and 7.5 at distances less than 50 km. The slope is less than unity.	20
3.4	Standard deviation of the linear fit of $\ln(PGV)$ for crustal earthquakes as a function of $\ln[PSA(T)]$ computed by magnitude bin.	20
3.5	Magnitude dependence of the period with highest correlation between PGV and $PSA(T)$	21
3.6	$PSA(T_{PGV})$ scaling of the conditional PGV model for $R_{RUP} = 10$ km and $V_{S30} = 425$ m/sec for magnitudes M4 to M8 for both the horizontal and vertical components.	22
3.7	$PSA(T_{PGV})$ scaling of the conditional PGV model for $M = 7$ and $V_{S30} = 425$ m/sec for R_{RUP} from 1 to 100 km for both the horizontal and vertical components.	23
3.8	$PSA(T_{PGV})$ dependence of the within-event residuals for the horizontal component.	24
3.9	Distance dependence of the within-event residuals for the horizontal component.	25
3.10	V_{S30} dependence of the within-event residuals for the horizontal component. The black symbols are the mean values by V_{S30} bin.	26
3.11	Between-event residuals for the horizontal component.	26
3.12	Within-event residuals of the conditional PGV model for near-fault ground motions with velocity pulses.	27
3.13	Within-event residuals of the conditional PGV model for near-fault ground motions for dipping faults. The sites with positive R_x are on the HW side and sites with negative R_x are on the footwall side.	27

4.1	Comparison of the magnitude scaling for the conditional PGV model for the horizontal component. The $PSA(T)$ is for the median spectrum from four NGA-West2 GMMs from a strike-slip earthquake at a rupture distance of 20 km at a stiff-soil site conditions ($V_{S30} = 400$ m/sec).	32
4.2	Comparison of the magnitude scaling for the horizontal component PGV using four different GMMs to compute the $PSA(T)$ values for the median spectrum from a strike-slip earthquake at a rupture distance of 20 km at a stiff-soil site conditions. The four GMMs used are: ASK14 = Abrahamson et al. (2014); BSSA14 = Boore et. al. (2014); CB14 = Campbell and Bozorgnia (2014); and CY14 = Chiou and Youngs (2014).	33
4.3	Magnitude dependence of the aleatory standard deviation for $\ln(PGV)$ for crustal earthquakes, horizontal component for a distance of 20 km.	34
4.4	Magnitude scaling at a rupture distance of 20 km for the PGA and $PSA(T = 1)$ models compared to the scaling for model based on $PSA(T_{PGV})$	35
4.5	Comparison of the aleatory standard deviation computed using the models conditioned on PGA and $PSA(T = 1)$ compared to the standard deviation for the conditional model based on $PSA(T_{PGV})$	36

1 Introduction

The most common ground-motion parameters used to develop design ground motions are horizontal-component elastic pseudo-spectral acceleration (PSA) values.

While the PSA values broadly represent the amplitude of the ground shaking important to the response of buildings, there are other ground-motion parameters that can significantly affect the response of different types of structures. Examples of secondary ground-motion parameters that are often considered when developing design ground motions are the duration, peak ground velocity (PGV), presence of a velocity pulse, Arias intensity (I_a), and cumulative absolute velocity (CAV).

There are two main approaches for estimating the secondary ground-motion parameters given a design earthquake scenario and a horizontal-component design spectrum. The first approach is to develop an empirical ground-motion model (GMM) for the secondary ground-motion parameters in a manner similar to the approach used to develop GMMs for the horizontal $PSA(T)$ values. The secondary parameter can be estimated using the design earthquake scenario (e.g., magnitude and distance) from the disaggregation of the hazard for the response spectral values at the periods important for the structure.

An alternative approach is to include the design $PSA(T)$ values as predictive parameters in the GMM for the secondary parameters in addition to the source, path, and site parameters used in traditional GMMs. For example, a GMM for secondary parameters may include the design $PSA(T = 1 \text{ sec})$ value as an input parameter. Abrahamson et al. (2016) used the term “conditional ground-motion model” for GMMs that include other ground-motion parameters as model input parameters. This is consistent with the term “conditional” used in the conditional mean spectrum (CMS) described by Baker and Cornell (2006). The CMS uses the design response spectral value at the conditioning period as input to compute the expected response spectral values at other spectral periods. The conditional GMM approach differs from the CMS approach in that the conditional GMM uses the design $PSA(T)$ value directly as an input parameter rather than using the normalized residual, ϵ , for the design $PSA(T)$ and the correlation coefficient between the ϵ values for the two spectral periods. Because the $PSA(T)$ value already includes magnitude, distance, and site scaling effects, conditional GMMs have weaker dependence on these parameters compared to traditional GMMs. In addition, they have much smaller aleatory variability, making the regression more robust.

An advantage of using the conditional GMM approach is that it leads to estimates of the secondary parameters that are compatible with the design response spectral values. In contrast,

using a traditional GMM approach can lead to estimates of the secondary parameters that are inconsistent with the design $PSA(T)$ values. For example, if the design $PSA(T)$ value from a probabilistic seismic hazard analysis corresponds to $\epsilon = 1.5$ (i.e., the 93th percentile spectral acceleration), then the common practice of computing the secondary parameter based on the 16th–84th percentile range for the controlling scenario from the disaggregation will lead to a target range of the values of the secondary parameter inconsistent with the design $PSA(T)$ values.

This inconsistency issue can be addressed using the correlation between the ϵ of the secondary parameter and the ϵ of spectral acceleration at the selected period, and computing the expected value of the secondary parameter given the ϵ of the design $PSA(T)$, similar to the approach for computing the CMS. It may seem easier to just follow this CMS-type approach; however, using the correlation approach implicitly assumes that the GMM for the secondary parameter has a consistent parameterization and consistent physical constraints on the extrapolation as the horizontal PSA GMM. This is the case for spectral accelerations at different periods from a single GMM, but it may not be the case for secondary parameters because the GMMs for the secondary parameters are often developed by different researchers, and there is less information available from analytical studies to provide physical constraints on the scaling for the secondary parameters.

A conditional GMM can be combined with a suite of GMMs for the median and standard deviation of the $PSA(T)$ values to develop a suite of GMMs for the secondary parameter that fully captures the aleatory variability as well as the magnitude, distance, and site scaling of the median of the secondary parameter. For example, the single conditional model for I_a , developed by Abrahamson et al. (2016), was combined with each of the five NGA-West2 GMMs per Gregor et al. (2014) for the PGA and $PSA(T = 1)$ values to produce five alternative GMMs for I_a . In this approach, the magnitude, distance, and site scaling for each $PSA(T)$ model is incorporated into a new I_a model. Because of the smaller aleatory variability and the simpler functional forms required, the coefficients of conditional models are stable and well constrained by the available empirical data.

Conditional GMMs have been considered as overly simplified models that should only be used if a traditional GMM is not available for the secondary parameter of interest. For example, Bommer and Alarcon (2006) have claimed that estimating PGV using traditional GMMs for PGV is preferable to estimating the PGV using conditional models based on the response spectral values. Furthermore, they recommended that conditional models should only be used for estimating a secondary parameter if there are no appropriate traditional GMMs available for the secondary parameter. We do not agree with this recommendation. More than just being a simplified model used as a last resort, there are several key advantages to using the conditional GMM approach.

1. Conditional GMMs may take advantage of the significant effort that has been put into developing constraints on the extrapolation in the PSA –GMM scaling using analytical modeling for effects not well constrained by the empirical data, such as short-distance saturation, hanging-wall (HW) effects, soil-depth effects, and nonlinear soil effects. For example, Abrahamson et al. (2016) showed that by combining a conditional GMM for I_a without HW effects with an NGA-West2 GMM that used seismological finite-fault simulations to constrain the HW effects, the resulting I_a model captured almost all of the HW effect on the I_a by using the PGA as an input parameter.

2. Regional differences in the scaling for the secondary parameters can be easily estimated by combining a global conditional model with region-specific GMMs for the $PSA(T)$ values. This leads to a region-specific model for the secondary parameters for the new region.
3. Using conditional GMMs leads to secondary parameters that are consistent with PSA GMM. Traditional GMMs for the secondary parameters are often developed by different researchers than those that developed the $PSA(T)$ GMM. As a result, they can have inconsistent scaling from the PSA GMM in terms of how the model extrapolates outside the empirical data range. So while the GMM for the secondary parameter fits the available data, it may give estimates that are inconsistent with the design $PSA(T)$ values if the models use different analytical and seismological constraints outside the range well constrained by the data.
4. The conditional GMMs have simpler functional forms and much smaller aleatory variability than traditional GMMs, so the coefficients of the conditional GMMs are better constrained than the coefficients for traditional GMMs.

1.1 PREVIOUS CONDITIONAL MODELS FOR PGV

Newmark and Hall (1982) developed a model for the ratio of the pseudo-spectral velocity (PSV) to the PGV for spectral periods in the velocity-controlled period range of the response spectrum. For 5% damping, the median $PSV(T)/PGV$ ratio in the velocity-controlled region given by Newmark and Hall (1982) is 1.65. While Newmark and Hall (1982) used this $PSV(T)/PGV$ ratio to estimate the $PSV(T)$ in velocity-controlled region given an estimate of the PGV , this ratio can be also used to develop a conditional ground-motion model for PGV given the $PSA(T)$. Converting the $PSV(T)$ in cm/sec to $PSA(T)$ in g and taking the natural logarithms, the Newmark and Hall (1982) scale factor for $PSV(T)/PGV$ can be rewritten as:

$$\ln(PGV) = 4.55 - \ln(T) + 1.0\ln[PSA(T)] \quad (1.1)$$

where the PGV is in cm/sec, the $PSA(T)$ is in g , and the period, T , is the period representing the constant-velocity region.

Bommer and Alarcon (2006) evaluated the relationship between PGV and $PSA(T)$ at a range of spectral periods. They found that the $\ln[PSA(T)]$ at a period of 0.5 sec had similar magnitude scaling as the $\ln(PGV)$. Therefore, they developed a simple conditional model for PGV for crustal earthquakes in active regions based on the 5% damped PSA at $T = 0.5$ sec.

$$PGV = \frac{980PSA(T = 0.5)}{20} \quad (1.2)$$

where the PGV is in cm/sec, and the $PSA(T)$ is in g . A magnitude term was not included in this model because the magnitude scaling of the PGV and the $PSA(T = 0.5)$ were found to be similar. This $PGV - PSA$ relation can be written as:

$$\ln(PGV) = 3.89 + 1.0\ln[PSA(T = 0.5)] \quad (1.3)$$

An issue with these models is the estimation of the standard deviation of the PGV . Bommer and Alarcon (2006) noted that GMMs developed for both PSA and PGV show that the standard deviation of $\ln(PGV)$ is smaller than the standard deviation of $\ln[PSA(T = 0.5)]$. In this case, adding the variance from the residuals of the conditional $\ln(PGV)$ model to the variance of the $\ln(PSA)$ model would add to the overestimation of the total standard deviation of $\ln(PGV)$ already present due to the use of the standard deviation of $\ln[PSA(T = 0.5)]$. Therefore, they recommended not including the standard deviation of the conditional model in estimating the aleatory variability of the resulting $\ln(PGV)$.

Huang and Whittaker (2015) developed an updated conditional PGV model for use in seismic performance evaluations described in FEMA-58-1 (2018). Using ground-motion data from the NGA-West2 dataset for active crustal regions, they developed two alternative empirical models for the PSV/PGV ratio: one based on the PSV/PGV ratio averaged over the period range of 0.5 to 2 sec, and one based on the PSV/PGV ratio at a period of 1.0 sec. Their PSV/PGV model using the $T=1$ sec PSV is given by:

$$\ln \left[\frac{PSV(T = 1)}{PGV} \right] = 1.3 - 0.13M \quad (1.4)$$

with a standard deviation of 0.43 natural log units. Converting the PSV in cm/sec to the PSA in g , their model can be written as:

$$\ln(PGV) = 3.75 + 1.0\ln[PSA(T = 1)] + 0.13M \quad (1.5)$$

For the model based on the $PSV(T)/PGV$ ratio averaged over the 0.5 to 2.0 sec period range, the standard deviation of $\ln[PSV(T)/PGV]$ is reduced to 0.33 natural log units. This reduction in the standard deviation reflects that there is not a single predominant period for the PGV for all earthquakes; therefore, using the PSV averaged over a period range is a better parameter for predicting the PGV for a range of magnitudes. For computing the standard deviation of $\ln(PGV)$, Huang and Whittaker (2015) add the variance of the conditional PGV model to the variance of the $\ln[PSA(T)]$ model.

All three of the previous models for estimating PGV given the response spectral values are based on statistical modeling of the $PSV(T)/PGV$ or $PSA(T)/PGV$ ratios, which is equivalent to constraining the slope on the $\ln[PSA(T)]$ term to be unity; see Equations (1.1), (1.3), and (1.5). As discussed later in the model development section, constraining the slope to unity limits the ability to accurately compute the standard deviation of PGV .

In this study, we have developed conditional ground-motion models for the horizontal and vertical components of $\ln(PGV)$ for active crustal regions. Our approach differs from the previous models in that the conditional PGV models are developed directly for the $\ln(PGV)$ rather than developing the model for the $PSV(T)/PGV$ or $PSA(T)/PGV$ ratio, which allows the slope on the $\ln[PSA(T)]$ term to be different from unity. This approach allows for the aleatory variability

of $\ln(PGV)$ for an earthquake scenario [i.e., without considering a given $PSA(T)$ value] to be accurately estimated by combining the conditional PGV model with the standard deviation of an appropriate GMM for the $PSA(T)$.

2 Datasets

For active crustal earthquakes, we used the NGA-west2 database (Ancheta et al., 2014) developed by the Pacific Earthquake Engineering Research Center (PEER). This database includes ground motions from earthquakes in active crustal regions around the world that have occurred between 1940 and 2011. The full database contains over 21,000 three-component recordings from 713 earthquakes. We used the same subset of this dataset as selected by Abrahamson et al. (2016) for their conditional ground-motion model for Arias intensity (AI). This subset consists of 11,353 recordings with distances between 0 and 340 km from 431 earthquakes, with magnitudes between 3.0 and 7.9.

Recordings with a usable long-period range that does not cover the spectral periods relevant to the PGV were removed. For the horizontal component, 47 recordings were removed due to the usable period-range constraint. For the vertical component, 427 recordings were removed. The magnitude and distance distribution of the 11,306 recordings from 427 earthquakes in the selected horizontal dataset is shown in Figure 2.1.

The distribution of the V_{S30} is shown in Figure 2.2. Most of the data are for V_{S30} between 200 and 800 m/sec. There are only a few recordings on hard-rock conditions. The sample from small and large magnitude is similar.

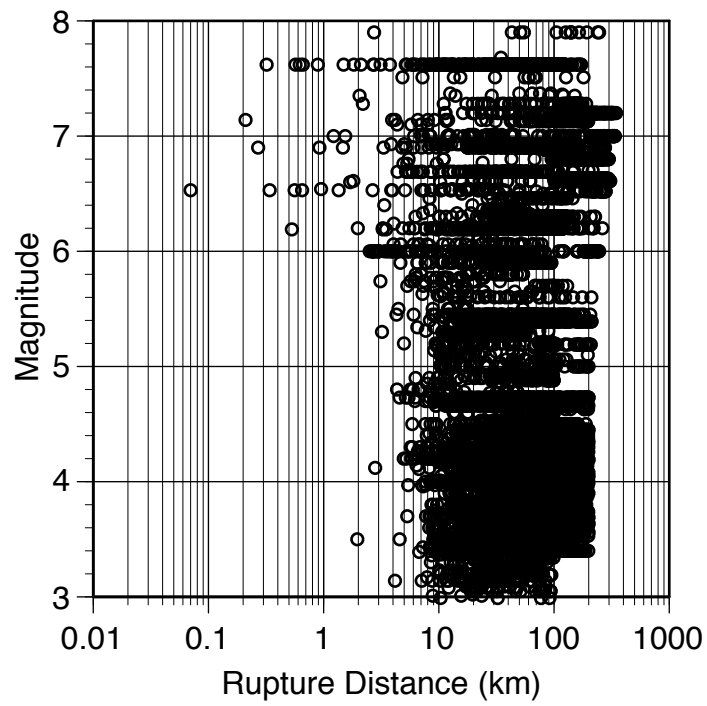


Figure 2.1: Magnitude-distance distribution of the selected dataset for crustal earthquakes.

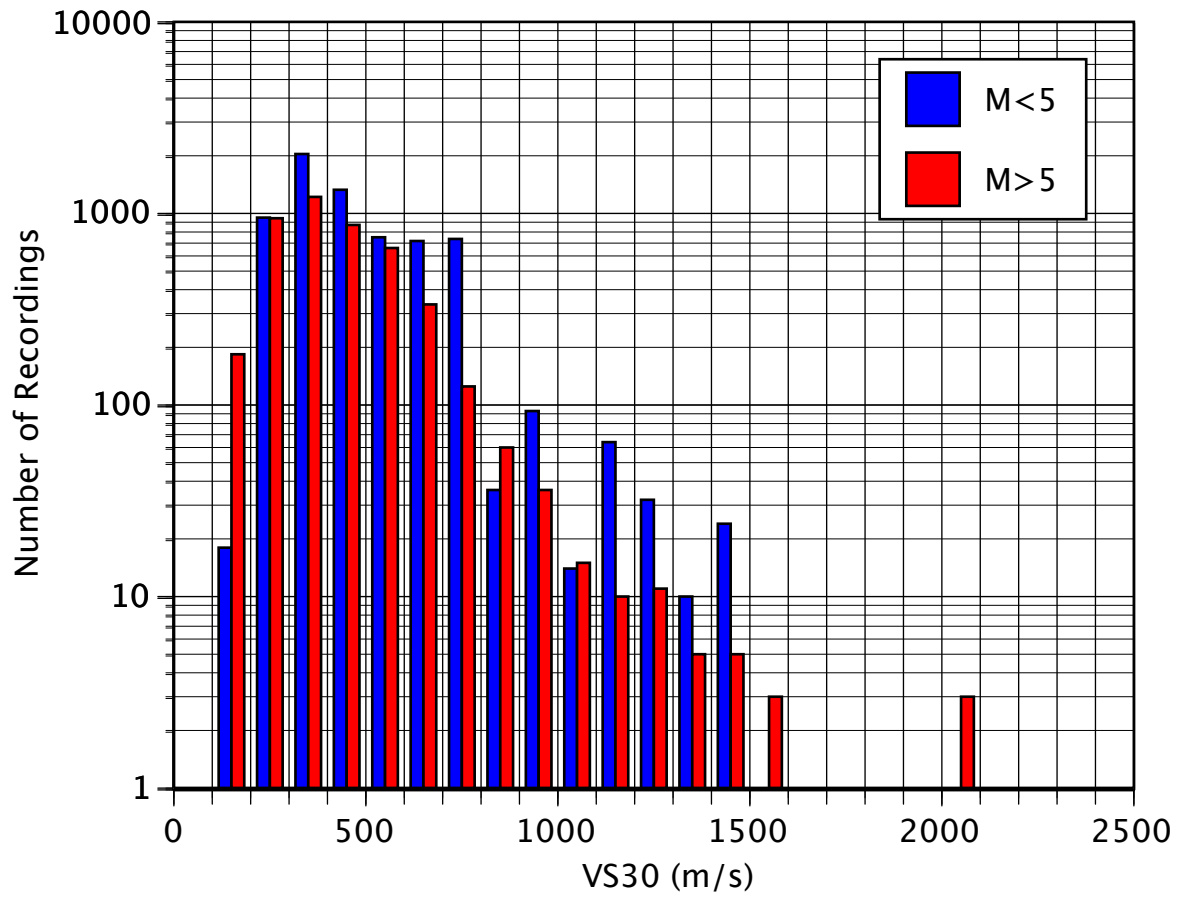


Figure 2.2: Distribution of V_{S30} for small and large magnitudes.

3 Conditional *PGV* Models

The development of good empirical GMMs for earthquake engineering applications is more than just a curve-fitting exercise. First, there should be a physical basis for the form of the model. Second, there should be appropriate constraints on the extrapolation of the model outside of the range constrained by the empirical data but that are important contributors to the seismic hazard. Given an appropriate functional form and appropriate constraints, the regression analysis is used to fit the model in the range covered by the empirical data.

3.1 PHYSICAL BASIS FOR THE *PGV* MODEL

For the relationship between $PSA(T)$ and PGV , the key physical constraint comes from the magnitude dependence of the source corner frequency in the Fourier amplitude spectrum (FAS) of ground motions. This change in frequency content can be seen in the magnitude scaling of the velocity FAS. Figure 3.1 shows the velocity FAS for **M3** to **M8** earthquakes in California based on the Bayless and Abrahamson (2019) FAS GMM. Due to the magnitude dependence of the corner frequency, there is an increase in the long-period content with increasing magnitude, and the predominant period of the peak velocity will increase as the earthquake magnitude increases. As a result, the period of the $PSA(T)$ that has the highest correlation between PGV and $PSA(T)$, denoted T_{PGV} , will also be magnitude dependent. The velocity time series for smaller magnitude earthquakes will have a smaller T_{PGV} values than for larger earthquakes.

The distance dependence on the frequency content of the velocity FAS is much weaker than the magnitude dependence. Figure 3.2 shows that velocity FAS for **M6** at distances of 5, 20, 50, 100, and 200 km using the Bayless and Abrahamson (2019) FAS GMM. Compared to the large changes in spectral shapes for different magnitudes, the spectral shapes for the different distances are very similar. Therefore, we do not consider the distance dependence in the model for T_{PGV} for the distance range of up to 200 km considered in this study.

3.2 DEVELOPMENT OF THE CONDITIONAL *PGV* MODEL

The development of the conditional PGV model starts with the evaluation of the magnitude dependence of the correlation of the PGV and $PSA(T)$. The data are first divided into magnitude bins with a width of 1 magnitude unit. For each magnitude bin, the correlation between the $\ln(PGV)$

and the $\ln[PSA(T)]$ is computed for 104 spectral periods between 0.01 and 10 sec, as given in the PEER NGA-West2 dataset. Unlike the previous studies discussed above, the slope of the $\ln(PSA)$ term is a free parameter rather than being fixed at unity:

$$\ln(PGV) = c_1 + c_2 \ln[PSA(T_{PGV})] \quad (3.1)$$

The inclusion of the slope, c_2 , as a free parameter is important because it captures the difference in the standard deviation of the $\ln(PGV)$ relative to the standard deviation of the $\ln[PSA(T)]$ as shown below.

Using simple propagation of errors, the variance of the $\ln(PGV)$ is given by

$$\sigma_{\ln PGV}^2 = \left(\frac{\partial \ln PGV}{\partial \ln PSA(T_{PGV})} \right)^2 \sigma_{\ln PSA(T_{PGV})}^2 + \sigma_{\ln PGV | PSA(T_{PGV})}^2 \quad (3.2)$$

in which $\sigma_{\ln PGV}$ and $\sigma_{\ln PSA(T)}$ are the standard deviations of the residuals from traditional GMMs for $\ln(PGV)$ and $\ln[PSA(T)]$, respectively. For the simple model given in Equation (3.1), the partial derivative is just a constant:

$$\frac{\partial \ln PGV}{\partial \ln PSA(T_{PGV})} = c_2 \quad (3.3)$$

The standard deviation of the conditional PGV GMM is related to the standard deviation of the traditional PGV GMM through the correlation coefficient:

$$\sigma_{\ln PGV | PSA(T_{PGV})}^2 = (1 - \rho^2) \sigma_{\ln PGV}^2 \quad (3.4)$$

where ρ is the correlation coefficient between the normalized residuals from a traditional GMMs for the $\ln(PGV)$ and $\ln[PSA(T)]$. Substituting Equation (3.3) and Equation (3.4) into Equation (3.2), the slope, c_2 , is given by

$$c_2 = \rho \frac{\sigma_{\ln PGV}}{\sigma_{\ln PSA(T_{PGV})}} \quad (3.5)$$

The correlation coefficient must be less than or equal to 1.0, and from the Abrahamson et al. (2014) NGA-West2 GMM, $\sigma_{\ln PGV} < \sigma_{\ln PSA(T)}$ for all periods. Therefore, using Equation (3.5), c_2 will be less than 1.0. Figure 3.3 shows the relation between the $\log(PGV)$ and the $\log[PSA(T = 1.5)]$ for a subset of crustal data with magnitudes between 6.5 and 7.5 and rupture distances less than 50 km. As expected, the slope of 0.829 is less than unity.

The magnitude dependence of the T_{PGV} is evaluated using a subset of the dataset, with rupture distances less than 50 km to focus on the source-scaling effects. The distance and site dependence of the conditional PGV model is modeled in a later step using the full dataset. Using this subset, a contour plot of the standard deviation of the fit to Equation (3.1) is shown as a function of magnitude and spectral period in Figure 3.4 for the horizontal component.

The T_{PGV} value found for each magnitude bin is listed in Table 3.1. The magnitude dependence of the T_{PGV} is shown in Figure 3.5, which is similar for both the horizontal and vertical components. Also, the contours of the correlations shown in Figure 3.4 are broad. Therefore, the T_{PGV} values for the horizontal and vertical components are combined, and a single relation is developed for both horizontal and vertical components. Based on the binned values shown in Figure 3.5, a simple linear relation is used to model the magnitude dependence of the T_{PGV} for rupture distances less than 50 km:

$$\ln(T_{PGV}) = b_1 + b_2 M \quad (3.6)$$

An ordinary least-squares fit to the combined horizontal and vertical data results in $b_1 = -4.09$ and $b_2 = 0.66$, with a standard deviation of 0.2 natural log units.

We can compare the magnitude dependence of T_{PGV} with the result of Bommer and Alarcon (2006), where $T = 0.5$ sec was the best single period to use for estimating the PGV from the $PSA(T)$. In the Abrahamson and Silva (1997) dataset used by Bommer and Alarcon (2006), the magnitudes range from **M**4.4 to **M**7.4. Using Equation (3.6), the spectral periods with the highest correlation for **M**4.4 to 7.4 range from 0.3 sec to 2.2 sec. The magnitude-independent value of $T_{PGV} = 0.5$ sec used by Bommer and Alarcon (2006) falls within this range.

Given the model for the magnitude dependence of T_{PGV} , a new ground-motion parameter, $PSA[T_{PGV}(M)]$, is computed from the NGA-West2 dataset. For T_{PGV} values that fall between the spectral periods in this dataset, the $PSA(T)$ value is computed using linear interpolation on the log-period and log- PSA values.

To fully take advantage of the conditional GMM approach, simple magnitude, distance, and site terms need to be included so that the slope of the $\ln(PSA)$ term represents the product of the correlation and the ratio of the standard deviations, as shown in Equation (3.5). For slopes less than unity, the full magnitude, distance, and site scaling is not included in the $c_2 \ln(PSA)$ term. The difference in the magnitude, distance, and site dependence of the $\ln(PGV)$ and that of the scaled $\ln(PSA)$ is captured by the explicit magnitude, distance, and site terms.

The functional form used for the conditional PGV model is given by

$$\begin{aligned} \ln(PGV) = & a_1 + f_1(M) \ln[PSA(T_{PGV})] + a_4 (M - 6) + a_5 (8.5 - M)^2 \\ & + a_6 \ln[R_{RUP} + 5e^{0.4(M-6)}] + [a_7 + a_8(M - 5)] \ln\left(\frac{V_{S30}}{425}\right) + \delta B + \delta W \end{aligned} \quad (3.7)$$

in which M is the moment magnitude, R_{RUP} is the rupture distance in kilometers, the PSA is the 5% damped spectral acceleration in g , V_{S30} is the time-averaged shear-wave velocity over the top 30 m in m/sec, and δB and δW are the between-event and within-event residuals, respectively. An initial analysis demonstrated that setting the finite-rupture saturation term at $5e^{0.4(M-6)}$ removed any short-distance trend in the residuals at large magnitudes. Because the period of the PSA used in the regression, T_{PGV} , is magnitude dependent, the V_{S30} scaling is also magnitude dependent. To reduce the trade offs in the coefficients, the regression was implemented in two steps.

1. The V_{S30} scaling terms (a_7 and a_8) are set to zero.
2. The within-event residuals are fit with just the (a_7 and a_8) terms.

As discussed earlier, the slope of the $\ln[PSA(T_{PGV})]$ term, f_1 , is related to the differences in the aleatory standard deviations for $\ln(PGV)$ and $\ln[PSA(T_{PGV})]$. The differences in the standard deviation for $\ln[PSA(T_{PGV})]$ and $\ln(PGV)$ from the Abrahamson et al. (2014) GMM are magnitude dependent. Therefore, the f_1 term is modeled as magnitude dependent. A simple tri-linear form is used for $f_1(M)$:

$$f_1(M) = \begin{cases} a_2 & \text{for } M < 5 \\ a_2 + (a_3 - a_2)(M - 5.0)/2.5 & \text{for } 5 \leq M \leq 7.5 \\ a_3 & \text{for } M > 7.5 \end{cases} \quad (3.8)$$

The coefficients are estimated using a random-effects regression analysis with a random effect for the earthquake; see Abrahamson and Youngs (1992). The standard deviations of the between-event and within-event residuals are denoted τ and ϕ , respectively. The total standard deviation is given by $\sigma = \sqrt{\phi^2 + \tau^2}$. The resulting coefficients and standard deviation terms are listed in Table 3.2. The $f_1(M)$ term for the vertical component is smaller than for the horizontal component, indicating that the correlation between PSA and PGV is weaker for the vertical component.

The $PSA(T)$, magnitude, and distance scaling of the conditional PGV model are shown in Figures 3.6 and 3.7. Both figures show a strong dependence of the PGV on the $PSA(T_{PGV})$. Figure 3.6 shows that the horizontal and vertical models are similar for **M**4, but they separate at larger magnitudes because the horizontal PGV has a stronger magnitude scaling than the vertical PGV . Note: Figure 3.7 shows that there is a shift to smaller PGV values for larger distances, but the scaling with distance is not strong.

3.3 EVALUATION OF RESIDUALS

The within-event residuals for the horizontal crustal data are shown as functions of the $PSA(T_{PGV})$ in Figure 3.8 and as a function of rupture distance in Figure 3.9. The residuals in these two figures are shown for subsets of the data by magnitude bin to check that there is not a trade off between the magnitude scaling and either the $PSA(T_{PGV})$ scaling or the distance scaling. In these figures, there are no clear trends seen in the within-event residuals. The within-event residuals are shown as a function of the V_{S30} in Figure 3.10. Again, there are no trends seen in the within-event residuals.

The between-event residuals are shown as a function of magnitude in Figure 3.11. There is no trend with magnitude in the between-event residuals, but there are two outlier events at **M**3.7 (EQIDs 1092 and 1100 in the NGA-West2 database). The event terms for $PSA(T = 0.2)$ from Abrahamson et al. (2014) for these two events are not outliers; therefore, we did not remove these two earthquakes. The residuals for the vertical component for crustal earthquakes are not shown, but no significant trends were observed in either the within-event residuals or the between-event residuals for the vertical component.

To check the applicability of the conditional PGV model for near-fault directivity effects, the within-event residuals for recordings with near-fault velocity pulses are shown in Figure 3.12. The residuals are centered near zero: the mean residual for $M > 6.5$ is 0.06 natural log units. Similarly, to check the applicability of the conditional PGV model for HW effects, the within-event residuals for recordings from dipping faults—a dip less than 65 degrees—are shown in Figure 3.13 as a function of R_x (the horizontal distance measured perpendicular to fault strike). For $0 < R_x < 10$ km (HW side), the residuals are also centered near zero: the mean residual is 0.02 natural log units. These residual plots indicate that the near-fault effects on the PGV are captured in the observed $PSA(T_{PGV})$ values, and that the conditional PGV GMM is applicable to the near-fault region.

3.4 MODEL APPLICATION

The conditional PGV model developed in this study uses the $PSA(T)$ at different periods depending on the magnitude of the controlling earthquake, as given in Equation (3.6). Given a response spectrum, the value of the $PSA(T_{PGV})$ should be interpolated using log-log interpolation on the available $PSA(T)$ values.

The use of magnitude-dependent period is a strength of the model, but it also limits for applications in which the $PSA(T)$ values are only available for a few spectral periods. For example, design seismic hazard maps may only provide the PSA at a few spectral periods. In this case, the model based on the PSA at a single period needs to be used rather than using the magnitude-dependent period, $PSA(T_{PGV})$.

To be applicable to the case in which only PGA or $PSA(T = 1)$ values are available, the regression was repeated using the PGA and the $PSA(T = 1)$ values in place of the $PSA(T_{PGV})$ values. The PGV scaling using a fixed spectral period does not work well over a large magnitude range, so the dataset used for these two models was limited to earthquakes with $M > 5$. In addition, the standard deviation will become magnitude dependent due to the worse fit to the PGV data when using PGA and the $PSA(T = 1)$ values in place of the $PSA(T_{PGV})$. For example, using the PGA , the conditional GMM will provide a better fit to the smaller magnitudes because $T_{PGV}(M)$ is closer to the PGA for **M5** than for **M7**. To capture this effect, the standard deviation of the within-event terms is modeled using a tri-linear form shown in Equation (3.9). This same functional form is used for the standard deviation of the between-event residuals, τ .

$$\phi(M) = \begin{cases} \phi_1 & \text{for } M < M_1 \\ \phi_1 + (\phi_2 - \phi_1) \frac{(M - M_1)}{(M_2 - M_1)} & \text{for } M_1 \leq M \leq M_2 \\ \phi_2 & \text{for } M > M_2 \end{cases} \quad (3.9)$$

Table 3.3 lists the coefficients for the PGA -based and the $PSA(T = 1)$ -based conditional PGV models for the horizontal component. Design maps are for the horizontal component only, so PGA -based and the $PSA(T = 1)$ -based conditional PGV models are not included for the vertical component.

Given an estimate of the controlling magnitude and distance from disaggregation of the hazard, the models given in Table 3.3 can be used to estimate the PGV from either the PGA or the $PSA(T = 1)$. While not as accurate as the full conditional PGV model, this simplified approach still accommodates the differences in the aleatory variability between the $\ln(PSA)$ and the $\ln(PGV)$.

Table 3.1: Response spectral period with highest correlation to PGV by magnitude bin.

Mag Bin	Mean Mag	Horiz T_{PGV} (sec)	Vert T_{PGV} (sec)
3.0-3.5	3.4	0.20	0.15
3.5-4.5	4.0	0.28	0.22
4.5-5.5	5.0	0.40	0.32
5.5-6.5	6.1	0.95	1.1
6.5-7.5	6.9	1.4	1.3
7.5-8.5	7.6	2.8	3.0

Table 3.2: Conditional PGV model coefficients for crustal earthquakes.

Coeff	Horizontal	Std Err	Vertical	Std Err
a_1	5.39	0.06	5.51	0.06
a_2	0.799	0.004	0.763	0.004
a_3	0.654	0.008	0.538	0.010
a_4	0.479	0.056	0.131	0.060
a_5	-0.062	0.008	-0.106	0.008
a_6	-0.359	0.007	-0.431	0.008
a_7	-0.134	0.007	-0.089	0.008
a_7	0.023	0.005	0.017	0.006
ϕ	0.29		0.32	
τ	0.16		0.15	
σ	0.33		0.35	

Table 3.3: Coefficients for PGA -based and $PSA(T = 1)$ -based models for PGV for crustal earthquakes

Coeff	Horizontal PGA Model	Horizontal PSA(T=1) Model
a_1	4.77	4.80
a_2	0.738	0.82
a_3	0.484	0.55
a_4	0.275	0.27
a_5	-0.036	0.054
a_6	-0.332	-0.382
a_7	-0.44	-0.21
a_8	0.0	0.0
ϕ_1	0.32	0.28
ϕ_2	0.42	0.38
τ_1	0.12	0.12
τ_2	0.26	0.17
σ_1	0.34	0.30
σ_2	0.49	0.42
M_1	5.0	5.0
M_2	7.0	7.0

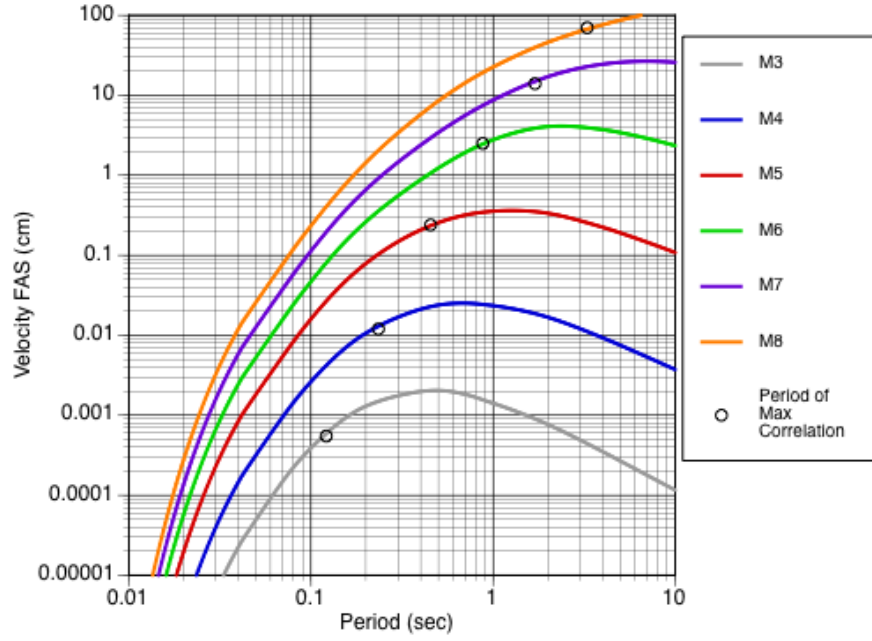


Figure 3.1: Horizontal velocity FAS for different magnitudes for crustal earthquakes at a distance of 30 km and for a site with $V_{S30} = 400$ m/sec from the Bayless and Abrahamson (2019) model. The circles show the period with the highest correlation between $\ln(PGV)$ and $\ln[PSA(T)]$.

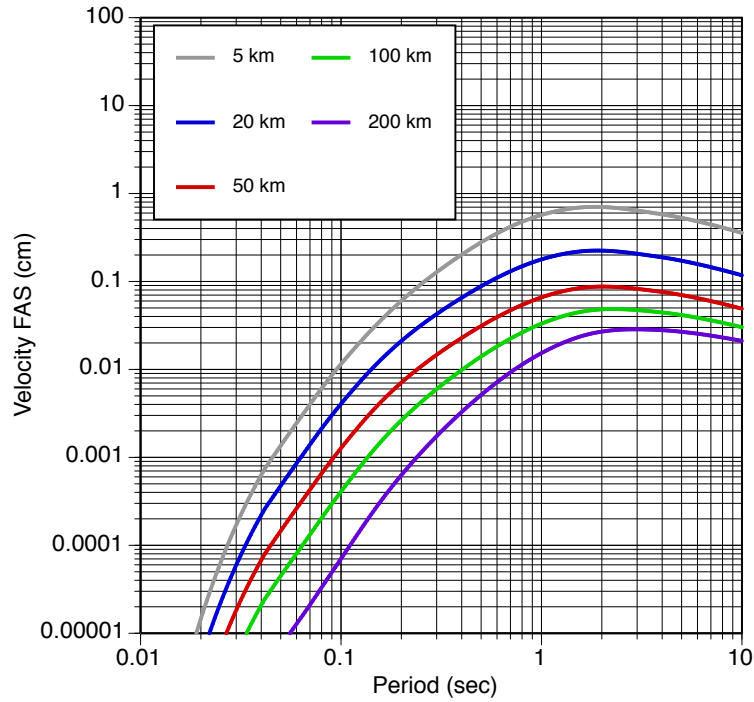


Figure 3.2: Horizontal velocity FAS for M6 at different rupture distances for a site with $V_{S30} = 400$ m/sec from the Bayless and Abrahamson (2019) model.

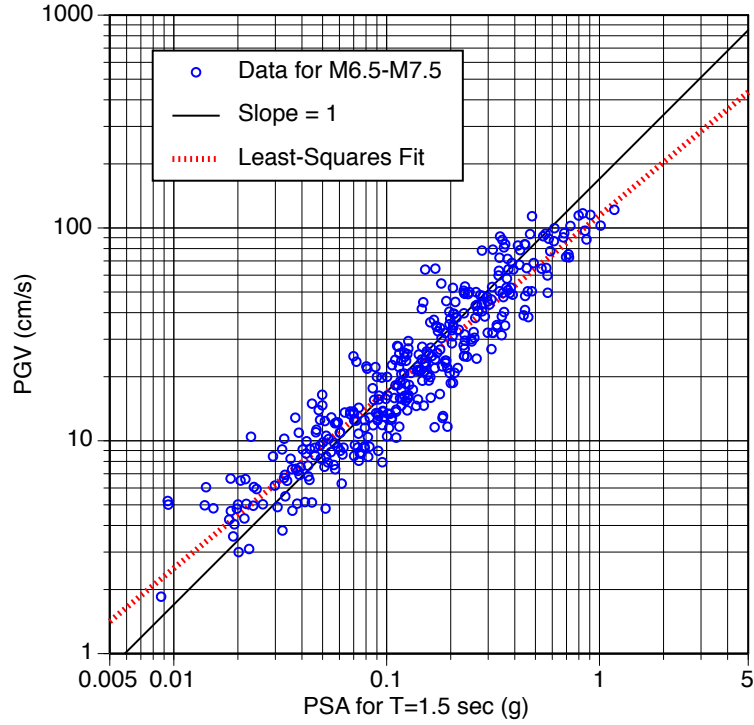


Figure 3.3: Example of the relation between the $\ln(PGV)$ and $\ln[PSA(T = 1.5)]$ for crustal earthquakes with magnitudes between 6.5 and 7.5 at distances less than 50 km. The slope is less than unity.

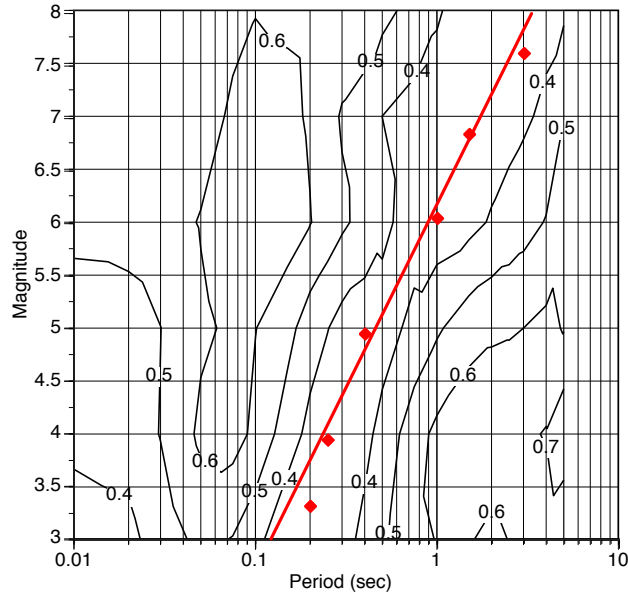


Figure 3.4: Standard deviation of the linear fit of $\ln(PGV)$ for crustal earthquakes as a function of $\ln[PSA(T)]$ computed by magnitude bin.

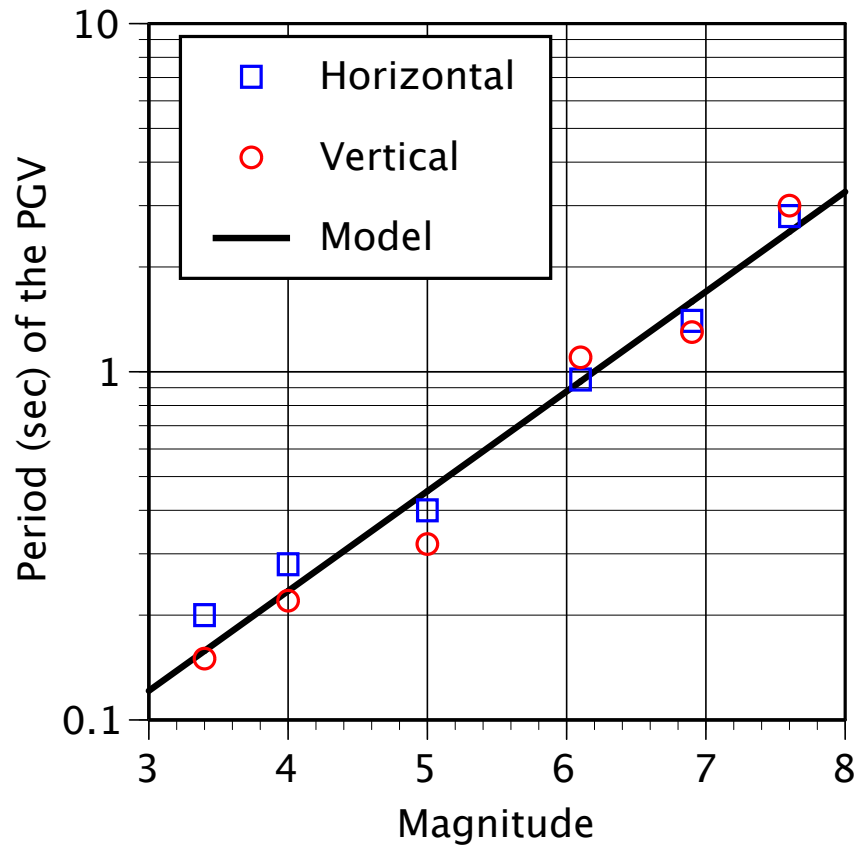


Figure 3.5: Magnitude dependence of the period with highest correlation between PGV and $PSA(T)$.

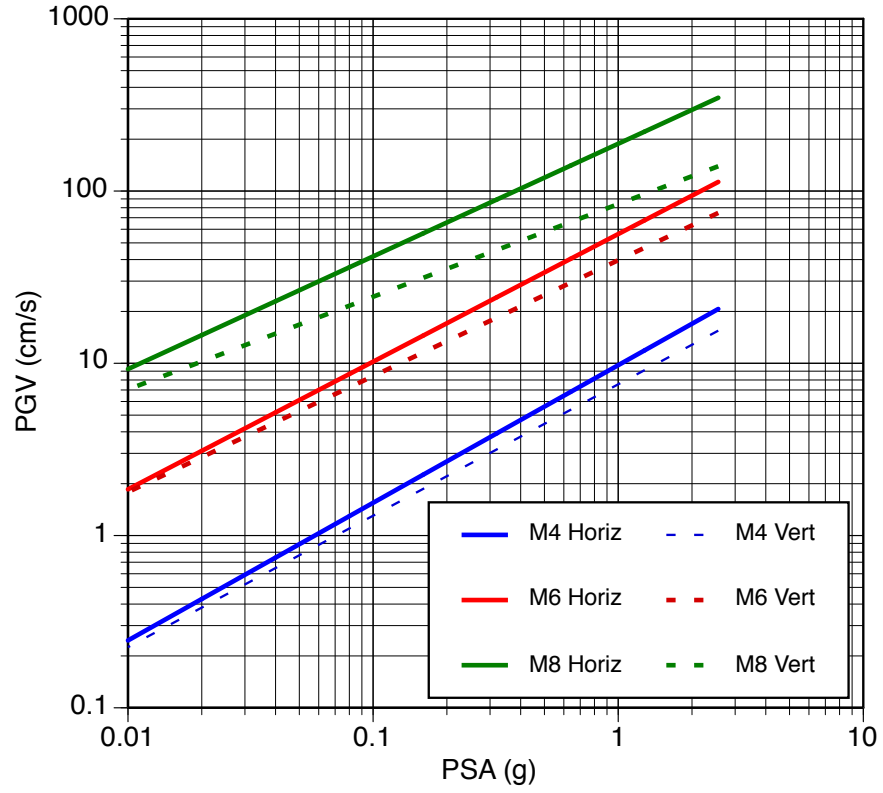


Figure 3.6: $PSA(T_{PGV})$ scaling of the conditional PGV model for $R_{RUP} = 10$ km and $V_{S30} = 425$ m/sec for magnitudes M4 to M8 for both the horizontal and vertical components.

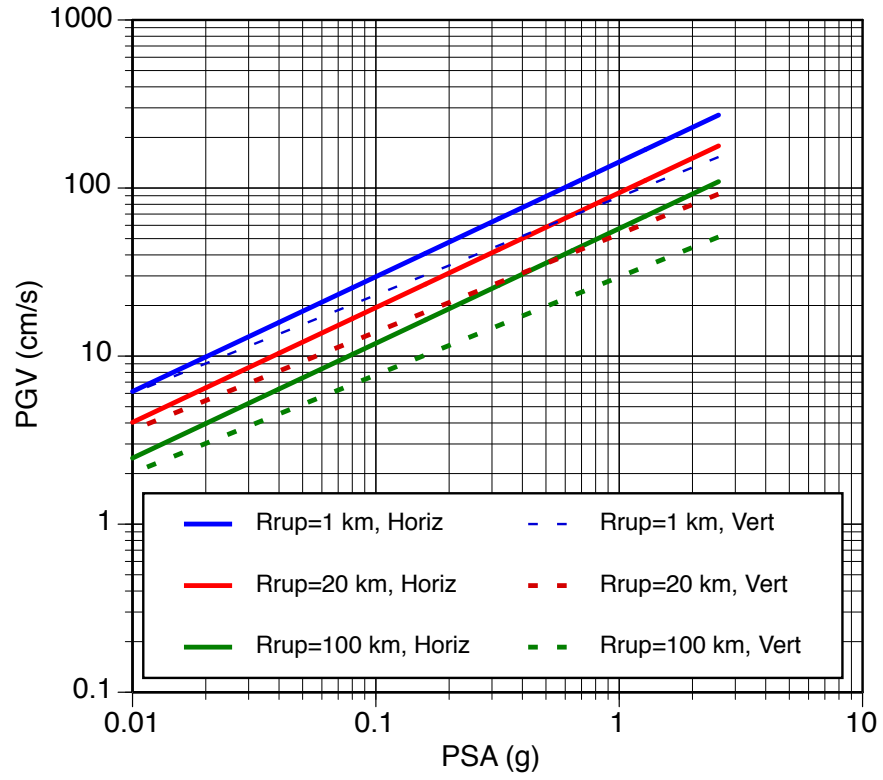


Figure 3.7: $PSA(T_{PGV})$ scaling of the conditional PGV model for $M = 7$ and $V_{S30} = 425$ m/sec for R_{RUP} from 1 to 100 km for both the horizontal and vertical components.

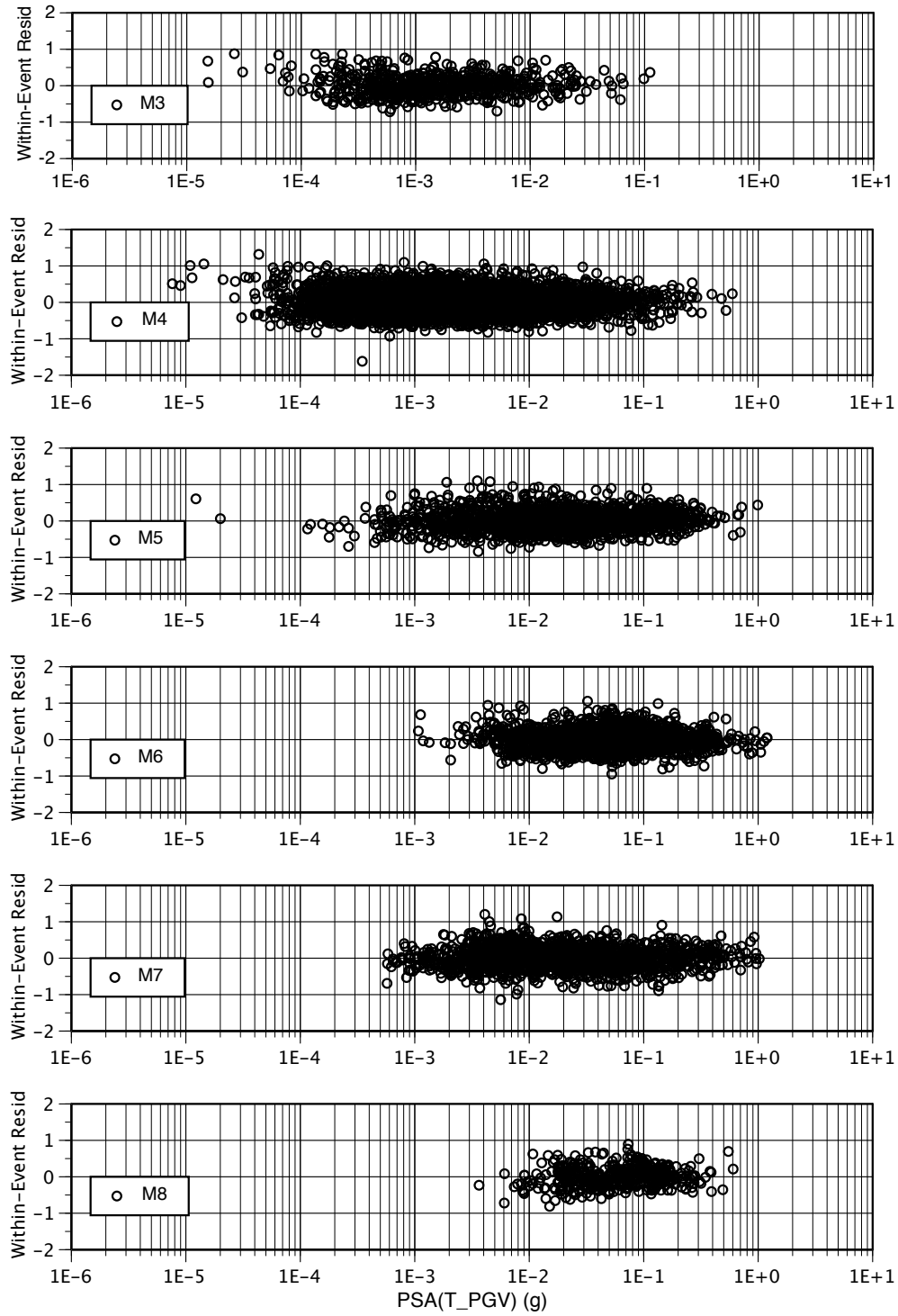


Figure 3.8: $PSA(T_{PGV})$ dependence of the within-event residuals for the horizontal component.

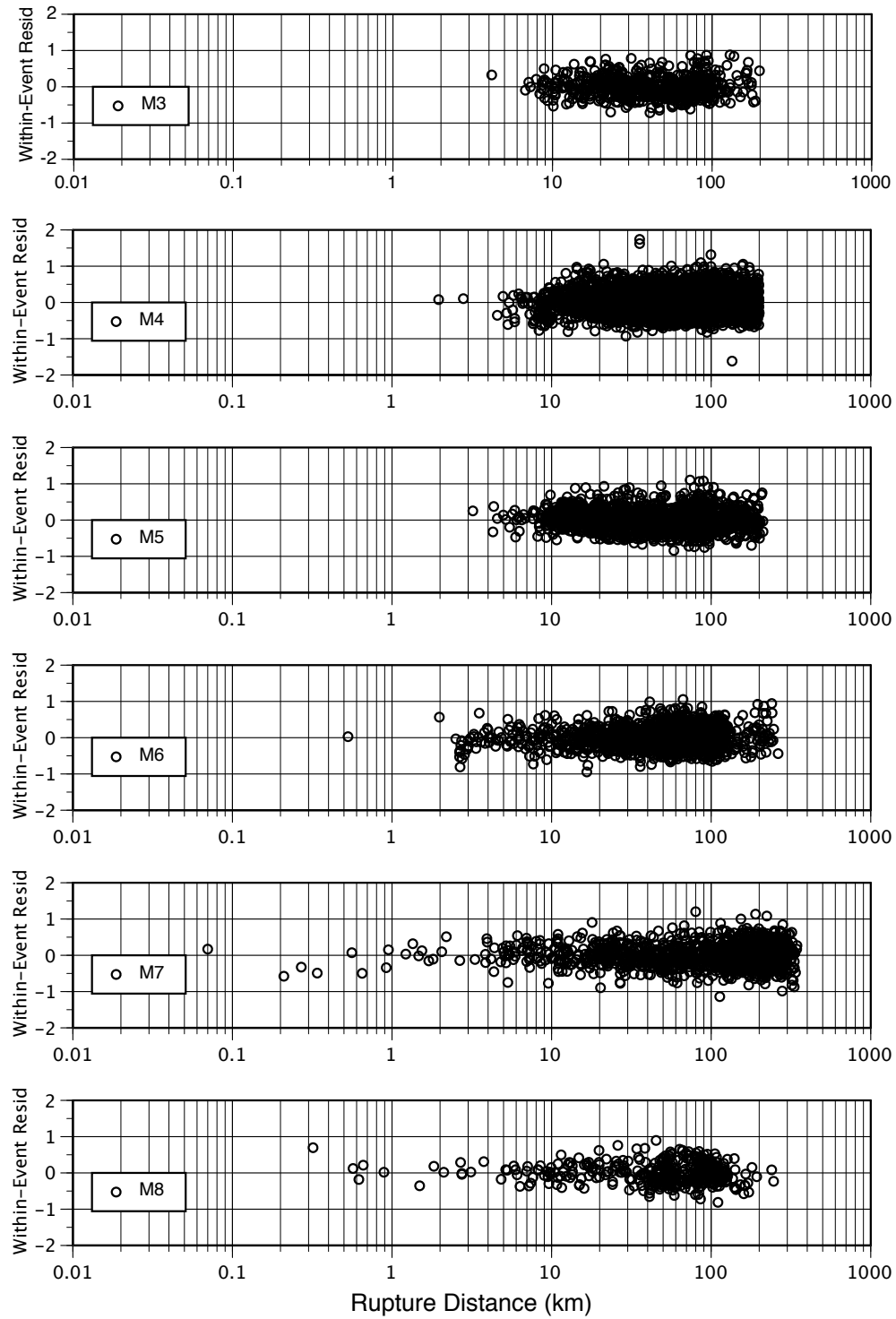


Figure 3.9: Distance dependence of the within-event residuals for the horizontal component.

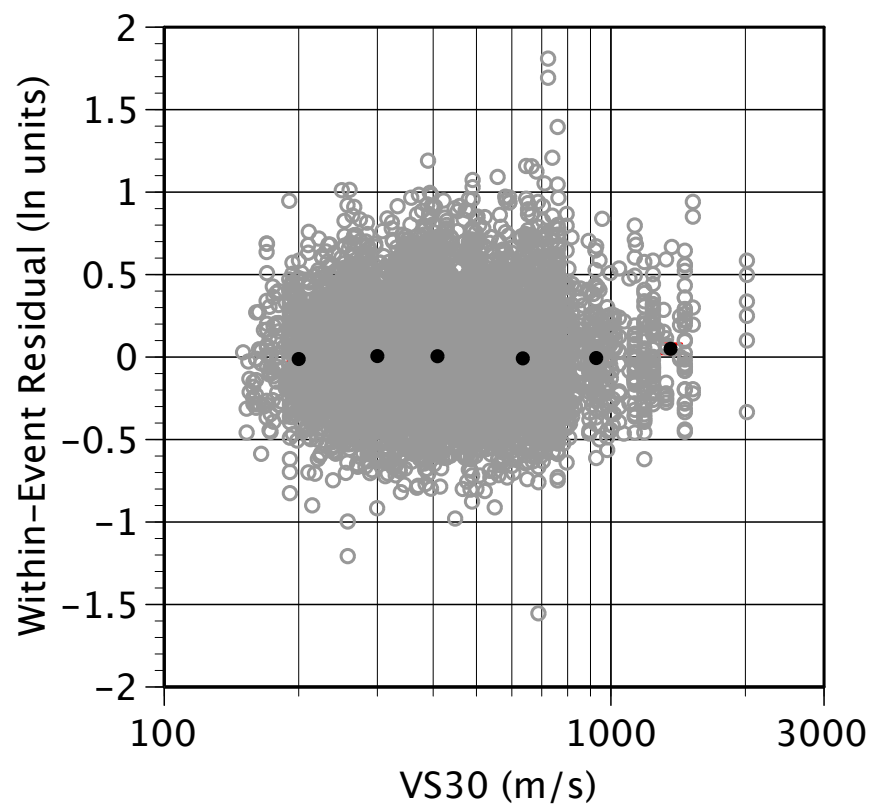


Figure 3.10: V_{S30} dependence of the within-event residuals for the horizontal component. The black symbols are the mean values by V_{S30} bin.

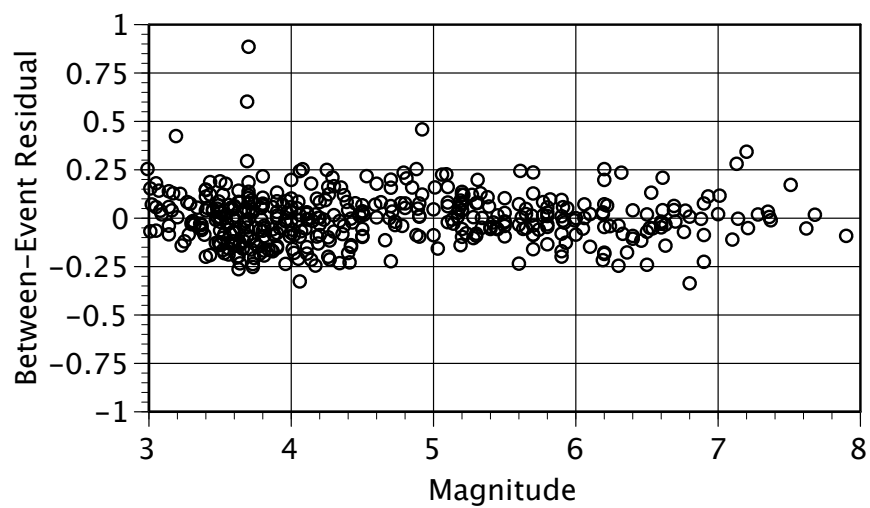


Figure 3.11: Between-event residuals for the horizontal component.

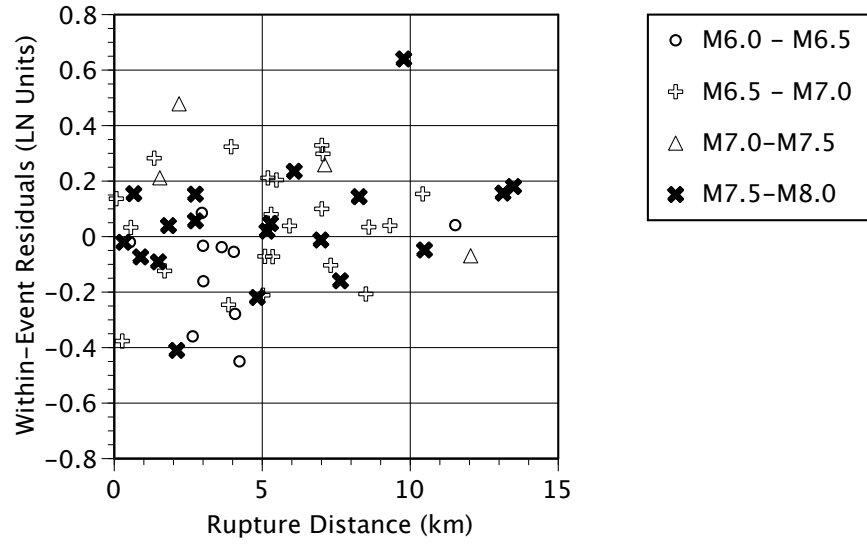


Figure 3.12: Within-event residuals of the conditional *PGV* model for near-fault ground motions with velocity pulses.

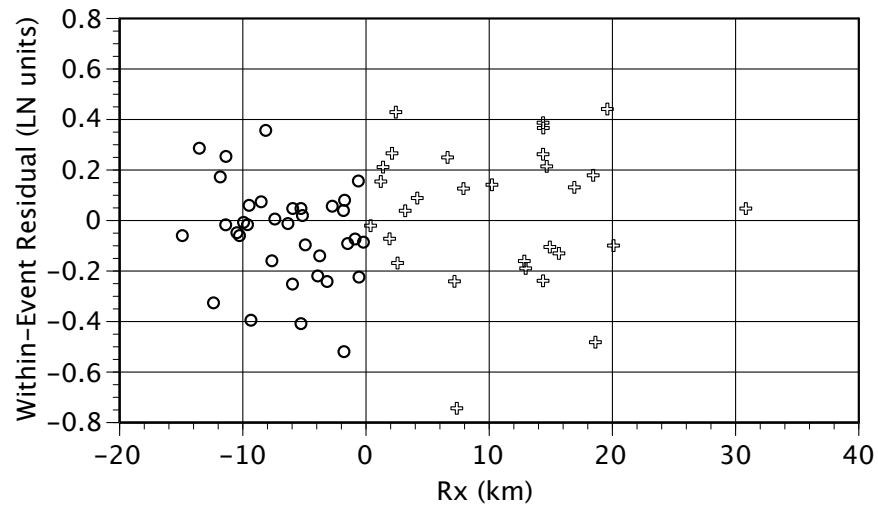


Figure 3.13: Within-event residuals of the conditional *PGV* model for near-fault ground motions for dipping faults. The sites with positive R_x are on the HW side and sites with negative R_x are on the footwall side.

4 Converting Conditional GMMs to Traditional GMMs

The conditional PGV model can be converted to a traditional scenario-based PGV model by combining it with a GMM for the $\ln[SA(T_{PGV})]$ values. The median PGV is computed by using the median $PSA(T_{PGV})$ from the GMM as input to the conditional GMM for PGV . The aleatory variability is computed using the propagation of errors given in Equation (3.2).

4.1 MEDIAN MODEL

Figure 4.1 shows the resulting median PGV values from the conditional models compared to the geometric mean of the PGV from the four NGA-W2 PGV GMMs for strike-slip earthquakes with magnitudes between 3 and 8 for a rupture distance of 20 km and a stiff-soil site condition. For this example, the geometric mean of the RotD50 $PSA(T)$ values from the four GMMs is computed and combined with the previous conditional PGV models and the conditional PGV model developed in this study. The PGV estimates from all four conditional PGV models are similar for the **M**6.0 to **M**6.5 range, which is near the center of the data available for the previous studies. The Newmark and Hall (1982) and Bommer and Alarcon (2006) models do not include a magnitude term, which results in weaker magnitude scaling above **M**6.5 for these two models than observed in the GMMs. The Huang and Whittaker (2015) model includes a magnitude scaling term, and this model is consistent with NGA-W2 PGV GMMs for $M > 6$. The model developed in this study captures the magnitude scaling in the PGV GMMs over the full range of magnitudes.

Figure 4.2 shows the PGV resulting from the four individual scenario-based PGV models as a function of magnitude along with the median PGV from the four NGA-West2 GMMs. The four scenario-based models all capture the curvature in the magnitude scaling from **M**3 to **M**8. There is only a small epistemic range in the median PGV , given the $PSA(T_{PGV})$ values. For this distance, there is adequate data to constrain the GMMs, so the four GMMs yield similar $PSA(T)$ values. The largest epistemic range is related to differences in break points in the magnitude scaling for the four GMMs, causing kinks in the magnitude scaling.

4.2 ALEATORY VARIABILITY

The aleatory variability of the $\ln(PGV)$ for a given earthquake scenario is computed using simple propagation of errors shown in Equation (3.2). With the functional form of the conditional PGV model given in Equation (3.7):

$$\frac{\partial \ln PGV}{\partial \ln PSA(T_{PGV})} = f_1(M) \quad (4.1)$$

The aleatory variability is then given by:

$$\sigma_{\ln PGV}^2 = f_1^2(M) \sigma_{\ln PSA(T_{PGV})}^2 + \sigma_{\ln PGV|PSA(T_{PGV})}^2 \quad (4.2)$$

Using the average of the NGA-West2 GMMs, the standard deviation of the $\ln(PGV)$ and the $PSA(T_{PGV})$ are shown in Table 4.1 for magnitudes of 3, 4, 5, 6, 7, and 8 at a distance of 30 km. Using these values, the standard deviation of the $\ln(PGV)$ given by the average of the NGA-West2 GMMs is compared to the standard deviation computed using Equation (4.2) in Figure 4.3. The standard deviation computed using the conditional PGV model shows a similar magnitude dependence of $\sigma_{\ln PGV}$ as given by the average of the four NGA-West2 GMMs for PGV .

Figure 4.3 also shows the standard deviations computed using the approaches recommended by Bommer and Alarcon (2006) and by Huang and Whittaker (2015). Bommer and Alarcon (2006) recommend using the standard deviation of the $PSA(T = 0.5)$ without considering the $\sigma_{\ln PGV|PSA(T_{PGV})}$ term, whereas Huang and Whittaker (2015) recommend adding the variance of the conditional PGV model to the variance of the $PSA(T = 1)$. In this comparison, the standard deviations from the ASK14 model are used for the $\sigma_{\ln PSA}$ terms; see Abrahamson et al. (2014). The Bommer and Alarcon (2006) approach overestimates the standard deviation by 0.05 to 0.1 natural log units, which simply reflects the difference between the standard deviation of $\ln(PGV)$ and $\ln[PSA(T = 0.5)]$. The Huang and Whittaker (2015) approach overestimates the standard deviation of the PGV by about 0.2 natural log units. This large overestimation results from both the larger standard deviation of $\ln[PSA(T = 1)]$ compared to $\ln(PGV)$ and the addition of the variability from the conditional PGV model. This comparison demonstrates the value of allowing the slope of the $\ln(PSA)$ term to be different from unity for computing appropriate standard deviations of the $\ln(PGV)$ for a given scenario.

The results using the conditional model based on PGA or $PSA(T = 1)$ are shown in Figure 4.4. These models lead to similar PGV values, but they do not fit the scaling over the full magnitude range as well as the model using a magnitude-dependent period, T_{PGV} . The aleatory standard deviations computed using the PGA or the $PSA(T = 1)$ conditional models are shown in Figure 4.5. The conditional model based on $PSA(T = 1)$ gives similar standard deviations, but the conditional model based on PGA underestimates the standard deviation.

Table 4.1: Standard deviation for unconditional $\ln(PGV)$ for crustal earthquakes, horizontal component.

Mag	T_{PGV}	$f_1(M)$	NGA-W2		$\sigma_{\ln PGV}$	
			$\sigma_{\ln[PSA(T_{PGV})]}$	$\sigma_{\ln PGV PSA(T_{PGV})}$	This Study	NGA-W2
3	0.12	0.819	0.86	0.33	0.78	0.75
4	0.23	0.819	0.84	0.33	0.75	0.75
5	0.45	0.819	0.76	0.33	0.70	0.70
6	0.88	0.772	0.72	0.33	0.65	0.62
7	1.7	0.724	0.71	0.33	0.61	0.60
8	3.3	0.677	0.71	0.33	0.58	0.60

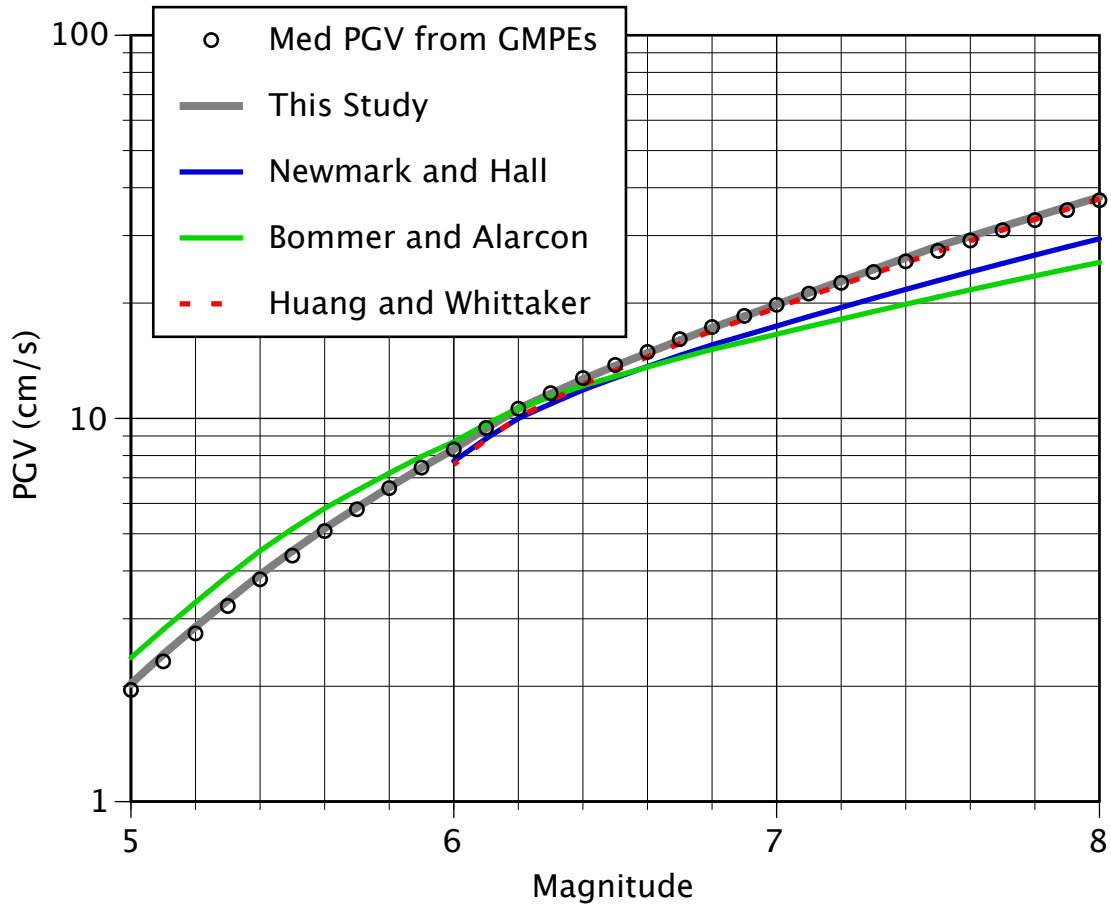


Figure 4.1: Comparison of the magnitude scaling for the conditional PGV model for the horizontal component. The $PSA(T)$ is for the median spectrum from four NGA-West2 GMMs from a strike-slip earthquake at a rupture distance of 20 km at a stiff-soil site conditions ($V_{S30} = 400$ m/sec).

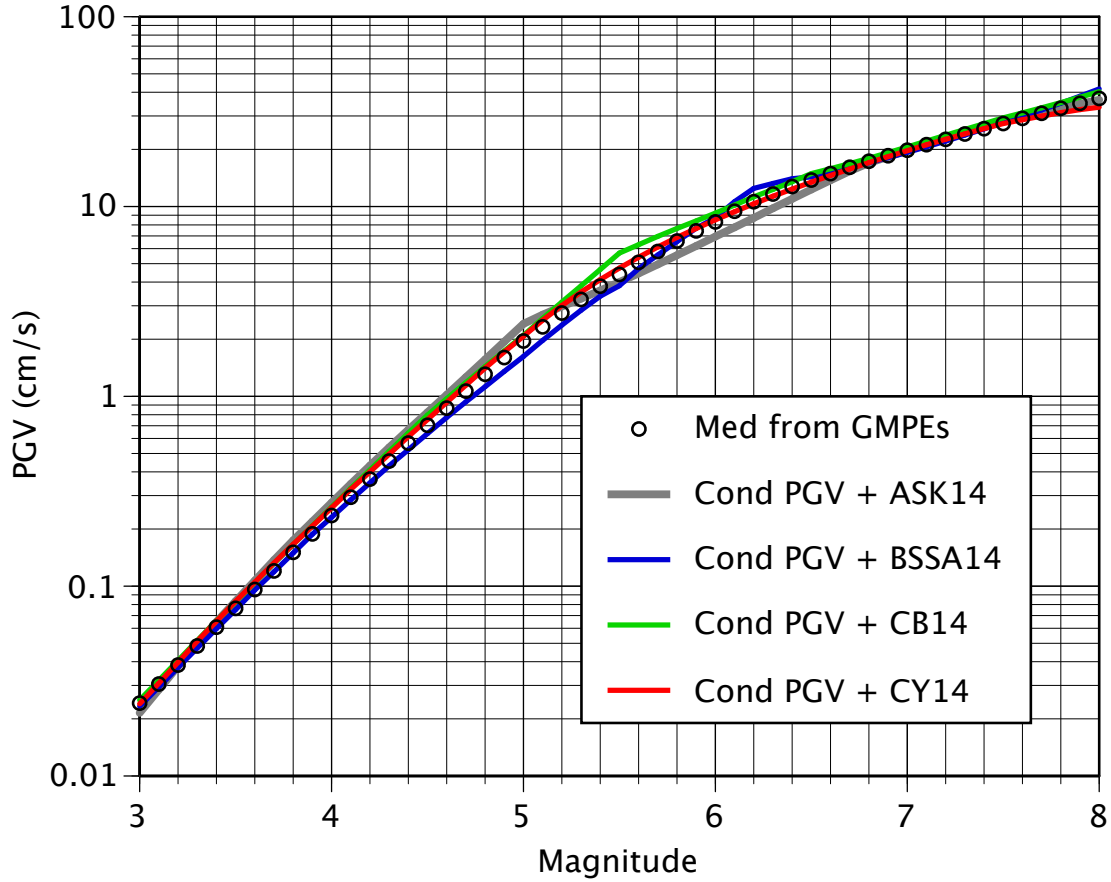


Figure 4.2: Comparison of the magnitude scaling for the horizontal component PGV using four different GMMs to compute the $PSA(T)$ values for the median spectrum from a strike-slip earthquake at a rupture distance of 20 km at a stiff-soil site conditions. The four GMMs used are: ASK14 = Abrahamson et al. (2014); BSSA14 = Boore et. al. (2014); CB14 = Campbell and Bozorgnia (2014); and CY14 = Chiou and Youngs (2014).

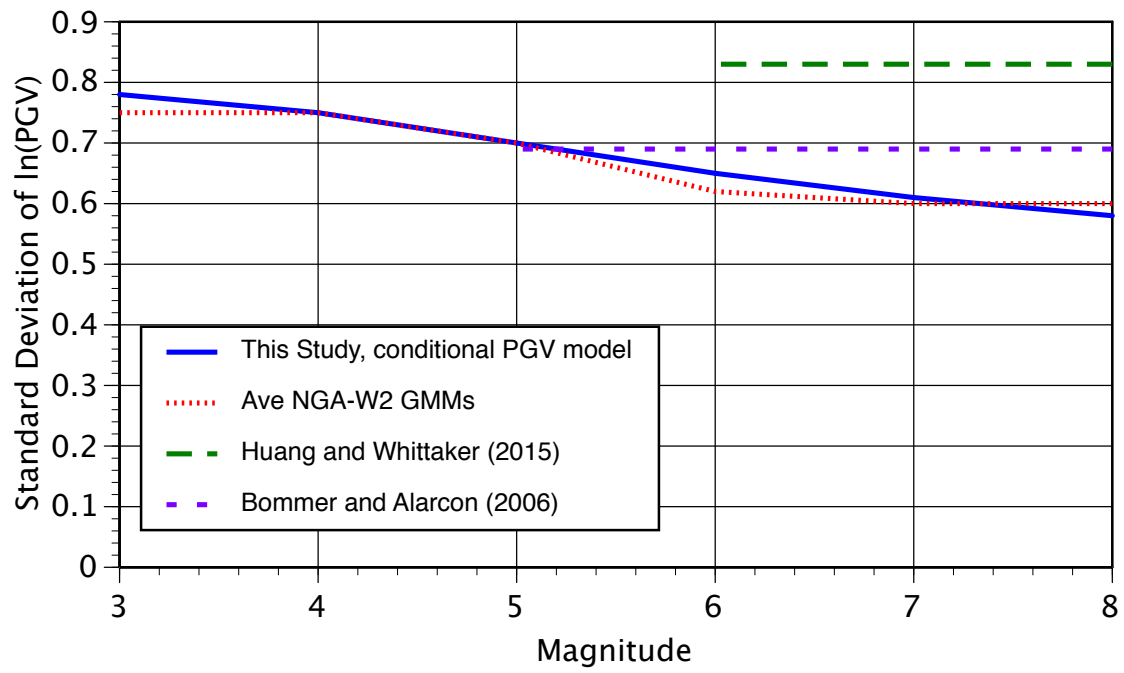


Figure 4.3: Magnitude dependence of the aleatory standard deviation for $\ln(PGV)$ for crustal earthquakes, horizontal component for a distance of 20 km.

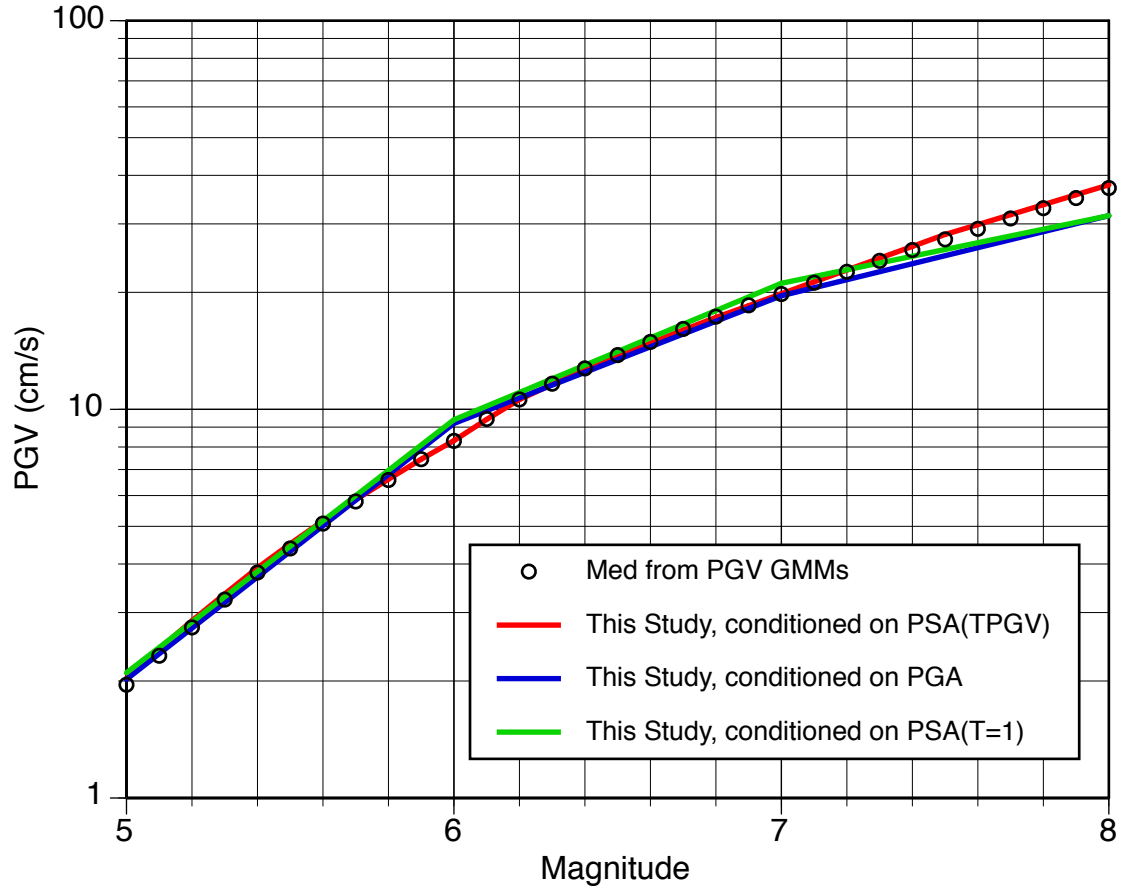


Figure 4.4: Magnitude scaling at a rupture distance of 20 km for the PGA and $PSA(T = 1)$ models compared to the scaling for model based on $PSA(T_{PGV})$.

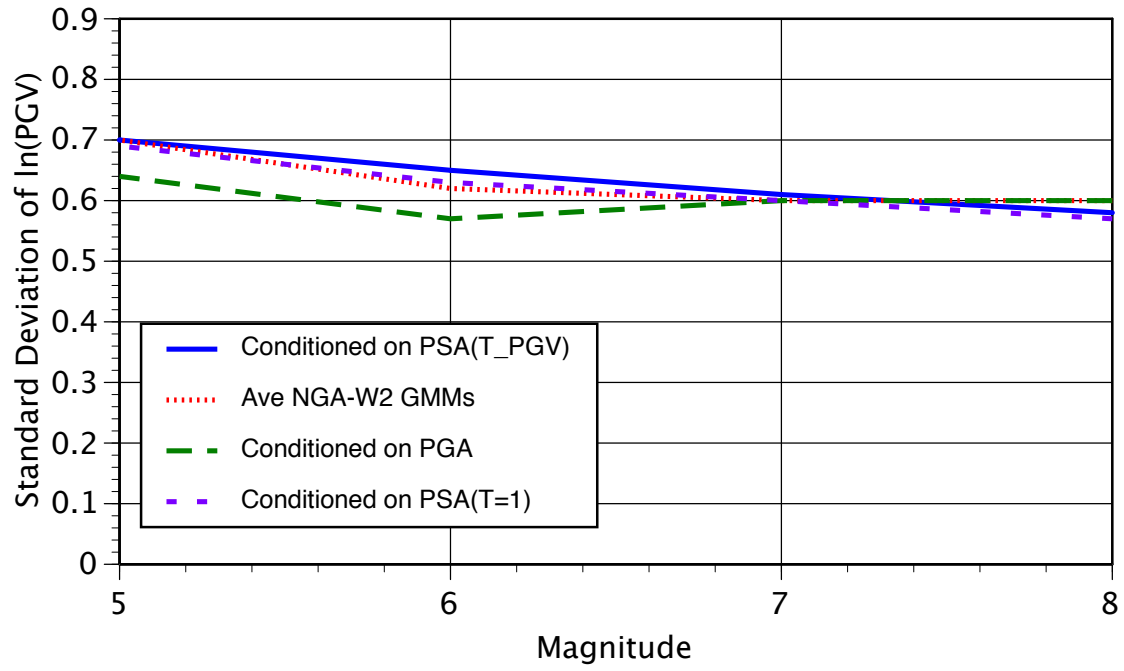


Figure 4.5: Comparison of the aleatory standard deviation computed using the models conditioned on PGA and $PSA(T = 1)$ compared to the standard deviation for the conditional model based on $PSA(T_{PGV})$.

5 Conclusions

Conditional ground-motion models are useful for developing design values for secondary ground-motion parameters consistent with the design response spectral values. While models for the $PGV/PSA(T)$ ratio have been developed in previous studies, our model uses a magnitude-dependent spectral period that captures a key physical behaviour of earthquake ground motion: the corner frequency is magnitude dependent. With a proper physical basis, the conditional models can be reliably extrapolated outside of the range that is constrained by the empirical data. For engineering applications, we judge that the conditional PGV models developed in this study can be reliably extrapolated up to **M**8.5 for crustal earthquakes based on the magnitude scaling of the corner frequency.

The conditional PGV models can also be combined with appropriate GMMs for $PSA(T)$ to develop traditional GMMs for PGV . Because the conditional models use the $PSA(T)$ values as predictive parameters, they show less regional differences than traditional GMMs. That is, the regional differences are captured in the $PSA(T)$ values; therefore, a global ergodic conditional GMM is more likely to be applicable to many different regions than a traditional GMM. Due to the use of non-unity slopes for the $\ln[PSA(T)]$ dependence in our conditional GMM, an appropriate aleatory standard deviation of the resulting $\ln(PGV)$ can be computed, avoiding the over-prediction of the aleatory standard deviation seen in previous models.

REFERENCES

- Abrahamson N.A., Shi H-J, Yang B. (2014). Ground-motion prediction equations for Arias intensity consistent with the NGA-West2 ground-motion models, *PEER Report No. 2016/05*, Pacific Earthquake Engineering Research Center, University of California, Berkeley, CA.
- Abrahamson N.A. Silva W.J. (1992). Empirical response spectral attenuation relations for shallow crustal earthquakes, *Seismol. Res. Lett.*, 68(1): 94–127.
- Abrahamson N.A., Silva W.J., Kamai R. (2014). Summary of the ASK14 ground motion relation for active crustal regions, *Earthq. Spectra*, 30(3): 1025–1055.
- Abrahamson N.A., Youngs R.R. (1992). A stable algorithm for regression analysis using the random effects model, *Bull. Seismol. Soc. Am.*, 82(1): 505–510.
- Ancheta T., Darragh R., Stewart J.P., Seyhan E., Silva W.J., Chiou B., Wooddell K., Graves R.W., Kottke A., Boore D.M., Kishida T., Donahue J. (2014). NGA-West2 Database, *Earthq. Spectra*, 30(3): 989–1005.
- Baker J., Cornell C.A. (2006). Spectral shape, epsilon and record selection, *Earthq. Eng. Struct. Dyn.*, 35(9): 1077–1095.
- Bayless J., Abrahamson N.A. (2019). Summary of the BA18 ground-motion model for Fourier spectra for crustal earthquakes in California, *Bull. Seismol. Soc. Am.*, 109: 2088–2105.
- Bommer J., Alarcon J. (2006). The prediction and use of peak ground velocity, *J. Earthq. Eng.*, 10(1): 1–31.
- Boore D.M., Stewart J.P., Seyhan E., Atkinson G.M. (2014). NGA-W2 equations for predicting PGA, PGV, and 5% damped PSA for shallow crustal earthquakes, *Earth. Spectra*, 30(3): 1057–1085.
- Campbell K.W., Bozorgnia Y. (2014). NGA-West2 ground motion model for the average horizontal components of PGA, PGV, and 5% damped linear acceleration response spectra, *Earthq. Spectra*, 30(3): 1087–1115.
- Chiou B.S.-J., Youngs R.R. (2014). Update of the Chiou and Youngs NGA model for the average horizontal component of peak ground motion and response spectra, *Earthq. Spectra*, 30(3): 1117–1153.
- FEMA (2018). *Seismic Performance of Buildings, FEMA 58-1*, Federal Emergency Management Agency, Washington, D.C.
- Gregor N., Abrahamson N.A., Atkinson G.M., Boore D.M., Bozorgnia Y., Campbell K.W., Chiou B.-S.J., Idriss I.M., Kamai R., Seyhan E., Silva W.J., Stewart J.P., Youngs R.R. (2014). Comparison of NGA-West2 GMMs, *Earthq. Spectra*, 30(3): 1179–1197.

Newmark N., Hall W.J. (1982). *Earthquake Spectra and Design*, Earthquake Engineering Research Institute, Oakland, CA, 103 pgs.

Huang Y.-N., Whittaker A. (2015). On the calculation of peak ground velocity for seismic performance assessment, *Earthq. Spectra*, 31: 785–794.

PEER REPORTS

PEER reports are available as a free PDF download from <https://peer.berkeley.edu/peer-reports>. In addition, printed hard copies of PEER reports can be ordered directly from our printer by following the instructions at <https://peer.berkeley.edu/peer-reports>. For other related questions about the PEER Report Series, contact the Pacific Earthquake Engineering Research Center, 325 Davis Hall, Mail Code 1792, Berkeley, CA 94720. Tel.: (510) 642-3437; and Email: peer_center@berkeley.edu.

- PEER 2020/04** *Partially Non-Ergodic Ground-Motion Model for Subduction Regions using the NGA-Subduction Database.* Nicolas Kuehn, Yousef Bozorgnia, Kenneth W. Campbell, and Nicholas Gregor. September 2020.
- PEER 2020/03** *NGA-Subduction Global Ground-Motion Models with Regional Adjustment Factors.* Grace A. Parker, Jonathan P. Stewart, David M. Boore, Gail M. Atkinson, and Behzad Hassani. September 2020.
- PEER 2020/02** *Data Resources for NGA-Subduction Project.* Yousef Bozorgnia (PI) and Jonathan P. Stewart (Editor). March 2020.
- PEER 2020/01** *Modeling Viscous Damping in Nonlinear Response History Analysis for Steel Moment-Frame Buildings.* Xin Qian, Anil K. Chopra, and Frank McKenna. June 2020.
- PEER 2019/09** *Seismic Behavior of Special Concentric Braced Frames under Short- and Long-Duration Ground Motions.* Ali Hammad and Mohamed A. Moustafa. December 2019.
- PEER 2019/08** *Influence of Vertical Ground Motion on Bridges Isolated with Spherical Sliding Bearings.* Rushil Mojidra and Keri L. Ryan. December 2019.
- PEER 2019/07** *PEER Hub ImageNet (ϕ -Net): A Large-Scale Multi-Attribute Benchmark Dataset of Structural Images.* Yuqing Gao, and Khalid. M. Mosalam. November 2019.
- PEER 2019/06** *Fluid-Structure Interaction and Python-Scripting Capabilities in OpenSees.* Minjie Zhu and Michael H. Scott. August 2019.
- PEER 2019/05** *Expected Earthquake Performance of Buildings Designed to the California Building Code (California Alfred E. Alquist Seismic Safety Publication 19-01).* Grace S. Kang, Sifat Muin, Jorge Archbold, Bitanoosh Woods, and Khalid Mosalam. July 2019.
- PEER 2019/04** *Aftershock Seismic Vulnerability and Time-Dependent Risk Assessment of Bridges.* Sujith Mangalathu, Mehrdad Shokrabadi, and Henry V. Burton. May 2019.
- PEER 2019/03** *Ground-Motion Directivity Modeling for Seismic Hazard Applications.* Jennifer L. Donahue, Jonathan P. Stewart, Nicolas Gregor, and Yousef Bozorgnia. Review Panel: Jonathan D. Bray, Stephen A. Mahin, I. M. Idriss, Robert W. Graves, and Tom Shantz. May 2019.
- PEER 2019/02** *Direct-Finite-Element Method for Nonlinear Earthquake Analysis of Concrete Dams Including Dam–Water–Foundation Rock Interaction.* Arnkjell Løkke and Anil K. Chopra. March 2019.
- PEER 2019/01** *Flow-Failure Case History of the Las Palmas, Chile, Tailings Dam.* R. E. S. Moss, T. R. Gebhart, D. J. Frost, and C. Ledezma. January 2019.
- PEER 2018/08** *Central and Eastern North America Ground-Motion Characterization: NGA-East Final Report.* Christine Goulet, Yousef Bozorgnia, Norman Abrahamson, Nicolas Kuehn, Linda Al Atik, Robert Youngs, Robert Graves, and Gail Atkinson. December 2018.
- PEER 2018/07** *An Empirical Model for Fourier Amplitude Spectra using the NGA-West2 Database.* Jeff Bayless, and Norman A. Abrahamson. December 2018.
- PEER 2018/06** *Estimation of Shear Demands on Rock-Socketed Drilled Shafts subjected to Lateral Loading.* Pedro Arduino, Long Chen, and Christopher R. McGann. December 2018.
- PEER 2018/05** *Selection of Random Vibration Procedures for the NGA-East Project.* Albert Kottke, Norman A. Abrahamson, David M. Boore, Yousef Bozorgnia, Christine Goulet, Justin Hollenback, Tadahiro Kishida, Armen Der Kiureghian, Olga-Joan Ktenidou, Nicolas Kuehn, Ellen M. Rathje, Walter J. Silva, Eric Thompson, and Xiaoyue Wang. December 2018.
- PEER 2018/04** *Capturing Directivity Effects in the Mean and Aleatory Variability of the NGA-West 2 Ground Motion Prediction Equations.* Jennie A. Watson-Lamprey. November 2018.
- PEER 2018/03** *Probabilistic Seismic Hazard Analysis Code Verification.* Christie Hale, Norman Abrahamson, and Yousef Bozorgnia. July 2018.

- PEER 2018/02** *Update of the BCHydro Subduction Ground-Motion Model using the NGA-Subduction Dataset.* Norman Abrahamson, Nicolas Kuehn, Zeynep Gulerce, Nicholas Gregor, Yousef Bozorgnia, Grace Parker, Jonathan Stewart, Brian Chiou, I. M. Idriss, Kenneth Campbell, and Robert Youngs. June 2018.
- PEER 2018/01** *PEER Annual Report 2017–2018.* Khalid Mosalam, Amarnath Kasalanati, and Selim Günay. June 2018.
- PEER 2017/12** *Experimental Investigation of the Behavior of Vintage and Retrofit Concentrically Braced Steel Frames under Cyclic Loading.* Barbara G. Simpson, Stephen A. Mahin, and Jiun-Wei Lai, December 2017.
- PEER 2017/11** *Preliminary Studies on the Dynamic Response of a Seismically Isolated Prototype Gen-IV Sodium-Cooled Fast Reactor (PGSFR).* Benshun Shao, Andreas H. Schellenberg, Matthew J. Schoettler, and Stephen A. Mahin. December 2017.
- PEER 2017/10** *Development of Time Histories for IEEE693 Testing and Analysis (including Seismically Isolated Equipment).* Shakhzod M. Takhirov, Eric Fujisaki, Leon Kempner, Michael Riley, and Brian Low. December 2017.
- PEER 2017/09** *“R” Package for Computation of Earthquake Ground-Motion Response Spectra.* Pengfei Wang, Jonathan P. Stewart, Yousef Bozorgnia, David M. Boore, and Tadahiro Kishida. December 2017.
- PEER 2017/08** *Influence of Kinematic SSI on Foundation Input Motions for Bridges on Deep Foundations.* Benjamin J. Turner, Scott J. Brandenburg, and Jonathan P. Stewart. November 2017.
- PEER 2017/07** *A Nonlinear Kinetic Model for Multi-Stage Friction Pendulum Systems.* Paul L. Drazin and Sanjay Govindjee. September 2017.
- PEER 2017/06** *Guidelines for Performance-Based Seismic Design of Tall Buildings, Version 2.02.* TBI Working Group led by co-chairs Ron Hamburger and Jack Moehle: Jack Baker, Jonathan Bray, C.B. Crouse, Greg Deierlein, John Hooper, Marshall Lew, Joe Maffei, Stephen Mahin, James Malley, Farzad Naeim, Jonathan Stewart, and John Wallace. May 2017.
- PEER 2017/05** *Recommendations for Ergodic Nonlinear Site Amplification in Central and Eastern North America.* Youssef M.A. Hashash, Joseph A. Harmon, Okan Ilhan, Grace A. Parker, and Jonathan P. Stewart. March 2017.
- PEER 2017/04** *Expert Panel Recommendations for Ergodic Site Amplification in Central and Eastern North America.* Jonathan P. Stewart, Grace A. Parker, Joseph P. Harmon, Gail M. Atkinson, David M. Boore, Robert B. Darragh, Walter J. Silva, and Youssef M.A. Hashash. March 2017.
- PEER 2017/03** *NGA-East Ground-Motion Models for the U.S. Geological Survey National Seismic Hazard Maps.* Christine A. Goulet, Yousef Bozorgnia, Nicolas Kuehn, Linda Al Atik, Robert R. Youngs, Robert W. Graves, and Gail M. Atkinson. March 2017.
- PEER 2017/02** *U.S.–New Zealand–Japan Workshop: Liquefaction-Induced Ground Movements Effects, University of California, Berkeley, California, 2–4 November 2016.* Jonathan D. Bray, Ross W. Boulanger, Misko Cubrinovski, Kohji Tokimatsu, Steven L. Kramer, Thomas O’Rourke, Ellen Rathje, Russell A. Green, Peter K. Robinson, and Christine Z. Beyzaei. March 2017.
- PEER 2017/01** *2016 PEER Annual Report.* Khalid M. Mosalam, Amarnath Kasalanati, and Grace Kang. March 2017.
- PEER 2016/10** *Performance-Based Robust Nonlinear Seismic Analysis with Application to Reinforced Concrete Bridge Systems.* Xiao Ling and Khalid M. Mosalam. December 2016.
- PEER 2017/09** *Detailing Requirements for Column Plastic Hinges subjected to Combined Flexural, Axial, and Torsional Seismic Loading.* Gabriel Hurtado and Jack P. Moehle. December 2016.
- PEER 2016/08** *Resilience of Critical Structures, Infrastructure, and Communities.* Gian Paolo Cimellaro, Ali Zamani-Noori, Omar Kamouh, Vesna Terzic, and Stephen A. Mahin. December 2016.
- PEER 2016/07** *Hybrid Simulation Theory for a Classical Nonlinear Dynamical System.* Paul L. Drazin and Sanjay Govindjee. September 2016.
- PEER 2016/06** *California Earthquake Early Warning System Benefit Study.* Laurie A. Johnson, Sharyl Rabinovici, Grace S. Kang, and Stephen A. Mahin. July 2006.
- PEER 2016/05** *Ground-Motion Prediction Equations for Arias Intensity Consistent with the NGA-West2 Ground-Motion Models.* Charlotte Abrahamson, Hao-Jun Michael Shi, and Brian Yang. July 2016.
- PEER 2016/04** *The Mw 6.0 South Napa Earthquake of August 24, 2014: A Wake-Up Call for Renewed Investment in Seismic Resilience Across California.* Prepared for the California Seismic Safety Commission, Laurie A. Johnson and Stephen A. Mahin. May 2016.
- PEER 2016/03** *Simulation Confidence in Tsunami-Driven Overland Flow.* Patrick Lynett. May 2016.
- PEER 2016/02** *Semi-Automated Procedure for Windowing time Series and Computing Fourier Amplitude Spectra for the NGA-West2 Database.* Tadahiro Kishida, Olga-Joan Ktenidou, Robert B. Darragh, and Walter J. Silva. May 2016.

- PEER 2016/01** *A Methodology for the Estimation of Kappa (κ) from Large Datasets: Example Application to Rock Sites in the NGA-East Database and Implications on Design Motions.* Olga-Joan Ktenidou, Norman A. Abrahamson, Robert B. Darragh, and Walter J. Silva. April 2016.
- PEER 2015/13** *Self-Centering Precast Concrete Dual-Steel-Shell Columns for Accelerated Bridge Construction: Seismic Performance, Analysis, and Design.* Gabriele Guerrini, José I. Restrepo, Athanassios Vervelidis, and Milena Massari. December 2015.
- PEER 2015/12** *Shear-Flexure Interaction Modeling for Reinforced Concrete Structural Walls and Columns under Reversed Cyclic Loading.* Kristijan Kolozvari, Kutay Orakcal, and John Wallace. December 2015.
- PEER 2015/11** *Selection and Scaling of Ground Motions for Nonlinear Response History Analysis of Buildings in Performance-Based Earthquake Engineering.* N. Simon Kwong and Anil K. Chopra. December 2015.
- PEER 2015/10** *Structural Behavior of Column-Bent Cap Beam-Box Girder Systems in Reinforced Concrete Bridges Subjected to Gravity and Seismic Loads. Part II: Hybrid Simulation and Post-Test Analysis.* Mohamed A. Moustafa and Khalid M. Mosalam. November 2015.
- PEER 2015/09** *Structural Behavior of Column-Bent Cap Beam-Box Girder Systems in Reinforced Concrete Bridges Subjected to Gravity and Seismic Loads. Part I: Pre-Test Analysis and Quasi-Static Experiments.* Mohamed A. Moustafa and Khalid M. Mosalam. September 2015.
- PEER 2015/08** *NGA-East: Adjustments to Median Ground-Motion Models for Center and Eastern North America.* August 2015.
- PEER 2015/07** *NGA-East: Ground-Motion Standard-Deviation Models for Central and Eastern North America.* Linda Al Atik. June 2015.
- PEER 2015/06** *Adjusting Ground-Motion Intensity Measures to a Reference Site for which $V_{S30} = 3000$ m/sec.* David M. Boore. May 2015.
- PEER 2015/05** *Hybrid Simulation of Seismic Isolation Systems Applied to an APR-1400 Nuclear Power Plant.* Andreas H. Schellenberg, Alireza Sarebanha, Matthew J. Schoettler, Gilberto Mosqueda, Gianmario Benzoni, and Stephen A. Mahin. April 2015.
- PEER 2015/04** *NGA-East: Median Ground-Motion Models for the Central and Eastern North America Region.* April 2015.
- PEER 2015/03** *Single Series Solution for the Rectangular Fiber-Reinforced Elastomeric Isolator Compression Modulus.* James M. Kelly and Niel C. Van Engelen. March 2015.
- PEER 2015/02** *A Full-Scale, Single-Column Bridge Bent Tested by Shake-Table Excitation.* Matthew J. Schoettler, José I. Restrepo, Gabriele Guerrini, David E. Duck, and Francesco Carrea. March 2015.
- PEER 2015/01** *Concrete Column Blind Prediction Contest 2010: Outcomes and Observations.* Vesna Terzic, Matthew J. Schoettler, José I. Restrepo, and Stephen A. Mahin. March 2015.
- PEER 2014/20** *Stochastic Modeling and Simulation of Near-Fault Ground Motions for Performance-Based Earthquake Engineering.* Mayssa Dabaghi and Armen Der Kiureghian. December 2014.
- PEER 2014/19** *Seismic Response of a Hybrid Fiber-Reinforced Concrete Bridge Column Detailed for Accelerated Bridge Construction.* Wilson Nguyen, William Trono, Marios Panagiotou, and Claudia P. Ostertag. December 2014.
- PEER 2014/18** *Three-Dimensional Beam-Truss Model for Reinforced Concrete Walls and Slabs Subjected to Cyclic Static or Dynamic Loading.* Yuan Lu, Marios Panagiotou, and Ioannis Koutromanos. December 2014.
- PEER 2014/17** *PEER NGA-East Database.* Christine A. Goulet, Tadahiro Kishida, Timothy D. Ancheta, Chris H. Cramer, Robert B. Darragh, Walter J. Silva, Youssef M.A. Hashash, Joseph Harmon, Jonathan P. Stewart, Katie E. Wooddell, and Robert R. Youngs. October 2014.
- PEER 2014/16** *Guidelines for Performing Hazard-Consistent One-Dimensional Ground Response Analysis for Ground Motion Prediction.* Jonathan P. Stewart, Kioumars Afshari, and Youssef M.A. Hashash. October 2014.
- PEER 2014/15** *NGA-East Regionalization Report: Comparison of Four Crustal Regions within Central and Eastern North America using Waveform Modeling and 5%-Damped Pseudo-Spectral Acceleration Response.* Jennifer Dreiling, Marius P. Isken, Walter D. Mooney, Martin C. Chapman, and Richard W. Godbee. October 2014.
- PEER 2014/14** *Scaling Relations between Seismic Moment and Rupture Area of Earthquakes in Stable Continental Regions.* Paul Somerville. August 2014.
- PEER 2014/13** *PEER Preliminary Notes and Observations on the August 24, 2014, South Napa Earthquake.* Grace S. Kang and Stephen A. Mahin, Editors. September 2014.
- PEER 2014/12** *Reference-Rock Site Conditions for Central and Eastern North America: Part II – Attenuation (Kappa) Definition.* Kenneth W. Campbell, Youssef M.A. Hashash, Byungmin Kim, Albert R. Kottke, Ellen M. Rathje, Walter J. Silva, and Jonathan P. Stewart. August 2014.

- PEER 2014/11** *Reference-Rock Site Conditions for Central and Eastern North America: Part I - Velocity Definition.* Youssef M.A. Hashash, Albert R. Kottke, Jonathan P. Stewart, Kenneth W. Campbell, Byungmin Kim, Ellen M. Rathje, Walter J. Silva, Sissy Nikolaou, and Cheryl Moss. August 2014.
- PEER 2014/10** *Evaluation of Collapse and Non-Collapse of Parallel Bridges Affected by Liquefaction and Lateral Spreading.* Benjamin Turner, Scott J. Brandenburg, and Jonathan P. Stewart. August 2014.
- PEER 2014/09** *PEER Arizona Strong-Motion Database and GMPEs Evaluation.* Tadahiro Kishida, Robert E. Kayen, Olga-Joan Ktenidou, Walter J. Silva, Robert B. Darragh, and Jennie Watson-Lamprey. June 2014.
- PEER 2014/08** *Unbonded Pretensioned Bridge Columns with Rocking Detail.* Jeffrey A. Schaefer, Bryan Kennedy, Marc O. Eberhard, and John F. Stanton. June 2014.
- PEER 2014/07** *Northridge 20 Symposium Summary Report: Impacts, Outcomes, and Next Steps.* May 2014.
- PEER 2014/06** *Report of the Tenth Planning Meeting of NEES/E-Defense Collaborative Research on Earthquake Engineering.* December 2013.
- PEER 2014/05** *Seismic Velocity Site Characterization of Thirty-One Chilean Seismometer Stations by Spectral Analysis of Surface Wave Dispersion.* Robert Kayen, Brad D. Carkin, Skye Corbet, Camilo Pinilla, Allan Ng, Edward Gorbis, and Christine Truong. April 2014.
- PEER 2014/04** *Effect of Vertical Acceleration on Shear Strength of Reinforced Concrete Columns.* Hyerin Lee and Khalid M. Mosalam. April 2014.
- PEER 2014/03** *Retest of Thirty-Year-Old Neoprene Isolation Bearings.* James M. Kelly and Niel C. Van Engelen. March 2014.
- PEER 2014/02** *Theoretical Development of Hybrid Simulation Applied to Plate Structures.* Ahmed A. Bakhaty, Khalid M. Mosalam, and Sanjay Govindjee. January 2014.
- PEER 2014/01** *Performance-Based Seismic Assessment of Skewed Bridges.* Peyman Kaviani, Farzin Zareian, and Ertugrul Taciroglu. January 2014.
- PEER 2013/26** *Urban Earthquake Engineering.* Proceedings of the U.S.-Iran Seismic Workshop. December 2013.
- PEER 2013/25** *Earthquake Engineering for Resilient Communities: 2013 PEER Internship Program Research Report Collection.* Heidi Tremayne (Editor), Stephen A. Mahin (Editor), Jorge Archbold Monterossa, Matt Brosman, Shelly Dean, Katherine deLaveaga, Curtis Fong, Donovan Holder, Rakeeb Khan, Elizabeth Jachens, David Lam, Daniela Martinez Lopez, Mara Minner, Geffen Oren, Julia Pavicic, Melissa Quinonez, Lorena Rodriguez, Sean Salazar, Kelli Slaven, Vivian Steyert, Jenny Taing, and Salvador Tena. December 2013.
- PEER 2013/24** *NGA-West2 Ground Motion Prediction Equations for Vertical Ground Motions.* September 2013.
- PEER 2013/23** *Coordinated Planning and Preparedness for Fire Following Major Earthquakes.* Charles Scawthorn. November 2013.
- PEER 2013/22** *GEM-PEER Task 3 Project: Selection of a Global Set of Ground Motion Prediction Equations.* Jonathan P. Stewart, John Douglas, Mohammad B. Javanbarg, Carola Di Alessandro, Yousef Bozorgnia, Norman A. Abrahamson, David M. Boore, Kenneth W. Campbell, Elise Delavaud, Mustafa Erdik, and Peter J. Stafford. December 2013.
- PEER 2013/21** *Seismic Design and Performance of Bridges with Columns on Rocking Foundations.* Grigorios Antonellis and Marios Panagiotou. September 2013.
- PEER 2013/20** *Experimental and Analytical Studies on the Seismic Behavior of Conventional and Hybrid Braced Frames.* Jiun-Wei Lai and Stephen A. Mahin. September 2013.
- PEER 2013/19** *Toward Resilient Communities: A Performance-Based Engineering Framework for Design and Evaluation of the Built Environment.* Michael William Mieler, Bozidar Stojadinovic, Robert J. Budnitz, Stephen A. Mahin, and Mary C. Comerio. September 2013.
- PEER 2013/18** *Identification of Site Parameters that Improve Predictions of Site Amplification.* Ellen M. Rathje and Sara Navidi. July 2013.
- PEER 2013/17** *Response Spectrum Analysis of Concrete Gravity Dams Including Dam-Water-Foundation Interaction.* Arnkjell Løkke and Anil K. Chopra. July 2013.
- PEER 2013/16** *Effect of Hoop Reinforcement Spacing on the Cyclic Response of Large Reinforced Concrete Special Moment Frame Beams.* Marios Panagiotou, Tea Visnjic, Grigorios Antonellis, Panagiotis Galanis, and Jack P. Moehle. June 2013.
- PEER 2013/15** *A Probabilistic Framework to Include the Effects of Near-Fault Directivity in Seismic Hazard Assessment.* Shrey Kumar Shahi, Jack W. Baker. October 2013.

- PEER 2013/14** *Hanging-Wall Scaling using Finite-Fault Simulations.* Jennifer L. Donahue and Norman A. Abrahamson. September 2013.
- PEER 2013/13** *Semi-Empirical Nonlinear Site Amplification and its Application in NEHRP Site Factors.* Jonathan P. Stewart and Emel Seyhan. November 2013.
- PEER 2013/12** *Nonlinear Horizontal Site Response for the NGA-West2 Project.* Ronnie Kamai, Norman A. Abramson, Walter J. Silva. May 2013.
- PEER 2013/11** *Epistemic Uncertainty for NGA-West2 Models.* Linda Al Atik and Robert R. Youngs. May 2013.
- PEER 2013/10** *NGA-West 2 Models for Ground-Motion Directionality.* Shrey K. Shahi and Jack W. Baker. May 2013.
- PEER 2013/09** *Final Report of the NGA-West2 Directivity Working Group.* Paul Spudich, Jeffrey R. Bayless, Jack W. Baker, Brian S.J. Chiou, Badie Rowshandel, Shrey Shahi, and Paul Somerville. May 2013.
- PEER 2013/08** *NGA-West2 Model for Estimating Average Horizontal Values of Pseudo-Absolute Spectral Accelerations Generated by Crustal Earthquakes.* I. M. Idriss. May 2013.
- PEER 2013/07** *Update of the Chiou and Youngs NGA Ground Motion Model for Average Horizontal Component of Peak Ground Motion and Response Spectra.* Brian Chiou and Robert Youngs. May 2013.
- PEER 2013/06** *NGA-West2 Campbell-Bozorgnia Ground Motion Model for the Horizontal Components of PGA, PGV, and 5%-Damped Elastic Pseudo-Acceleration Response Spectra for Periods Ranging from 0.01 to 10 sec.* Kenneth W. Campbell and Yousef Bozorgnia. May 2013.
- PEER 2013/05** *NGA-West 2 Equations for Predicting Response Spectral Accelerations for Shallow Crustal Earthquakes.* David M. Boore, Jonathan P. Stewart, Emel Seyhan, and Gail M. Atkinson. May 2013.
- PEER 2013/04** *Update of the AS08 Ground-Motion Prediction Equations Based on the NGA-West2 Data Set.* Norman Abrahamson, Walter Silva, and Ronnie Kamai. May 2013.
- PEER 2013/03** *PEER NGA-West2 Database.* Timothy D. Ancheta, Robert B. Darragh, Jonathan P. Stewart, Emel Seyhan, Walter J. Silva, Brian S.J. Chiou, Katie E. Wooddell, Robert W. Graves, Albert R. Kottke, David M. Boore, Tadahiro Kishida, and Jennifer L. Donahue. May 2013.
- PEER 2013/02** *Hybrid Simulation of the Seismic Response of Squat Reinforced Concrete Shear Walls.* Catherine A. Whyte and Bozidar Stojadinovic. May 2013.
- PEER 2013/01** *Housing Recovery in Chile: A Qualitative Mid-program Review.* Mary C. Comerio. February 2013.
- PEER 2012/08** *Guidelines for Estimation of Shear Wave Velocity.* Bernard R. Wair, Jason T. DeJong, and Thomas Shantz. December 2012.
- PEER 2012/07** *Earthquake Engineering for Resilient Communities: 2012 PEER Internship Program Research Report Collection.* Heidi Tremayne (Editor), Stephen A. Mahin (Editor), Collin Anderson, Dustin Cook, Michael Erceg, Carlos Esparza, Jose Jimenez, Dorian Krausz, Andrew Lo, Stephanie Lopez, Nicole McCurdy, Paul Shipman, Alexander Strum, Eduardo Vega. December 2012.
- PEER 2012/06** *Fragilities for Precarious Rocks at Yucca Mountain.* Matthew D. Purvance, Rasool Anooshehpour, and James N. Brune. December 2012.
- PEER 2012/05** *Development of Simplified Analysis Procedure for Piles in Laterally Spreading Layered Soils.* Christopher R. McGann, Pedro Arduino, and Peter Mackenzie-Helnwein. December 2012.
- PEER 2012/04** *Unbonded Pre-Tensioned Columns for Bridges in Seismic Regions.* Phillip M. Davis, Todd M. Janes, Marc O. Eberhard, and John F. Stanton. December 2012.
- PEER 2012/03** *Experimental and Analytical Studies on Reinforced Concrete Buildings with Seismically Vulnerable Beam-Column Joints.* Sangjoon Park and Khalid M. Mosalam. October 2012.
- PEER 2012/02** *Seismic Performance of Reinforced Concrete Bridges Allowed to Uplift during Multi-Directional Excitation.* Andres Oscar Espinoza and Stephen A. Mahin. July 2012.
- PEER 2012/01** *Spectral Damping Scaling Factors for Shallow Crustal Earthquakes in Active Tectonic Regions.* Sanaz Rezaeian, Yousef Bozorgnia, I. M. Idriss, Kenneth Campbell, Norman Abrahamson, and Walter Silva. July 2012.
- PEER 2011/10** *Earthquake Engineering for Resilient Communities: 2011 PEER Internship Program Research Report Collection.* Heidi Faison and Stephen A. Mahin, Editors. December 2011.
- PEER 2011/09** *Calibration of Semi-Stochastic Procedure for Simulating High-Frequency Ground Motions.* Jonathan P. Stewart, Emel Seyhan, and Robert W. Graves. December 2011.
- PEER 2011/08** *Water Supply in regard to Fire Following Earthquake.* Charles Scawthorn. November 2011.

- PEER 2011/07** *Seismic Risk Management in Urban Areas*. Proceedings of a U.S.-Iran-Turkey Seismic Workshop. September 2011.
- PEER 2011/06** *The Use of Base Isolation Systems to Achieve Complex Seismic Performance Objectives*. Troy A. Morgan and Stephen A. Mahin. July 2011.
- PEER 2011/05** *Case Studies of the Seismic Performance of Tall Buildings Designed by Alternative Means*. Task 12 Report for the Tall Buildings Initiative. Jack Moehle, Yousef Bozorgnia, Nirmal Jayaram, Pierson Jones, Mohsen Rahnama, Niles Shome, Zeynep Tuna, John Wallace, Tony Yang, and Farzin Zareian. July 2011.
- PEER 2011/04** *Recommended Design Practice for Pile Foundations in Laterally Spreading Ground*. Scott A. Ashford, Ross W. Boulanger, and Scott J. Brandenberg. June 2011.
- PEER 2011/03** *New Ground Motion Selection Procedures and Selected Motions for the PEER Transportation Research Program*. Jack W. Baker, Ting Lin, Shrey K. Shahi, and Nirmal Jayaram. March 2011.
- PEER 2011/02** *A Bayesian Network Methodology for Infrastructure Seismic Risk Assessment and Decision Support*. Michelle T. Bensi, Armen Der Kiureghian, and Daniel Straub. March 2011.
- PEER 2011/01** *Demand Fragility Surfaces for Bridges in Liquefied and Laterally Spreading Ground*. Scott J. Brandenberg, Jian Zhang, Pirooz Kashighandi, Yili Huo, and Minxing Zhao. March 2011.
- PEER 2010/05** *Guidelines for Performance-Based Seismic Design of Tall Buildings*. Developed by the Tall Buildings Initiative. November 2010.
- PEER 2010/04** *Application Guide for the Design of Flexible and Rigid Bus Connections between Substation Equipment Subjected to Earthquakes*. Jean-Bernard Dastous and Armen Der Kiureghian. September 2010.
- PEER 2010/03** *Shear Wave Velocity as a Statistical Function of Standard Penetration Test Resistance and Vertical Effective Stress at Caltrans Bridge Sites*. Scott J. Brandenberg, Naresh Bellana, and Thomas Shantz. June 2010.
- PEER 2010/02** *Stochastic Modeling and Simulation of Ground Motions for Performance-Based Earthquake Engineering*. Sanaz Rezaeian and Armen Der Kiureghian. June 2010.
- PEER 2010/01** *Structural Response and Cost Characterization of Bridge Construction Using Seismic Performance Enhancement Strategies*. Ady Aviram, Božidar Stojadinović, Gustavo J. Parra-Montesinos, and Kevin R. Mackie. March 2010.
- PEER 2009/03** *The Integration of Experimental and Simulation Data in the Study of Reinforced Concrete Bridge Systems Including Soil-Foundation-Structure Interaction*. Matthew Dryden and Gregory L. Fenves. November 2009.
- PEER 2009/02** *Improving Earthquake Mitigation through Innovations and Applications in Seismic Science, Engineering, Communication, and Response*. Proceedings of a U.S.-Iran Seismic Workshop. October 2009.
- PEER 2009/01** *Evaluation of Ground Motion Selection and Modification Methods: Predicting Median Interstory Drift Response of Buildings*. Curt B. Haselton, Editor. June 2009.
- PEER 2008/10** *Technical Manual for Strata*. Albert R. Kottke and Ellen M. Rathje. February 2009.
- PEER 2008/09** *NGA Model for Average Horizontal Component of Peak Ground Motion and Response Spectra*. Brian S.-J. Chiou and Robert R. Youngs. November 2008.
- PEER 2008/08** *Toward Earthquake-Resistant Design of Concentrically Braced Steel Structures*. Patxi Uriz and Stephen A. Mahin. November 2008.
- PEER 2008/07** *Using OpenSees for Performance-Based Evaluation of Bridges on Liquefiable Soils*. Stephen L. Kramer, Pedro Arduino, and HyungSuk Shin. November 2008.
- PEER 2008/06** *Shaking Table Tests and Numerical Investigation of Self-Centering Reinforced Concrete Bridge Columns*. Hyung IL Jeong, Junichi Sakai, and Stephen A. Mahin. September 2008.
- PEER 2008/05** *Performance-Based Earthquake Engineering Design Evaluation Procedure for Bridge Foundations Undergoing Liquefaction-Induced Lateral Ground Displacement*. Christian A. Ledezma and Jonathan D. Bray. August 2008.
- PEER 2008/04** *Benchmarking of Nonlinear Geotechnical Ground Response Analysis Procedures*. Jonathan P. Stewart, Annie On-Lei Kwok, Youssef M. A. Hashash, Neven Matasovic, Robert Pyke, Zhiliang Wang, and Zhaohui Yang. August 2008.
- PEER 2008/03** *Guidelines for Nonlinear Analysis of Bridge Structures in California*. Ady Aviram, Kevin R. Mackie, and Božidar Stojadinović. August 2008.
- PEER 2008/02** *Treatment of Uncertainties in Seismic-Risk Analysis of Transportation Systems*. Evangelos Stergiou and Anne S. Kiremidjian. July 2008.

- PEER 2008/01** *Seismic Performance Objectives for Tall Buildings.* William T. Holmes, Charles Kircher, William Petak, and Nabih Youssef. August 2008.
- PEER 2007/12** *An Assessment to Benchmark the Seismic Performance of a Code-Conforming Reinforced Concrete Moment-Frame Building.* Curt Haselton, Christine A. Goulet, Judith Mitrani-Reiser, James L. Beck, Gregory G. Deierlein, Keith A. Porter, Jonathan P. Stewart, and Ertugrul Taciroglu. August 2008.
- PEER 2007/11** *Bar Buckling in Reinforced Concrete Bridge Columns.* Wayne A. Brown, Dawn E. Lehman, and John F. Stanton. February 2008.
- PEER 2007/10** *Computational Modeling of Progressive Collapse in Reinforced Concrete Frame Structures.* Mohamed M. Talaat and Khalid M. Mosalam. May 2008.
- PEER 2007/09** *Integrated Probabilistic Performance-Based Evaluation of Benchmark Reinforced Concrete Bridges.* Kevin R. Mackie, John-Michael Wong, and Božidar Stojadinović. January 2008.
- PEER 2007/08** *Assessing Seismic Collapse Safety of Modern Reinforced Concrete Moment-Frame Buildings.* Curt B. Haselton and Gregory G. Deierlein. February 2008.
- PEER 2007/07** *Performance Modeling Strategies for Modern Reinforced Concrete Bridge Columns.* Michael P. Berry and Marc O. Eberhard. April 2008.
- PEER 2007/06** *Development of Improved Procedures for Seismic Design of Buried and Partially Buried Structures.* Linda Al Atik and Nicholas Sitar. June 2007.
- PEER 2007/05** *Uncertainty and Correlation in Seismic Risk Assessment of Transportation Systems.* Renee G. Lee and Anne S. Kiremidjian. July 2007.
- PEER 2007/04** *Numerical Models for Analysis and Performance-Based Design of Shallow Foundations Subjected to Seismic Loading.* Sivapalan Gajan, Tara C. Hutchinson, Bruce L. Kutter, Prishati Raychowdhury, José A. Ugalde, and Jonathan P. Stewart. May 2008.
- PEER 2007/03** *Beam-Column Element Model Calibrated for Predicting Flexural Response Leading to Global Collapse of RC Frame Buildings.* Curt B. Haselton, Abbie B. Liel, Sarah Taylor Lange, and Gregory G. Deierlein. May 2008.
- PEER 2007/02** *Campbell-Bozorgnia NGA Ground Motion Relations for the Geometric Mean Horizontal Component of Peak and Spectral Ground Motion Parameters.* Kenneth W. Campbell and Yousef Bozorgnia. May 2007.
- PEER 2007/01** *Boore-Atkinson NGA Ground Motion Relations for the Geometric Mean Horizontal Component of Peak and Spectral Ground Motion Parameters.* David M. Boore and Gail M. Atkinson. May 2007.
- PEER 2006/12** *Societal Implications of Performance-Based Earthquake Engineering.* Peter J. May. May 2007.
- PEER 2006/11** *Probabilistic Seismic Demand Analysis Using Advanced Ground Motion Intensity Measures, Attenuation Relationships, and Near-Fault Effects.* Polsak Tothong and C. Allin Cornell. March 2007.
- PEER 2006/10** *Application of the PEER PBEE Methodology to the I-880 Viaduct.* Sashi Kunnath. February 2007.
- PEER 2006/09** *Quantifying Economic Losses from Travel Forgone Following a Large Metropolitan Earthquake.* James Moore, Sungbin Cho, Yue Yue Fan, and Stuart Werner. November 2006.
- PEER 2006/08** *Vector-Valued Ground Motion Intensity Measures for Probabilistic Seismic Demand Analysis.* Jack W. Baker and C. Allin Cornell. October 2006.
- PEER 2006/07** *Analytical Modeling of Reinforced Concrete Walls for Predicting Flexural and Coupled-Shear-Flexural Responses.* Kutay Orakcal, Leonardo M. Massone, and John W. Wallace. October 2006.
- PEER 2006/06** *Nonlinear Analysis of a Soil-Drilled Pier System under Static and Dynamic Axial Loading.* Gang Wang and Nicholas Sitar. November 2006.
- PEER 2006/05** *Advanced Seismic Assessment Guidelines.* Paolo Bazzurro, C. Allin Cornell, Charles Menun, Maziar Motahari, and Nicolas Luco. September 2006.
- PEER 2006/04** *Probabilistic Seismic Evaluation of Reinforced Concrete Structural Components and Systems.* Tae Hyung Lee and Khalid M. Mosalam. August 2006.
- PEER 2006/03** *Performance of Lifelines Subjected to Lateral Spreading.* Scott A. Ashford and Teerawut Juirnarongrit. July 2006.
- PEER 2006/02** *Pacific Earthquake Engineering Research Center Highway Demonstration Project.* Anne Kiremidjian, James Moore, Yue Yue Fan, Nesrin Basoz, Ozgur Yazali, and Meredith Williams. April 2006.
- PEER 2006/01** *Bracing Berkeley. A Guide to Seismic Safety on the UC Berkeley Campus.* Mary C. Comerio, Stephen Tobriner, and Ariane Fehrenkamp. January 2006.

- PEER 2005/17** *Earthquake Simulation Tests on Reducing Residual Displacements of Reinforced Concrete Bridges.* Junichi Sakai, Stephen A Mahin, and Andres Espinoza. December 2005.
- PEER 2005/16** *Seismic Response and Reliability of Electrical Substation Equipment and Systems.* Junho Song, Armen Der Kiureghian, and Jerome L. Sackman. April 2006.
- PEER 2005/15** *CPT-Based Probabilistic Assessment of Seismic Soil Liquefaction Initiation.* R. E. S. Moss, R. B. Seed, R. E. Kayen, J. P. Stewart, and A. Der Kiureghian. April 2006.
- PEER 2005/14** *Workshop on Modeling of Nonlinear Cyclic Load-Deformation Behavior of Shallow Foundations.* Bruce L. Kutter, Geoffrey Martin, Tara Hutchinson, Chad Harden, Sivapalan Gajan, and Justin Phalen. March 2006.
- PEER 2005/13** *Stochastic Characterization and Decision Bases under Time-Dependent Aftershock Risk in Performance-Based Earthquake Engineering.* Gee Liek Yeo and C. Allin Cornell. July 2005.
- PEER 2005/12** *PEER Testbed Study on a Laboratory Building: Exercising Seismic Performance Assessment.* Mary C. Comerio, Editor. November 2005.
- PEER 2005/11** *Van Nuys Hotel Building Testbed Report: Exercising Seismic Performance Assessment.* Helmut Krawinkler, Editor. October 2005.
- PEER 2005/10** *First NEES/E-Defense Workshop on Collapse Simulation of Reinforced Concrete Building Structures.* September 2005.
- PEER 2005/09** *Test Applications of Advanced Seismic Assessment Guidelines.* Joe Maffei, Karl Telleen, Danya Mohr, William Holmes, and Yuki Nakayama. August 2006.
- PEER 2005/08** *Damage Accumulation in Lightly Confined Reinforced Concrete Bridge Columns.* R. Tyler Ranf, Jared M. Nelson, Zach Price, Marc O. Eberhard, and John F. Stanton. April 2006.
- PEER 2005/07** *Experimental and Analytical Studies on the Seismic Response of Freestanding and Anchored Laboratory Equipment.* Dimitrios Konstantinidis and Nicos Makris. January 2005.
- PEER 2005/06** *Global Collapse of Frame Structures under Seismic Excitations.* Luis F. Ibarra and Helmut Krawinkler. September 2005.
- PEER 2005/05** *Performance Characterization of Bench- and Shelf-Mounted Equipment.* Samit Ray Chaudhuri and Tara C. Hutchinson. May 2006.
- PEER 2005/04** *Numerical Modeling of the Nonlinear Cyclic Response of Shallow Foundations.* Chad Harden, Tara Hutchinson, Geoffrey R. Martin, and Bruce L. Kutter. August 2005.
- PEER 2005/03** *A Taxonomy of Building Components for Performance-Based Earthquake Engineering.* Keith A. Porter. September 2005.
- PEER 2005/02** *Fragility Basis for California Highway Overpass Bridge Seismic Decision Making.* Kevin R. Mackie and Božidar Stojadinović. June 2005.
- PEER 2005/01** *Empirical Characterization of Site Conditions on Strong Ground Motion.* Jonathan P. Stewart, Yoojoong Choi, and Robert W. Graves. June 2005.
- PEER 2004/09** *Electrical Substation Equipment Interaction: Experimental Rigid Conductor Studies.* Christopher Stearns and André Filiatrault. February 2005.
- PEER 2004/08** *Seismic Qualification and Fragility Testing of Line Break 550-kV Disconnect Switches.* Shakhzod M. Takhirov, Gregory L. Fenves, and Eric Fujisaki. January 2005.
- PEER 2004/07** *Ground Motions for Earthquake Simulator Qualification of Electrical Substation Equipment.* Shakhzod M. Takhirov, Gregory L. Fenves, Eric Fujisaki, and Don Clyde. January 2005.
- PEER 2004/06** *Performance-Based Regulation and Regulatory Regimes.* Peter J. May and Chris Koski. September 2004.
- PEER 2004/05** *Performance-Based Seismic Design Concepts and Implementation: Proceedings of an International Workshop.* Peter Fajfar and Helmut Krawinkler, Editors. September 2004.
- PEER 2004/04** *Seismic Performance of an Instrumented Tilt-up Wall Building.* James C. Anderson and Vitelmo V. Bertero. July 2004.
- PEER 2004/03** *Evaluation and Application of Concrete Tilt-up Assessment Methodologies.* Timothy Graf and James O. Malley. October 2004.
- PEER 2004/02** *Analytical Investigations of New Methods for Reducing Residual Displacements of Reinforced Concrete Bridge Columns.* Junichi Sakai and Stephen A. Mahin. August 2004.

- PEER 2004/01** *Seismic Performance of Masonry Buildings and Design Implications.* Kerri Anne Taeko Tokoro, James C. Anderson, and Vitelmo V. Bertero. February 2004.
- PEER 2003/18** *Performance Models for Flexural Damage in Reinforced Concrete Columns.* Michael Berry and Marc Eberhard. August 2003.
- PEER 2003/17** *Predicting Earthquake Damage in Older Reinforced Concrete Beam-Column Joints.* Catherine Pagni and Laura Lowes. October 2004.
- PEER 2003/16** *Seismic Demands for Performance-Based Design of Bridges.* Kevin Mackie and Božidar Stojadinović. August 2003.
- PEER 2003/15** *Seismic Demands for Nondeteriorating Frame Structures and Their Dependence on Ground Motions.* Ricardo Antonio Medina and Helmut Krawinkler. May 2004.
- PEER 2003/14** *Finite Element Reliability and Sensitivity Methods for Performance-Based Earthquake Engineering.* Terje Haukaas and Armen Der Kiureghian. April 2004.
- PEER 2003/13** *Effects of Connection Hysteretic Degradation on the Seismic Behavior of Steel Moment-Resisting Frames.* Janise E. Rodgers and Stephen A. Mahin. March 2004.
- PEER 2003/12** *Implementation Manual for the Seismic Protection of Laboratory Contents: Format and Case Studies.* William T. Holmes and Mary C. Comerio. October 2003.
- PEER 2003/11** *Fifth U.S.-Japan Workshop on Performance-Based Earthquake Engineering Methodology for Reinforced Concrete Building Structures.* February 2004.
- PEER 2003/10** *A Beam-Column Joint Model for Simulating the Earthquake Response of Reinforced Concrete Frames.* Laura N. Lowes, Nilanjan Mitra, and Arash Altoontash. February 2004.
- PEER 2003/09** *Sequencing Repairs after an Earthquake: An Economic Approach.* Marco Casari and Simon J. Wilkie. April 2004.
- PEER 2003/08** *A Technical Framework for Probability-Based Demand and Capacity Factor Design (DCFD) Seismic Formats.* Fatemeh Jalayer and C. Allin Cornell. November 2003.
- PEER 2003/07** *Uncertainty Specification and Propagation for Loss Estimation Using FOSM Methods.* Jack W. Baker and C. Allin Cornell. September 2003.
- PEER 2003/06** *Performance of Circular Reinforced Concrete Bridge Columns under Bidirectional Earthquake Loading.* Mahmoud M. Hachem, Stephen A. Mahin, and Jack P. Moehle. February 2003.
- PEER 2003/05** *Response Assessment for Building-Specific Loss Estimation.* Eduardo Miranda and Shahram Taghavi. September 2003.
- PEER 2003/04** *Experimental Assessment of Columns with Short Lap Splices Subjected to Cyclic Loads.* Murat Melek, John W. Wallace, and Joel Conte. April 2003.
- PEER 2003/03** *Probabilistic Response Assessment for Building-Specific Loss Estimation.* Eduardo Miranda and Hesameddin Aslani. September 2003.
- PEER 2003/02** *Software Framework for Collaborative Development of Nonlinear Dynamic Analysis Program.* Jun Peng and Kincho H. Law. September 2003.
- PEER 2003/01** *Shake Table Tests and Analytical Studies on the Gravity Load Collapse of Reinforced Concrete Frames.* Kenneth John Elwood and Jack P. Moehle. November 2003.
- PEER 2002/24** *Performance of Beam to Column Bridge Joints Subjected to a Large Velocity Pulse.* Natalie Gibson, André Filiatrault, and Scott A. Ashford. April 2002.
- PEER 2002/23** *Effects of Large Velocity Pulses on Reinforced Concrete Bridge Columns.* Greg L. Orozco and Scott A. Ashford. April 2002.
- PEER 2002/22** *Characterization of Large Velocity Pulses for Laboratory Testing.* Kenneth E. Cox and Scott A. Ashford. April 2002.
- PEER 2002/21** *Fourth U.S.-Japan Workshop on Performance-Based Earthquake Engineering Methodology for Reinforced Concrete Building Structures.* December 2002.
- PEER 2002/20** *Barriers to Adoption and Implementation of PBEE Innovations.* Peter J. May. August 2002.
- PEER 2002/19** *Economic-Engineered Integrated Models for Earthquakes: Socioeconomic Impacts.* Peter Gordon, James E. Moore II, and Harry W. Richardson. July 2002.

- PEER 2002/18** *Assessment of Reinforced Concrete Building Exterior Joints with Substandard Details.* Chris P. Pantelides, Jon Hansen, Justin Nadauld, and Lawrence D. Reaveley. May 2002.
- PEER 2002/17** *Structural Characterization and Seismic Response Analysis of a Highway Overcrossing Equipped with Elastomeric Bearings and Fluid Dampers: A Case Study.* Nicos Makris and Jian Zhang. November 2002.
- PEER 2002/16** *Estimation of Uncertainty in Geotechnical Properties for Performance-Based Earthquake Engineering.* Allen L. Jones, Steven L. Kramer, and Pedro Arduino. December 2002.
- PEER 2002/15** *Seismic Behavior of Bridge Columns Subjected to Various Loading Patterns.* Asadollah Esmaeily-Gh. and Yan Xiao. December 2002.
- PEER 2002/14** *Inelastic Seismic Response of Extended Pile Shaft Supported Bridge Structures.* T.C. Hutchinson, R.W. Boulanger, Y.H. Chai, and I.M. Idriss. December 2002.
- PEER 2002/13** *Probabilistic Models and Fragility Estimates for Bridge Components and Systems.* Paolo Gardoni, Armen Der Kiureghian, and Khalid M. Mosalam. June 2002.
- PEER 2002/12** *Effects of Fault Dip and Slip Rake on Near-Source Ground Motions: Why Chi-Chi Was a Relatively Mild M7.6 Earthquake.* Brad T. Aagaard, John F. Hall, and Thomas H. Heaton. December 2002.
- PEER 2002/11** *Analytical and Experimental Study of Fiber-Reinforced Strip Isolators.* James M. Kelly and Shakhzod M. Takhirov. September 2002.
- PEER 2002/10** *Centrifuge Modeling of Settlement and Lateral Spreading with Comparisons to Numerical Analyses.* Sivapalan Gajan and Bruce L. Kutter. January 2003.
- PEER 2002/09** *Documentation and Analysis of Field Case Histories of Seismic Compression during the 1994 Northridge, California, Earthquake.* Jonathan P. Stewart, Patrick M. Smith, Daniel H. Whang, and Jonathan D. Bray. October 2002.
- PEER 2002/08** *Component Testing, Stability Analysis and Characterization of Buckling-Restrained Unbonded Braces™.* Cameron Black, Nicos Makris, and Ian Aiken. September 2002.
- PEER 2002/07** *Seismic Performance of Pile-Wharf Connections.* Charles W. Roeder, Robert Graff, Jennifer Soderstrom, and Jun Han Yoo. December 2001.
- PEER 2002/06** *The Use of Benefit-Cost Analysis for Evaluation of Performance-Based Earthquake Engineering Decisions.* Richard O. Zerbe and Anthony Falit-Baiamonte. September 2001.
- PEER 2002/05** *Guidelines, Specifications, and Seismic Performance Characterization of Nonstructural Building Components and Equipment.* André Filiatrault, Constantin Christopoulos, and Christopher Stearns. September 2001.
- PEER 2002/04** *Consortium of Organizations for Strong-Motion Observation Systems and the Pacific Earthquake Engineering Research Center Lifelines Program: Invited Workshop on Archiving and Web Dissemination of Geotechnical Data, 4–5 October 2001.* September 2002.
- PEER 2002/03** *Investigation of Sensitivity of Building Loss Estimates to Major Uncertain Variables for the Van Nuys Testbed.* Keith A. Porter, James L. Beck, and Rustem V. Shaikhutdinov. August 2002.
- PEER 2002/02** *The Third U.S.-Japan Workshop on Performance-Based Earthquake Engineering Methodology for Reinforced Concrete Building Structures.* July 2002.
- PEER 2002/01** *Nonstructural Loss Estimation: The UC Berkeley Case Study.* Mary C. Comerio and John C. Stallmeyer. December 2001.
- PEER 2001/16** *Statistics of SDF-System Estimate of Roof Displacement for Pushover Analysis of Buildings.* Anil K. Chopra, Rakesh K. Goel, and Chatpan Chintanapakdee. December 2001.
- PEER 2001/15** *Damage to Bridges during the 2001 Nisqually Earthquake.* R. Tyler Ranf, Marc O. Eberhard, and Michael P. Berry. November 2001.
- PEER 2001/14** *Rocking Response of Equipment Anchored to a Base Foundation.* Nicos Makris and Cameron J. Black. September 2001.
- PEER 2001/13** *Modeling Soil Liquefaction Hazards for Performance-Based Earthquake Engineering.* Steven L. Kramer and Ahmed-W. Elgamel. February 2001.
- PEER 2001/12** *Development of Geotechnical Capabilities in OpenSees.* Boris Jeremić. September 2001.
- PEER 2001/11** *Analytical and Experimental Study of Fiber-Reinforced Elastomeric Isolators.* James M. Kelly and Shakhzod M. Takhirov. September 2001.

- PEER 2001/10** *Amplification Factors for Spectral Acceleration in Active Regions.* Jonathan P. Stewart, Andrew H. Liu, Yoojoong Choi, and Mehmet B. Baturay. December 2001.
- PEER 2001/09** *Ground Motion Evaluation Procedures for Performance-Based Design.* Jonathan P. Stewart, Shyh-Jeng Chiou, Jonathan D. Bray, Robert W. Graves, Paul G. Somerville, and Norman A. Abrahamson. September 2001.
- PEER 2001/08** *Experimental and Computational Evaluation of Reinforced Concrete Bridge Beam-Column Connections for Seismic Performance.* Clay J. Naito, Jack P. Moehle, and Khalid M. Mosalam. November 2001.
- PEER 2001/07** *The Rocking Spectrum and the Shortcomings of Design Guidelines.* Nicos Makris and Dimitrios Konstantinidis. August 2001.
- PEER 2001/06** *Development of an Electrical Substation Equipment Performance Database for Evaluation of Equipment Fragilities.* Thalia Agnanos. April 1999.
- PEER 2001/05** *Stiffness Analysis of Fiber-Reinforced Elastomeric Isolators.* Hsiang-Chuan Tsai and James M. Kelly. May 2001.
- PEER 2001/04** *Organizational and Societal Considerations for Performance-Based Earthquake Engineering.* Peter J. May. April 2001.
- PEER 2001/03** *A Modal Pushover Analysis Procedure to Estimate Seismic Demands for Buildings: Theory and Preliminary Evaluation.* Anil K. Chopra and Rakesh K. Goel. January 2001.
- PEER 2001/02** *Seismic Response Analysis of Highway Overcrossings Including Soil-Structure Interaction.* Jian Zhang and Nicos Makris. March 2001.
- PEER 2001/01** *Experimental Study of Large Seismic Steel Beam-to-Column Connections.* Egor P. Popov and Shakhzod M. Takhirov. November 2000.
- PEER 2000/10** *The Second U.S.-Japan Workshop on Performance-Based Earthquake Engineering Methodology for Reinforced Concrete Building Structures.* March 2000.
- PEER 2000/09** *Structural Engineering Reconnaissance of the August 17, 1999 Earthquake: Kocaeli (Izmit), Turkey.* Halil Sezen, Kenneth J. Elwood, Andrew S. Whittaker, Khalid Mosalam, John J. Wallace, and John F. Stanton. December 2000.
- PEER 2000/08** *Behavior of Reinforced Concrete Bridge Columns Having Varying Aspect Ratios and Varying Lengths of Confinement.* Anthony J. Calderone, Dawn E. Lehman, and Jack P. Moehle. January 2001.
- PEER 2000/07** *Cover-Plate and Flange-Plate Reinforced Steel Moment-Resisting Connections.* Taejin Kim, Andrew S. Whittaker, Amir S. Gilani, Vitelmo V. Bertero, and Shakhzod M. Takhirov. September 2000.
- PEER 2000/06** *Seismic Evaluation and Analysis of 230-kV Disconnect Switches.* Amir S. J. Gilani, Andrew S. Whittaker, Gregory L. Fenves, Chun-Hao Chen, Henry Ho, and Eric Fujisaki. July 2000.
- PEER 2000/05** *Performance-Based Evaluation of Exterior Reinforced Concrete Building Joints for Seismic Excitation.* Chandra Clyde, Chris P. Pantelides, and Lawrence D. Reaveley. July 2000.
- PEER 2000/04** *An Evaluation of Seismic Energy Demand: An Attenuation Approach.* Chung-Che Chou and Chia-Ming Uang. July 1999.
- PEER 2000/03** *Framing Earthquake Retrofitting Decisions: The Case of Hillside Homes in Los Angeles.* Detlof von Winterfeldt, Nels Roselund, and Alicia Kitsuse. March 2000.
- PEER 2000/02** *U.S.-Japan Workshop on the Effects of Near-Field Earthquake Shaking.* Andrew Whittaker, Editor. July 2000.
- PEER 2000/01** *Further Studies on Seismic Interaction in Interconnected Electrical Substation Equipment.* Armen Der Kiureghian, Kee-Jeung Hong, and Jerome L. Sackman. November 1999.
- PEER 1999/14** *Seismic Evaluation and Retrofit of 230-kV Porcelain Transformer Bushings.* Amir S. Gilani, Andrew S. Whittaker, Gregory L. Fenves, and Eric Fujisaki. December 1999.
- PEER 1999/13** *Building Vulnerability Studies: Modeling and Evaluation of Tilt-up and Steel Reinforced Concrete Buildings.* John W. Wallace, Jonathan P. Stewart, and Andrew S. Whittaker, Editors. December 1999.
- PEER 1999/12** *Rehabilitation of Nonductile RC Frame Building Using Encasement Plates and Energy-Dissipating Devices.* Mehrdad Sasani, Vitelmo V. Bertero, James C. Anderson. December 1999.
- PEER 1999/11** *Performance Evaluation Database for Concrete Bridge Components and Systems under Simulated Seismic Loads.* Yael D. Hose and Frieder Seible. November 1999.
- PEER 1999/10** *U.S.-Japan Workshop on Performance-Based Earthquake Engineering Methodology for Reinforced Concrete Building Structures.* December 1999.

- PEER 1999/09** *Performance Improvement of Long Period Building Structures Subjected to Severe Pulse-Type Ground Motions.* James C. Anderson, Vitelmo V. Bertero, and Raul Bertero. October 1999.
- PEER 1999/08** *Envelopes for Seismic Response Vectors.* Charles Menun and Armen Der Kiureghian. July 1999.
- PEER 1999/07** *Documentation of Strengths and Weaknesses of Current Computer Analysis Methods for Seismic Performance of Reinforced Concrete Members.* William F. Cofer. November 1999.
- PEER 1999/06** *Rocking Response and Overturning of Anchored Equipment under Seismic Excitations.* Nicos Makris and Jian Zhang. November 1999.
- PEER 1999/05** *Seismic Evaluation of 550 kV Porcelain Transformer Bushings.* Amir S. Gilani, Andrew S. Whittaker, Gregory L. Fenves, and Eric Fujisaki. October 1999.
- PEER 1999/04** *Adoption and Enforcement of Earthquake Risk-Reduction Measures.* Peter J. May, Raymond J. Burby, T. Jens Feeley, and Robert Wood. August 1999.
- PEER 1999/03** *Task 3 Characterization of Site Response General Site Categories.* Adrian Rodriguez-Marek, Jonathan D. Bray and Norman Abrahamson. February 1999.
- PEER 1999/02** *Capacity-Demand-Diagram Methods for Estimating Seismic Deformation of Inelastic Structures: SDF Systems.* Anil K. Chopra and Rakesh Goel. April 1999.
- PEER 1999/01** *Interaction in Interconnected Electrical Substation Equipment Subjected to Earthquake Ground Motions.* Armen Der Kiureghian, Jerome L. Sackman, and Kee-Jeung Hong. February 1999.
- PEER 1998/08** *Behavior and Failure Analysis of a Multiple-Frame Highway Bridge in the 1994 Northridge Earthquake.* Gregory L. Fenves and Michael Ellery. December 1998.
- PEER 1998/07** *Empirical Evaluation of Inertial Soil-Structure Interaction Effects.* Jonathan P. Stewart, Raymond B. Seed, and Gregory L. Fenves. November 1998.
- PEER 1998/06** *Effect of Damping Mechanisms on the Response of Seismic Isolated Structures.* Nicos Makris and Shih-Po Chang. November 1998.
- PEER 1998/05** *Rocking Response and Overturning of Equipment under Horizontal Pulse-Type Motions.* Nicos Makris and Yiannis Roussos. October 1998.
- PEER 1998/04** *Pacific Earthquake Engineering Research Invitational Workshop Proceedings, May 14–15, 1998: Defining the Links between Planning, Policy Analysis, Economics and Earthquake Engineering.* Mary Comerio and Peter Gordon. September 1998.
- PEER 1998/03** *Repair/Upgrade Procedures for Welded Beam to Column Connections.* James C. Anderson and Xiaojing Duan. May 1998.
- PEER 1998/02** *Seismic Evaluation of 196 kV Porcelain Transformer Bushings.* Amir S. Gilani, Juan W. Chavez, Gregory L. Fenves, and Andrew S. Whittaker. May 1998.
- PEER 1998/01** *Seismic Performance of Well-Confined Concrete Bridge Columns.* Dawn E. Lehman and Jack P. Moehle. December 2000.

PEER REPORTS: ONE HUNDRED SERIES

- PEER 2012/103** *Performance-Based Seismic Demand Assessment of Concentrically Braced Steel Frame Buildings.* Chui-Hsin Chen and Stephen A. Mahin. December 2012.
- PEER 2012/102** *Procedure to Restart an Interrupted Hybrid Simulation: Addendum to PEER Report 2010/103.* Vesna Terzic and Božidar Stojadinovic. October 2012.
- PEER 2012/101** *Mechanics of Fiber Reinforced Bearings.* James M. Kelly and Andrea Calabrese. February 2012.
- PEER 2011/107** *Nonlinear Site Response and Seismic Compression at Vertical Array Strongly Shaken by 2007 Niigata-ken Chuetsu-oki Earthquake.* Eric Yee, Jonathan P. Stewart, and Kohji Tokimatsu. December 2011.
- PEER 2011/106** *Self Compacting Hybrid Fiber Reinforced Concrete Composites for Bridge Columns.* Pardeep Kumar, Gabriel Jen, William Trono, Marios Panagiotou, and Claudia Ostertag. September 2011.
- PEER 2011/105** *Stochastic Dynamic Analysis of Bridges Subjected to Spatially Varying Ground Motions.* Katerina Konakli and Armen Der Kiureghian. August 2011.
- PEER 2011/104** *Design and Instrumentation of the 2010 E-Defense Four-Story Reinforced Concrete and Post-Tensioned Concrete Buildings.* Takuya Nagae, Kenichi Tahara, Taizo Matsumori, Hitoshi Shiohara, Toshimi Kabeyasawa, Susumu Kono, Minehiro Nishiyama (Japanese Research Team) and John Wallace, Wassim Ghannoum, Jack Moehle, Richard Sause, Wesley Keller, Zeynep Tuna (U.S. Research Team). June 2011.
- PEER 2011/103** *In-Situ Monitoring of the Force Output of Fluid Dampers: Experimental Investigation.* Dimitrios Konstantinidis, James M. Kelly, and Nicos Makris. April 2011.
- PEER 2011/102** *Ground-Motion Prediction Equations 1964–2010.* John Douglas. April 2011.
- PEER 2011/101** *Report of the Eighth Planning Meeting of NEES/E-Defense Collaborative Research on Earthquake Engineering.* Convened by the Hyogo Earthquake Engineering Research Center (NIED), NEES Consortium, Inc. February 2011.
- PEER 2010/111** *Modeling and Acceptance Criteria for Seismic Design and Analysis of Tall Buildings.* Task 7 Report for the Tall Buildings Initiative - Published jointly by the Applied Technology Council. October 2010.
- PEER 2010/110** *Seismic Performance Assessment and Probabilistic Repair Cost Analysis of Precast Concrete Cladding Systems for Multistory Buildings.* Jeffrey P. Hunt and Božidar Stojadinovic. November 2010.
- PEER 2010/109** *Report of the Seventh Joint Planning Meeting of NEES/E-Defense Collaboration on Earthquake Engineering. Held at the E-Defense, Miki, and Shin-Kobe, Japan, September 18–19, 2009.* August 2010.
- PEER 2010/108** *Probabilistic Tsunami Hazard in California.* Hong Kie Thio, Paul Somerville, and Jascha Polet, preparers. October 2010.
- PEER 2010/107** *Performance and Reliability of Exposed Column Base Plate Connections for Steel Moment-Resisting Frames.* Ady Aviram, Božidar Stojadinovic, and Armen Der Kiureghian. August 2010.
- PEER 2010/106** *Verification of Probabilistic Seismic Hazard Analysis Computer Programs.* Patricia Thomas, Ivan Wong, and Norman Abrahamson. May 2010.
- PEER 2010/105** *Structural Engineering Reconnaissance of the April 6, 2009, Abruzzo, Italy, Earthquake, and Lessons Learned.* M. Selim Günay and Khalid M. Mosalam. April 2010.
- PEER 2010/104** *Simulating the Inelastic Seismic Behavior of Steel Braced Frames, Including the Effects of Low-Cycle Fatigue.* Yuli Huang and Stephen A. Mahin. April 2010.
- PEER 2010/103** *Post-Earthquake Traffic Capacity of Modern Bridges in California.* Vesna Terzic and Božidar Stojadinović. March 2010.
- PEER 2010/102** *Analysis of Cumulative Absolute Velocity (CAV) and JMA Instrumental Seismic Intensity (I_{JMA}) Using the PEER–NGA Strong Motion Database.* Kenneth W. Campbell and Yousef Bozorgnia. February 2010.
- PEER 2010/101** *Rocking Response of Bridges on Shallow Foundations.* Jose A. Ugalde, Bruce L. Kutter, and Boris Jeremic. April 2010.
- PEER 2009/109** *Simulation and Performance-Based Earthquake Engineering Assessment of Self-Centering Post-Tensioned Concrete Bridge Systems.* Won K. Lee and Sarah L. Billington. December 2009.

- PEER 2009/108** *PEER Lifelines Geotechnical Virtual Data Center.* J. Carl Stepp, Daniel J. Ponti, Loren L. Turner, Jennifer N. Swift, Sean Devlin, Yang Zhu, Jean Benoit, and John Bobbitt. September 2009.
- PEER 2009/107** *Experimental and Computational Evaluation of Current and Innovative In-Span Hinge Details in Reinforced Concrete Box-Girder Bridges: Part 2: Post-Test Analysis and Design Recommendations.* Matias A. Hube and Khalid M. Mosalam. December 2009.
- PEER 2009/106** *Shear Strength Models of Exterior Beam-Column Joints without Transverse Reinforcement.* Sangjoon Park and Khalid M. Mosalam. November 2009.
- PEER 2009/105** *Reduced Uncertainty of Ground Motion Prediction Equations through Bayesian Variance Analysis.* Robb Eric S. Moss. November 2009.
- PEER 2009/104** *Advanced Implementation of Hybrid Simulation.* Andreas H. Schellenberg, Stephen A. Mahin, Gregory L. Fenves. November 2009.
- PEER 2009/103** *Performance Evaluation of Innovative Steel Braced Frames.* T. Y. Yang, Jack P. Moehle, and Božidar Stojadinovic. August 2009.
- PEER 2009/102** *Reinvestigation of Liquefaction and Nonliquefaction Case Histories from the 1976 Tangshan Earthquake.* Robb Eric Moss, Robert E. Kayen, Liyuan Tong, Songyu Liu, Guojun Cai, and Jiaer Wu. August 2009.
- PEER 2009/101** *Report of the First Joint Planning Meeting for the Second Phase of NEES/E-Defense Collaborative Research on Earthquake Engineering.* Stephen A. Mahin et al. July 2009.
- PEER 2008/104** *Experimental and Analytical Study of the Seismic Performance of Retaining Structures.* Linda Al Atik and Nicholas Sitar. January 2009.
- PEER 2008/103** *Experimental and Computational Evaluation of Current and Innovative In-Span Hinge Details in Reinforced Concrete Box-Girder Bridges. Part 1: Experimental Findings and Pre-Test Analysis.* Matias A. Hube and Khalid M. Mosalam. January 2009.
- PEER 2008/102** *Modeling of Unreinforced Masonry Infill Walls Considering In-Plane and Out-of-Plane Interaction.* Stephen Kadysiewski and Khalid M. Mosalam. January 2009.
- PEER 2008/101** *Seismic Performance Objectives for Tall Buildings.* William T. Holmes, Charles Kircher, William Petak, and Nabih Youssef. August 2008.
- PEER 2007/101** *Generalized Hybrid Simulation Framework for Structural Systems Subjected to Seismic Loading.* Tarek Elkhoraibi and Khalid M. Mosalam. July 2007.
- PEER 2007/100** *Seismic Evaluation of Reinforced Concrete Buildings Including Effects of Masonry Infill Walls.* Alidad Hashemi and Khalid M. Mosalam. July 2007.

The Pacific Earthquake Engineering Research Center (PEER) is a multi-institutional research and education center with headquarters at the University of California, Berkeley. Investigators from over 20 universities, several consulting companies, and researchers at various state and federal government agencies contribute to research programs focused on performance-based earthquake engineering.

These research programs aim to identify and reduce the risks from major earthquakes to life safety and to the economy by including research in a wide variety of disciplines including structural and geotechnical engineering, geology/seismology, lifelines, transportation, architecture, economics, risk management, and public policy.

PEER is supported by federal, state, local, and regional agencies, together with industry partners.



PEER Core Institutions

University of California, Berkeley (Lead Institution)
California Institute of Technology
Oregon State University
Stanford University
University of California, Davis
University of California, Irvine
University of California, Los Angeles
University of California, San Diego
University of Nevada, Reno
University of Southern California
University of Washington

PEER reports can be ordered at <https://peer.berkeley.edu/peer-reports> or by contacting

Pacific Earthquake Engineering Research Center
University of California, Berkeley
325 Davis Hall, Mail Code 1792
Berkeley, CA 94720-1792
Tel: 510-642-3437
Email: peer_center@berkeley.edu

ISSN 2770-8314
<https://doi.org/10.55461/AORD2776>